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Subsolidus of the MO– Cr_2O_3 – V_2O_5 systems, where M = Ni, Mg

I. Rychlowska-Himmel, M. Bosacka*

Department of Inorganic and Analytical Chemistry, Szczecin University of Technology, Al. Piastów 42, 71-065 Szczecin, Poland

Abstract

Phase relations in the system: MO– Cr_2O_3 – V_2O_5 , where M = Ni and Mg, were determined up to the solidus lines over the whole components concentration range. On the basis of this, a division of both systems into subsidiary subsystems was performed. The melting temperatures of individual areas were also established. \bigcirc 2007 Elsevier Ltd. All rights reserved.

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1. Introduction

The development of industry poses a considerable threat. Therefore, increasingly, all sorts of enterprises aiming at minimizing the negative consequences of industrial activity are undertaken. Owing to the fact that norms permitting the values of harmful HCl, NO_x molecules and others are being tightened, one can expect much stricter boundary values of exhaust gas emissions. Therefore, their effective purification, thanks to DENOX filters and catalysts, will become highly necessary. In the years 1970-1980, the bloc d metal oxides, implemented as catalysts removing NO₂, were found to be highly selective [1]; thus, the research on further improvement of the catalysts' selectivity is far flung. The oxide multicomponent systems are the area of search for the catalysts characterized by high selectivity and activity. For many years, the vanadates of bivalent metals [2] have been known owing to their interesting properties. Thoroughly conducted studies have revealed that the catalytic characteristics are connected with the presence of isolated tetrahedra VO_4 in vanadates'(V) molecules [2].

During the works conducted on $M_2V_2O_7$ reactivity in relation to CrVO₄, where M = Ni, Mg, Zn, it was demonstrated that, in the solid phase, these compounds react with forming a new phase of the general formula $M_2CrV_3O_{11}$ [3–5]. The $M_2CrV_3O_{11}$ compounds, where M = Ni, Mg crystallize in the triclinic system and melt

congruently at the temperatures: $Ni_2CrV_3O_{11}-940\pm5$ °C [5], $Mg_2CrV_3O_{11}-900\pm5$ °C [3].

Until today, phase relations corresponding to the solidus line, settling in three intersections of the ternary NiO- $Cr_2O_3-V_2O_5$, i.e. $NiV_2O_6-NiCr_2O_4$, $Ni_2V_2O_7-CrVO_4$ and $Ni_3V_2O_8$ -NiCr₂O₄ system [4,5] have been examined. The results of these investigations made it possible to draw a few lines of the division of the triangle of the ternary NiO-Cr₂O₃-V₂O₅ system concentrations (Fig. 1a) [4,5]. This figure implies that the NiV₂O₆—NiCr₂O₄ system is the actual bivalent system up to the 25 mol% NiCr₂O₄ content only. Above the content of 25 mol% NiCr₂O₄, the NiV₂O₆-NiCr₂O₄ system constitutes the cross-section of the NiO-Cr₂O₃-V₂O₅, going through two subsidiary subsystems: Ni₂CrV₄O₁₁-Ni₃V₂O₈-Cr₂O₃ and Ni₃V₂O₈-NiCr₂O₄-Cr₂O₃. The investigation into the Ni₂V₂O₇-CrVO₄ system demