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# Synthesis, characterization and activity pattern of Cu–ZnO/ZrO<sub>2</sub> catalysts in the hydrogenation of carbon dioxide to methanol

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## Abstract

A novel synthesis route based on reverse co-precipitation under ultrasound irradiation has led to  $Cu-ZnO/ZrO_2$  catalysts ( $Zn_{at}/Cu_{at}$ , 0–3;  $ZrO_2$ , 42–44 wt%) with a remarkable development of total surface area ( $SA_{BET}$ , 120–180 m<sup>2</sup>/g) and very high dispersion (3–58%) and exposure (MSA 9–63 m<sup>2</sup>/g) of the active Cu phase. The activity pattern in the hydrogenation of CO<sub>2</sub> to CH<sub>3</sub>OH ( $T_R$ , 433–533 K;  $P_R$ , 1.0–3.0 MPa) was addressed in comparison with a commercial Cu–ZnO/Al<sub>2</sub>O<sub>3</sub> methanol synthesis catalyst. Volcano-shaped trends in total and metal surface area signal an optimum zinc loading (Zn/Cu, 0.3–0.7), ensuring higher concentration of active sites and methanol productivity values, whereas the basic relationships among dispersion, reducibility, and TOF indicate a structurally sensitive character of the title reaction and a superior reactivity of poorly dispersed Cu particles. Thermodynamic analysis of the reaction stream revealed that methanol formation proceeds along a parallel path, whereas a stronger "water affinity" accounts for the poorer performance of the conventional alumina-based catalyst compared with zirconia-based ones.

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Keywords: Cu-ZnO/ZrO<sub>2</sub> catalysts; CO<sub>2</sub> hydrogenation; CH<sub>3</sub>OH synthesis; Physicochemical characterization; Dispersion; Reducibility; Catalytic pattern; Structure sensitivity

### 1. Introduction

Incessant technological progress over the past century aimed at continuously improving lifestyle quality has produced a progressive deterioration of natural resources and rise in pollutant levels in the atmosphere, responsible for global warming ("greenhouse effect") and, in turn, impressive climate changes in recent years [1,2]. Pressed by the imperative to avoid further irreversible damage to the environment with the resulting catastrophic consequences for the future of mankind, many countries worldwide are now pursuing a general reduction of pollutant and carbon dioxide emissions, the major contributors to the greenhouse effect [1]. Among the viable strategies to reduce carbon dioxide emissions, mostly "sequestration" and

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novel process technologies based on " $CO_2$  recycling," are actually attracting the major scientific and technological interest [3]. Indeed, the approach of using  $CO_2$  as "reagent" for producing bulk chemicals like methanol and dimethylether (DME) [4–8] appears to be particularly attractive, because these are also potential substitutes for traditional oil-based fuels for automobiles, which may help reduce air pollution in metropolitan areas [4]. Accomplishing the strategic goal of reducing the Western nations' dependence on oil, these energy carriers are in fact easily accessible from natural gas (NG) via syngas. The ability to exploit  $CO_2$ -rich NG resources and the possibility of decreasing the reforming temperature to reduce syngas generation costs [1–3] are other important advantages of the methanol synthesis via  $CO_2$  hydrogenation.

Currently, methanol synthesis is run mostly on Cu–ZnO/ $Al_2O_3$  catalysts at 493–573 K and a pressure of 5–10 MPa with a syngas feed containing typically 5% CO–5% CO<sub>2</sub> and H<sub>2</sub> [9–11]. However, recent studies have found that methanol

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Table 1	
List of the studied catalysts and relative physicochemical pr	operties

Code <sup>a</sup>	Chemical composition (%)		Znat/Cuat	SABET	PV	APD	MSA <sup>b</sup>	$D_{Cu}^{b}$	$d_{Cu}^{b}$	
	CuO	ZnO	ZrO <sub>2</sub>		$(m^2/g_{cat})$	$(cm^3/g_{cat})$	(Å)	$(m^2/g_{cat})$	(%)	(nm)
Cu(12)/ZrO <sub>2</sub> (6)	58.6	0	41.4	0.0	118	0.33	74	8.7	3.3	32
Cu(11)ZnO(1)/ZrO <sub>2</sub> (6)	51.9	4.6	43.5	0.1	128	0.24	91	17.4	6.2	17
Cu(10)ZnO(2)/ZrO <sub>2</sub> (6)	45.0	11.8	43.2	0.3	163	0.59	118	63.0	27.6	4
Cu(9)ZnO(3)/ZrO <sub>2</sub> (6)	41.2	14.8	44.0	0.4	174	0.56	106	60.8	29.1	4
Cu(8)ZnO(4)/ZrO <sub>2</sub> (6)	36.2	19.6	44.2	0.5	162	0.54	110	59.7	32.5	3
Cu(7)ZnO(5)/ZrO <sub>2</sub> (6)	31.6	24.0	44.4	0.7	159	0.36	85	59.3	37.0	3
Cu(3)ZnO(9)/ZrO <sub>2</sub> (6)	15.1	41.8	43.1	2.7	147	0.35	73	44.7	57.9	2
ZnO(12)/ZrO <sub>2</sub> (6)	0	56.1	43.9	-	103	0.31	121	_	-	-
$Cu(4)ZnO(4)/Al_2O_3(6)$	35.0	33.1	_ c	0.9	105	0.23	70	34.4	19.2	5

<sup>a</sup> Number in parentheses refer to the atomic/molecular concentration.

<sup>b</sup> From "single-pulse" (363 K) N<sub>2</sub>O titration measurements (see Ref. [60]).

 $^{\rm c}$  Commercial synthesis catalyst containing Al\_2O\_3 (31.9 wt%) as carrier.

can be obtained with rates and carbon utilization factors superior than those of the traditional route by  $CO_2$  hydrogenation [11,12]. Even if some details of the reaction mechanism remain controversial, several authors have in fact claimed that under typical industrial conditions, methanol is formed mostly via  $CO_2$  hydrogenation, with CO serving as the  $CO_2$  source and as a scavenger of oxygen atoms coming from water, which in turn acts as an inhibitor of the active metal sites [9–11]. Just water formation would account for the poorer performance of traditional alumina-supported catalysts in  $CO_2$ -rich syngas feed-stocks [13–15] compared with zirconia-based systems [16–22]. Moreover, despite being generally attributed to a synergism of  $Cu^0-Cu^+$  sites and the reactivity of ZnO-promoted catalysts [6,14,23–28], the catalytic role of  $Cu^0$  [29,30] and/or Cu–Zn alloy [31–37] also has been envisaged.

Many research groups have adopted unconventional preparation routes to improve the activity, selectivity, poison resistance, or lifetime of Cu-ZnO systems [20-24,26,38-53]. For example, Coteron and Hayhurst [54] found that Cu–Zn catalysts prepared by "spark-erosion" feature high methanol selectivity, whereas we ascribed higher TOF in the CO<sub>2</sub> hydrogenation reaction to a very "intimate" contact of the Cu/ZnO/ZrO2 phases ensured by the "combustion" route [55]. Köppel et al. [22] and Sun and Sermon [56] adopted the sol-gel technique to enhance total and metal surface areas, whereas Jingfa et al. [57] emphasized the superior activity of oxalate-coprecipitated catalysts. Dopant addition [24,46-49] was found to improve either dispersion or Cu-Zn(O) contact area [20-22,26,38-45], whereas alternative active phases (e.g., Ag, Au) seem to exhibit superior selectivity in the CO<sub>2</sub> hydrogenation reaction [23,50-53].

Consequently, the present study was undertaken to assess the efficiency of a new preparation method based on reverse co-precipitation under ultrasound irradiation in improving the physicochemical properties of the Cu–ZnO/ZrO<sub>2</sub> system. Catalytic tests in a wide range of experimental conditions and the relative thermodynamic evaluations can provide fundamental insight into process optimization and structural factors controlling the functionality of the Cu–ZnO system in the CO<sub>2</sub> hydrogenation reaction.

## 2. Experimental

#### 2.1. Materials

A series of Cu-ZnO/ZrO<sub>2</sub> catalysts with different Zn/Cu atomic ratios (0–3) and a constant zirconia loading ( $\approx$ 44 wt%) was prepared by the new reverse co-precipitation under ultrasound irradiation route [58] as follows. An aqueous solution (ca. 100 mL) of the  $Cu(NO_3)_2 \cdot 3H_2O$ ,  $Zn(NO_3)_2 \cdot 6H_2O$ , and ZrO(NO<sub>3</sub>)<sub>2</sub>·nH<sub>2</sub>O (Sigma Aldrich) precursors was added dropwise under vigorous stirring to a 0.1 M NaHCO<sub>3</sub> solution (500 mL) kept in an ultrasound bath (Bransonic B-120E1) operating at 47 kHz and with a power of 30 W (T =310-320 K) [58]. The pH of the precipitating solution was maintained in the range of 7.0-7.5 by the continuous addition of a 0.1 M NaHCO<sub>3</sub> solution. After precipitation, the solid was kept for another 30 min under stirring and ultrasound irradiation, then aged at room temperature for 2 h, filtered, and washed with hot distilled water. Thereafter the catalysts were dried at 373 K for 16 h and further calcined in air at 623 K for 4 h. Powdered catalysts were pressed (40 MPa), crushed, and sieved to the particle size fraction (40–70 mesh) used for both characterization and testing measurements. A commercial Cu-ZnO/Al<sub>2</sub>O<sub>3</sub> methanol synthesis catalyst (G66A, Sud Chemie AG) was used as a reference system. The catalysts' relative notation and main physicochemical properties are listed in Table 1.

#### 2.2. Physicochemical characterization

Surface area (SA<sub>BET</sub>), pore volume (PV), and the pore size distribution (PSD) were determined from the nitrogen adsorption/desorption isotherms at 77 K, using a fully automated ASAP 2010 (Micromeritics) gas adsorption device. Before analysis, all the samples were outgassed at 423 K under vacuum for 2 h. The isotherms were elaborated according to the BET method for surface area calculation, with the Horwarth–Kavazoe and BJH methods used for micropore and mesopore evaluation, respectively.

Temperature-programmed reduction (TPR) measurements at 273–1073 K were performed in a continuous-flow apparatus

using a linear quartz microreactor (4 mm i.d.) fed with a 6% H<sub>2</sub>/Ar mixture flowing at 60 stp mL/min and heated at the rate of 20 K/min. A ca. 15-mg catalyst sample was used, with H<sub>2</sub> consumption monitored by a TCD quantitatively calibrated with a commercial CuO standard (Carlo Erba) [59].

Metal surface area (MSA) values were obtained with  $\pm 5\%$ accuracy by single-pulse (1.0 mL) N<sub>2</sub>O titration (T = 363 K) [60]. Before measurements, catalysts were reduced in situ at 573 K in a H<sub>2</sub> flow (100 stp mL/min) for 1 h. After reduction, the samples were "flushed" in the He carrier flow at 583 K for 15 min, and then cooled to 363 K. For the MSA calculations, a Cu:N<sub>2</sub>O = 2:1 chemisorption stoichiometry and a value of  $1.46 \times 10^{19}$  Cu atom/m<sup>2</sup> density were assumed, with the volume surface average particle size ( $d_{Cu}$ ) obtained from the conventional formula

$$d_{\rm Cu} \,({\rm nm}) = \frac{104}{D \,(\%)}$$

assuming a spherical shape of Cu particles [29,60].

X-ray diffraction (XRD) analysis of samples in the  $2\theta$  range 10–80° was performed using a Philips X-Pert diffractometer operating with Ni  $\beta$ -filtered Cu $K_{\alpha}$  radiation at 40 kV and 30 mA. Thermogravimetric (TG-DSC) analysis of the dried and calcined samples in the range 293–1073 K was performed using a Netzsch STA 409 C analyzer running at a heating rate of 12 K/min in air atmosphere.

## 2.3. Catalyst testing

Catalyst tests in the hydrogenation of CO<sub>2</sub> were performed at 433-533 K and 1.0-3.0 MPa using an Inconel microreactor (6 mm i.d.). A CO<sub>2</sub>-H<sub>2</sub>-N<sub>2</sub> reaction mixture with a molar ratio of 3/9/1 was fed at the rate of 40 stp mL/min  $(GHSV = 4400 N L/(hkg_{cat}))$  or 80 stp mL/min (GHSV = 8800 N L/(hkg<sub>cat</sub>)) on a 0.5-g catalyst sample diluted with 0.5 g of same-sized SiC. The temperature was controlled by a thermocouple in contact with the catalyst bed. Before each test, the catalysts were reduced in situ at 573 K for 1 h in  $H_2$  flow (100 stp mL/min) at atmospheric pressure. Then the reactor was cooled to 433 K and the reaction mixture was admitted, raising the pressure to 1.0 or 3.0 MPa. The activity was probed by performing heating-cooling cycles to rule out "hysteresis" phenomena. The reaction stream was analyzed by a gas chromatograph equipped with a two-column analytical system connected to a flame ionization detector (CH<sub>3</sub>OH, CH<sub>3</sub>OCH<sub>3</sub>) and thermal conductivity detector (CO, N2, CO2, H2). Conversion values were calculated by both internal standard (a) and mass-balance (b) methods,

$$X_{\rm CO_2} = 1 - \left[ (\rm CO_{2,out} / \rm CO_{2,in}) \cdot (\rm N_{2,in} / \rm N_{2,out}) \right]$$
(a)

and

$$X_{\rm CO_2} = {\rm CO}_{2,\rm out} / \left( \sum_{\rm prod} + {\rm CO}_{2,\rm out} \right), \tag{b}$$

with selectivity data obtained from standard formulas

$$S_{\rm CH_3OH} = \rm CH_3OH_{out} / (1 - \rm CO_{2,out})$$
(a')



Fig. 1. TG and DSC profiles of the "dried" and "calcined"  $\mbox{Cu(9)ZnO(3)/ZrO_2(6)}$  catalyst.

and

$$S_{CH_3OH} = CH_3OH_{out} / \sum_{prod}$$
 (b')

Each data set was obtained, with an accuracy of  $\pm 3\%$ , from an average of three independent measurements.

## 3. Results

#### 3.1. Physicochemical characterization

The systematic TG-DSC study of representative "dried" and "calcined" catalyst samples was preliminarily carried out to determine the minimum calcination temperature for attaining complete decomposition of precursors. The TG-DSC pattern of the dried Cu(9)ZnO(3)/ZrO<sub>2</sub>(6) catalyst (Fig. 1) exhibits considerable ( $\approx 25\%$ ) weight loss in the range 300–620 K, with an exothermal peak at ca. 600 K and only negligible weight variations thereafter up to 1073 K. Indeed, with a ca. 5 wt% loss below 400 K due to dehydration, TGA confirms the substantial thermal stability of the catalyst sample previously calcined at 623 K for 4 h. Only a small exothermic peak at ca. 900 K, analogous to that observed for the dried sample, is associated with a comparably small weight loss (<1%). Based on this, we systematically adopted a calcination temperature of 623 K to ensure complete decomposition of catalyst precursor(s) and minimize sintering phenomena.

Surface characterization data confirm that the new synthesis route improves the total surface exposure to remarkably high levels (Table 1), although the ZnO content has a significant influence on catalyst texture (Fig. 2A). Lower SA<sub>BET</sub> (120–130 m<sup>2</sup>/g) values are in fact recorded at low ( $\leq 0.1$ ) and high (>0.7) Zn/Cu ratios, with the maximum value of 175 m<sup>2</sup>/g found for a Zn/Cu of 0.3–0.4 (Fig. 2A). It is noteworthy that similar changes in the Cu surface exposure account for a straight-line increase of MSA with SA<sub>BET</sub> from 9 to 63 m<sup>2</sup>/g<sub>cat</sub> (Fig. 2B). Further, both pore volume (Fig. 2A) and



Fig. 2. (A) Effect of the Zn/Cu atomic ratio on the SA<sub>BET</sub> and pore volume of the Cu–ZnO/ZrO<sub>2</sub> catalysts. (B) Relationship between MSA and SA<sub>BET</sub> of the Cu–ZnO/ZrO<sub>2</sub> catalysts.

average pore diameter (Table 1) follow a trend analogous to that of SA<sub>BET</sub> due to marked changes in the PSD (Fig. 3). The "unpromoted" Cu(12)/ZrO<sub>2</sub>(6) system (Fig. 3A) displays a very "broad" and featureless PSD, accounting for a cumulative volume of ca. 0.33 cm<sup>3</sup>/g. In contrast, the catalyst with intermediate Zn/Cu ratio (0.4) is characterized by a prevalence of 70–120 Å mesopores (Fig. 3B), resulting in a much greater cumulative volume (ca. 0.6 cm<sup>3</sup>/g). Although a pronounced maximum is centered at 90 Å (Fig. 3C), the Cu(3)ZnO(9)/ZrO<sub>2</sub>(6) sample with the largest (2.7) Zn/Cu ratio has a pore volume (0.3 cm<sup>3</sup>/g) comparable with that of low Zn-loaded samples (Table 1).

The results of XRD measurements performed to obtain information on the crystalline phases present both on dried (Fig. 4A) and calcined (Fig. 4B) catalysts are collected in Fig. 4. Apart from minor differences in the  $2\theta$  range of  $15-30^{\circ}$ , the rather featureless diffraction patterns indicate a significant lack of "long-range" crystalline order in both dried and calcined Cu(9)ZnO(3)/ZrO<sub>2</sub>(6) samples (Fig. 4A). However, similar diffraction patterns signal that all of the calcined samples (Fig. 4B) with Zn/Cu > 0.1 are characterized by a prevalently amorphous architecture. Only at low ( $\leq 0.1$ ) Zn loading are the typical reflexes of a crystalline tenorite (JCPDS 5-661) CuO phase evident [59]. Applying Sherrer's equation to the  $\langle 002 \rangle$ line produces mean CuO particle sizes of 12 nm for Cu(12)/ ZrO<sub>2</sub>(6) and 10 nm for Cu(11)ZnO(1)/ZrO<sub>2</sub>(6). Then the significantly larger  $d_{Cu}$  value quoted for the former system from N<sub>2</sub>O uptake measurements (Table 1) should indicate a major resistance to sintering of the promoted  $Cu(11)ZnO(1)/ZrO_2(6)$ sample.

TPR measurements were carried out to highlight the reduction pattern of the various catalysts and settle a proper activation (reduction) protocol for testing. The reduction profiles of the studied catalysts are shown in Fig. 5, and the onset ( $T_{o,red}$ ) and maximum ( $T_{Mi}$ ) temperatures and the values of hydrogen consumption are summarized in Table 2. All of the systems display reduction profiles characterized by a main peak with a  $T_{M1}$  maximum between 486 and 511 K, well below that of the standard bulk CuO (ca. 570 K), accounting for a regu-



Fig. 3. Pore size distribution curves of representative Cu-ZnO/ZrO2 catalysts.

lar rise in the onset temperature of reduction with the Zn/Cu ratio (Table 2). A shoulder on the left side of the maximum is particularly evident at low Zn content [Cu(12)/ZrO<sub>2</sub>(6) and Cu(11)ZnO(1)/ZrO<sub>2</sub>(6)], whereas the peak is sharper and much more symmetrical for all of the other systems. The amount of hydrogen consumption at 273–573 K is always close to (although somewhat greater than) the stoichiometric amount for CuO reduction (H<sub>2</sub>/Cu = 1.05–1.22). Moreover, a baseline drift at 573–1073 K with a poorly resolved  $T_{M2}$  maximum (830–890 K), the shape of which depends on the zinc loading,



Fig. 4. XRD patterns of the "dried" and "calcined"  $Cu(9)ZnO(3)/ZrO_2(6)$  samples (A) and of the calcined catalysts with different Zn/Cu ratio (B).

Table 2

TPR data of Cu–ZnO/ZrO<sub>2</sub> catalysts. Onset temperature of reduction ( $T_{o,red}$ ), temperature of peak maxima ( $T_{Mi}$ ) and extent of hydrogen consumption

Catalyst	$T_{\rm o, red}$	$T_{M1}$	$T_{M2}$	mmol H <sub>2tot</sub> /g <sub>cat</sub>	H <sub>2</sub> /Cu <sup>a</sup>
	(K)	(K)	(K)		
Cu(12)/ZrO <sub>2</sub> (6)	388	501	831	9.2	1.22
Cu(11)ZnO(1)/ZrO <sub>2</sub> (6)	390	511	870	7.8	1.15
Cu(10)ZnO(2)/ZrO <sub>2</sub> (6)	395	486	831	8.4	1.06
Cu(9)ZnO(3)/ZrO <sub>2</sub> (6)	404	488	845	8.2	1.13
Cu(8)ZnO(4)/ZrO <sub>2</sub> (6)	428	497	826	6.7	1.05
Cu(7)ZnO(5)/ZrO <sub>2</sub> (6)	431	501	845	6.1	1.07
Cu(3)ZnO(9)/ZrO <sub>2</sub> (6)	448	506	862	2.7	1.11
ZnO(12)/ZrO <sub>2</sub> (6)	_	_	891	1.4	-
$Cu(4)ZnO(4)/Al_2O_3(6)$	422	521	962	6.1	0.98
CuO "bulk"	474	568	-	12.6	1.00

<sup>a</sup> In the *T* range: 273–573 K.

Table 3



Fig. 5. TPR profiles of the Cu–ZnO/ZrO $_2$  and reference catalysts.

is associated with an ongoing reduction of the ZnO promoter and/or the decomposition of a residual carbonate phase (Fig. 1).

The TPR profile of the reference catalyst is similar to that of Cu–ZnO/ZrO<sub>2</sub> catalysts, with a main peak centered at 521 K and markedly skewed on the low-*T* side ( $T_{o,red} = 422$  K), accounting for a stoichiometric H<sub>2</sub>/Cu ratio (Table 2). Also at T > 573 K, the trend in H<sub>2</sub> consumption appears similar, even though a poorly resolved maximum occurs at temperatures above those for Cu–ZnO/ZrO<sub>2</sub> catalysts (Table 2).

## 3.2. Catalytic activity

Activity data of representative catalysts in the CO<sub>2</sub> hydrogenation reaction ( $T_{\rm R} = 473-513$  K; GHSV = 4400 N L/ (hkg<sub>cat</sub>);  $P_{\rm R} = 1.0$ ; 3.0 MPa) are collected in Table 3 in terms of CO<sub>2</sub> conversion ( $X_{\rm CO_2}$ ) and CH<sub>3</sub>OH selectivity ( $S_{\rm CH_3OH}$ ). At lower pressure, all the systems feature a similar catalytic pattern characterized by  $X_{\rm CO_2}$  values rising from 4 to 14%, counterbalanced by a drop in  $S_{\rm CH_3OH}$  from 63 to 17%, whereas

Conversion-selectivity data ( $X_{CO_2}$ - $S_{CH_3OH}$ ) of Cu–ZnO/ZrO<sub>2</sub> and reference catalysts in the CO<sub>2</sub> hydrogenation reaction at different temperature and pressure (GHSV, 4400 N L/(hkg<sub>cat</sub>))

Catalyst	<i>P</i> <sub>R</sub> , 1.0 MPa			<i>P</i> <sub>R</sub> , 3.0 MPa			
	<i>T</i> <sub>R</sub> , 473 K	<i>T</i> <sub>R</sub> , 493 K	<i>T</i> <sub>R</sub> , 513 K	<i>T</i> <sub>R</sub> , 473 K	<i>T</i> <sub>R</sub> , 493 K	<i>T</i> <sub>R</sub> , 513 K	
Cu(12)/ZrO <sub>2</sub> (6)	3.9-63.0	7.1-41.1	11.4-25.2	7.2-70.2	12.6-57.4	17.6-48.8	
$Cu(10)ZnO(2)/ZrO_{2}(6)$	5.8-55.2	10.0-35.5	14.1-18.0	6.2-66.9	10.8-49.9	16.5-45.0	
$Cu(3)ZnO(9)/ZrO_2(6)$	4.1-59.5	8.6-34.6	13.3-16.9	6.5-70.9	12.6-55.2	17.5-48.4	
$Cu(4)ZnO(4)/Al_2O_3(6)$	5.5-53.8	10.2-30.9	14.2–18.6	6.4-72.0	11.5-56.0	15.9–48.4	

at 3.0 MPa, a systematic increase of  $X_{CO_2}$  from 6 to 18% implies a much smaller decrease in S<sub>CH3OH</sub> from 73 to 45%. Overall, under such experimental conditions, a very slight affect of the composition on reactivity of the Cu-ZnO system is found. However, comparing the selectivity-conversion pattern of the Cu(10)ZnO(2)/ZrO<sub>2</sub>(6) and reference catalyst at higher GHSV  $(8800 N L/(hkg_{cat}))$  demonstrates the poorer performance of the latter system at both 1.0 and 3.0 MPa, mainly in terms of methanol selectivity (Fig. 6). Through a systematic decrease with conversion, at 1.0 MPa an increase in  $X_{CO_2}$  from 0.5 to 2.5% (reference catalyst) and to 3.5% [Cu(10)ZnO(2)/ZrO<sub>2</sub>(6)] causes a steep decay in S<sub>CH<sub>3</sub>OH</sub>, from 100% to ca. 65%. At 3.0 MPa, a much more pronounced increase in  $X_{CO_2}$  (from ca. 2.5% to 7-7.5%) accounts for "smoother" decreases in the  $S_{CH_3OH}$  from 100 to 50% on the reference catalyst and 75% on Cu(10)ZnO(2)/ZrO<sub>2</sub>(6). Accordingly, productivity data (STY, kg<sub>CH<sub>2</sub>OH</sub>/(kg<sub>cat</sub> h)) as a function of the Zn/Cu ratio (Fig. 7) display an optimum Zn/Cu ratio of 0.3-0.5, ensuring higher STY values at both low (Fig. 7A) and higher (Fig. 7B) GHSV's. In



Fig. 6. Selectivity to methanol vs  $X_{CO_2}$  (GHSV, 8800 N L/(hkg<sub>cat</sub>)) for the Cu(10)ZnO(2)/ZrO<sub>2</sub>(6) and reference catalysts at 1.0 and 3.0 MPa in the range 473–513 K.

comparison, the productivity of the reference system is particularly depressed at the highest GHSV (Fig. 7B).

Short-term stability tests on the reference and Cu(9)ZnO(3)/ ZrO<sub>2</sub>(6) catalysts at 473 K and 1.0 MPa (GHSV = 4400 N L/ (hkg<sub>cat</sub>)) were carried out to address the occurrence of potential deactivation phenomena. Both catalysts exhibited constant conversion–selectivity values during 18 h of time on stream, indicating substantial stability of the Cu–ZnO system irrespective of the carrier.

#### 4. Discussion

#### 4.1. Aims and strategy of the design of the new synthesis route

Addressing the effects of the preparation method (e.g., combustion, coprecipitation), we previously ascertained a marked influence of the textural properties on the CO<sub>2</sub> hydrogenation pattern of Cu-ZnO/ZrO2 catalysts [55]. However, the low development of total and/or metal surface areas has prompted the search for more effective synthesis routes to improve the texture and reactivity of the Cu-ZnO/ZrO<sub>2</sub> system [55]. Due to the different precipitation kinetics of each cation, the conventional coprecipitation technique leads to mixtures of more or less small "monophase" particles, with limited dispersion of the active phase in the final catalyst [22,40,55–57,61]. To overcome this drawback, we attempted to accomplish simultaneous precipitation of the three cations ( $Cu^{2+}$ ,  $Zn^{2+}$ , and  $ZrO^{2+}$ ) through a slow dropwise addition of the precursor solution to a large volume of the precipitating agent (i.e., reverse coprecipitation), keeping the pH between 7.0 and 7.5 to allow for coprecipitation of precursors mostly as (hydroxi)carbonates. Moreover, evaluating the influence of the ultrasound field on the textural properties of the representative Cu(9)ZnO(3)/ZrO<sub>2</sub>(6) system, we preliminarily found improvements in both SA<sub>BET</sub> ( $\approx 10\%$ ) and MSA ( $\approx$ 20%) due to irradiation during co-precipitation [55,58]. Based on such evidence, we systematically adopted the reverse co-precipitation under ultrasound irradiation technique for catalyst preparation.



Fig. 7. STY of Cu–ZnO/ZrO2 catalysts vs Zn/Cu ratio at 453 and 473 K and 1.0 MPa. (A) GHSV, 4400 N L/(hkg<sub>cat</sub>); (B) GHSV, 8800 N L/(hkg<sub>cat</sub>).

#### 4.2. Structural properties

Surface area and, mostly, metal dispersion and MSA values (Table 1) were much larger than those reported so far for bulky Cu-based catalysts [22,40,55–57,61]. This finding provides the best indication of the successful strategy of design of the reverse co-precipitation under ultrasound irradiation route [58]. Indeed, the improvement in textural properties depends on the characteristics of the preparation method that allows precipitation of very small oxide particles, also ensuring very good mixing of the various precursors in the first stage of solid formation [58]. Together, the evident  $CO_2$  release during aging, the weight loss (Fig. 1) corresponding to ca. 70% decomposition of carbonates, and the peculiar diffraction pattern of the dried Cu(9)ZnO(3)/ZrO<sub>2</sub>(6) sample (Fig. 4A) provide probatory experimental evidence supporting the formation of a homogeneous hydroxycarbonate phase in the co-precipitation stage. Its subsequent decomposition by the "soft" calcination treatment (at 623 K) retains a disordered architecture with no significant long-range crystalline order (Fig. 4B). Meanwhile, the very fine texture of the oxide particles, the sintering of which would be hindered by the release of great amounts of CO<sub>2</sub> from (hydroxy)carbonate decomposition, accounts for a very significant surface exposure. Then the stabilization of a prevalently amorphous structure for Zn/Cu > 0.1 (Fig. 4) matches the greater development of total and metal surface area (Fig. 2). Whereas at low ZnO concentration (Zn/Cu < 0.3), segregation of the crystalline CuO (tenorite) phase (Fig. 4) matches the lower SA<sub>BET</sub>, MSA, and D values of the Cu(12)/ZrO<sub>2</sub>(6) and Cu(11)ZnO(1)/ZrO<sub>2</sub>(6) samples (Table 1). Therefore, the shape of the reduction peak (Fig. 5) also should be related to the morphology of the CuO phase, which is in turn affected by the ZnO loading. In fact, a broad and "stepped" TPR peak could signal the reduction of different-sized CuO particles in the  $Cu(12)/ZrO_2(6)$  and  $Cu(11)ZnO(1)/ZrO_2(6)$  samples. Considering surface (Table 1) and structural (Fig. 4) characterization data, and the higher  $T_{M1}$  value recorded for the bulk CuO system (Table 2), the component at higher temperature (Fig. 5) can be assigned to the more difficult reduction of larger crystalline CuO particles [59,61]. In contrast, a narrower and more symmetric peak shape of the catalysts with Zn/Cu > 0.1 denotes the simultaneous reduction of smaller CuO particles with a much more uniform size distribution [59,61]. Such data infer a fundamental role of the ZnO as a structural promoter of the active Cu phase, which in turn affects the reducibility of the system. In fact, an exponential increase in metal dispersion with the Zn/Cu ratio (Fig. 8A) parallels a straightforward increase in  $T_{o,red}$  with ZnO loading (Fig. 8B). This suggests that a weaker Cu-O bond strength enables easier generation of "inucleation" metal centers (e.g.,  $T_{0,red}$ ) on large CuO particles characterized by only slight (if any) interaction with the ZnO promoter, whereas the higher dispersion and stronger promoter interaction of the CuO phase cause a shift of  $T_{o,red}$  to higher temperatures at greater ZnO loadings. Nevertheless, a faster reduction of smaller CuO particles in the bulk would explain the lower  $T_{M1}$  values of the systems characterized by larger Zn/Cu ratios [61]. Overall, higher  $T_{M1}$  and  $T_{M2}$  values signal a more difficult reduction of both active phase and promoter on the reference system, likely due to the stronger interaction with the  $Al_2O_3$  carrier [61]. Spanning a dispersion range (3–58%) much larger than that attained so far for massive Cu-based catalysts [22,40,55–57,61], the novel synthesis route indicates a very effective CuO-ZnO/ZrO2 interaction affecting the texture, morphology, and reactivity of Cu-ZnO/ZrO<sub>2</sub> catalysts [61].

#### 4.3. Structure-activity relationships

Although different physicochemical properties point to an optimum Zn/Cu ratio ensuring the maximum development of  $SA_{BET}$  and MSA (Fig. 2), catalyst productivity is not a direct function of such parameters [31,61,62]. Actually, variations in MSA of about 1 order of magnitude (9–63 m<sup>2</sup>/g) reflect in a less than threefold rise in STY between minimum and maximum (Fig. 7). Then it can be argued that the different reactivities of active centers, a multicenter reaction path, and/or thermodynamic factors combine to "smooth" the potential of the



Fig. 8. (A) Effect of the Zn/Cu ratio on metal dispersion; (B) relationship between onset temperature of reduction (Table 2) and ZnO loading.



Fig. 9. (A) Methanol selectivity vs conversion data of the various catalysts in the range 453–513 K at 1.0 and 3.0 MPa. (B) STY of the various catalysts in the range 453-513 K. (- - -) Represent equilibrium data at 1.0 and 3.0 MPa.



Fig. 10. Influence of the metal dispersion (A) and average Cu particle diameter (B) on the turnover frequency of CO<sub>2</sub> conversion and CH<sub>3</sub>OH formation ( $T_R$ , 473 K;  $P_R$ , 1.0 MPa; GHSV, 8800 N L/(hkg<sub>cat</sub>)).

MSA exposure. This is confirmed by the fact that the catalytic pattern of all Cu–ZnO/ZrO<sub>2</sub> catalysts can be described by general relationships between selectivity and conversion (Fig. 9A) and between STY and temperature (Fig. 9B). Due to the marked volume decrease of the synthesis reaction, these correlations are strongly dependent on pressure. Overall, a much smaller decrease in methanol selectivity coupled with higher conversions provide substantially larger STY values at 3.0 MPa (Fig. 9B), with the maximum values (0.12–0.14 kg<sub>CH<sub>3</sub>OH</sub>/(kg<sub>cat</sub> h)) equal to or greater than those attained so far under even more favorable reaction conditions [22,29,35,41].

To highlight the slight influence of MSA on STY, it is helpful to evaluate the influence of Cu dispersion on the reactivity of the metal phase. The turnover frequency (TOF, s<sup>-1</sup>) of CH<sub>3</sub>OH formation and CO<sub>2</sub> conversion ( $T_R = 473$  K;  $P_R = 1.0$  MPa; GHSV = 8800 N L/(hkg<sub>cat</sub>)) as functions of Cu dispersion (Fig. 10A) and particle size (Fig. 10B) are shown in Fig. 10. Matching with the TOF values of methanol reforming reactions under similar experimental conditions [61], such values depict analogously decreasing curves (Fig. 10A), accounting for the linear decrease in reactivity of metal sites with  $d_{Cu}$ (Fig. 10B). Considering the close relationship between particle size and particle morphology, the latter trend may indicate a different functionality of Cu sites located at different positions of the crystal structure, roughly mirroring the density of planar sites with relative particle sizes [23,32,33,61]. However, according to the direct relationship between  $T_{o,red}$  and ZnO loading (Fig. 8B), a modification in the electronic properties of smaller Cu particles could also produce a stronger bonding of oxygen-containing intermediates (e.g., formate, water, hydroxyls), resulting in low TOF values [23,32,33,61,63]. The possibility that high ZnO loadings can depress the stabilization of Cu<sup>+</sup> sites in the octahedral cavities of the zirconia carrier [6], perhaps due to a stronger CuO-ZnO interaction, must

Reaction	Stoichiometry	$K_{\rm p}^{\rm a}$							
		453 K	473 K	493 K	513 K	533 K			
1	$CO_2 + 3H_2 \leftrightarrows CH_3OH + H_2O$	1.81E-4	9.60E-5	5.33E-5	3.08E-5	1.84E-5			
2	$CO_2 + H_2 \cong CO + H_2O$	2.72E-3	4.26E-3	6.44E-3	9.41E-3	1.33E-2			
3	$CH_3OH \hookrightarrow CO + 2H_2$	1.50E+1	4.44E+1	1.21E+2	3.05E+2	7.25E+2			

 Table 4

 List of reactions considered for thermodynamic evaluations of catalytic activity data

<sup>a</sup> Equilibrium pressure constant referred to pressure expressed in MPa.

be considered. This could enhance the negative effect of dispersion (>10%) on TOF in the case of a "multisite" reaction path involving Cu<sup>0</sup> and Cu<sup>+</sup> centers for hydrogen and CO<sub>x</sub> adsorption/activation [6,14,23–28,40,55]. In the case of a reaction path involving the adsorption/activation of CO<sub>2</sub> on zirconia carrier [64], progressively increased coverage of the ZrO<sub>2</sub> surface by ZnO could occur to depress the TOF at high Zn/Cu ratios.

#### 4.4. Thermodynamic analysis

A thermodynamic analysis of the reaction stream [65] was carried out to address the kinetics of the various functionalities and the influence of thermodynamics thereon. In particular,  $CO_2$  hydrogenation can be described by a reaction network involving (1) the synthesis of methanol, (2) the reverse water–gas shift (RWGS), and (3) the methanol decomposition equilibriums:

$$CO_2 + 3H_2 \leftrightarrows CH_3OH + H_2O, \tag{1}$$

$$CO_2 + H_2 \hookrightarrow CO + H_2O,$$
 (2)

and

$$CH_3OH \leftrightarrows CO + 2H_2. \tag{3}$$

Here (3) represents a linear combination of (1) and (2), and thus the thermodynamic evaluation depends on the analysis of (1) and (2), although the (3) can shed light on the  $CO/CH_3OH$ distribution [e.g.,  $K_3 = \{[(P_{CO}) \times (P_{H_2})^2]/(P_{CH_3OH})\}]$ . Substituting the  $P_x$  values (from conversion-selectivity data) into the expression of the equilibrium constants, we obtained experimental  $K_{exp}$  values for the above reactions. Then the ratio ( $\beta$ ) between  $K_{exp}$  and the corresponding value of the equilibrium constant  $K_{eq}$  (Table 4) represents the distance from equilibrium as a measure of the relative kinetics of forward and reverse functionalities. The values of the various  $\beta_x$  at various temperatures at 1.0 (A) and 3.0 MPa (B) are shown in Fig. 11. Such data confirm that at the highest GHSV, all reactions below 473 K proceed under a prevailing kinetic regime. Moreover, although the trend of increasing  $\beta_1$  and  $\beta_2$  indicates a parallel reaction network, a steeper increase in  $\beta_1$  leads to a steady decrease in  $\beta_3$  at all pressures; that is, a  $\beta_3$  value larger than that recorded at higher pressure (Fig. 11B) indicates that the Cu–ZnO/ZrO<sub>2</sub> system has a specific functionality for the hydrogenation of CO<sub>2</sub> (reaction (1)) rather than that of CO (reaction (3)). But although  $\beta_2$  values are affected only slightly (if at all) by a rise in pressure (according to the negligible volume variation of the RWGS reaction), the lower  $\beta_1$  values at 3.0 MPa indicate a decrease in the relative rate of methanol formation. This finding proves



Fig. 11. Thermodynamic analysis of the reaction stream. Effect of temperature on the  $\beta_x$  values (e.g.,  $\beta = K_{exp}/K_{eq}$ ) of the reactions listed in Table 4 at 1.0 (A) and 3.0 MPa (B). For reference, the average experimental values of water vapor and hydrogen pressure are also shown.

that the rate of the synthesis reaction does not increase with the potential of the gas phase, due to the lower dependence of reaction kinetics on pressure. This is in agreement with the fact that the RDS is the surface decomposition of the formate intermediate and/or the abstraction of oxygen derived from its decomposition [23,33,63]. Accordingly, the RDS would proceed at a lower rate at higher surface coverage (higher  $P_{\rm R}$ ) and on low-index sites of small Cu particles [23,32,33,63]. Moreover, such data also demonstrate the "negative" role of water [see reactions (1) and (2)] on the methanol synthesis rate. Favoring water desorption, a temperature increase and/or pressure decrease mainly enhance(s) the rate of CH<sub>3</sub>OH formation, despite the rise in  $P_{\text{H}_2\text{O}}$  (Fig. 11). Then a much stronger chemical affinity of alumina carrier for water, enabling more extensive wetting of the catalyst surface, should account for the poorer performance of the reference Cu(4)Zn(4)/Al<sub>2</sub>O<sub>3</sub>(6) catalyst in the title reaction (Figs. 6 and 7).

#### 5. Conclusions

The activity-selectivity pattern of the Cu–ZnO/ZrO<sub>2</sub> system in the hydrogenation of  $CO_2$  to methanol has been explored, with evaluation of kinetic and thermodynamic factors affecting catalytic functionality. The main findings of this work can be summarized as follows:

- A new method for preparing Cu–ZnO/ZrO<sub>2</sub> catalysts, based on reverse coprecipitation under ultrasound irradiation, provides a significant improvement in the total surface exposure as well as in the dispersion and surface area of the active metal phase.
- Basic relationships among surface area, dispersion, and catalyst reducibility point to a strong promoting effect of ZnO on catalyst texture.
- Marked changes in TOF with metal dispersion indicate the structurally sensitive character of the title reaction.
- Thermodynamic analysis of the reaction stream demonstrates the prevailing functionality of the title system for methanol formation via CO<sub>2</sub> hydrogenation.
- The negative effect of water on the rate of methanol formation accounts for the poorer catalytic performance of the reference Cu–ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst in the title reaction.

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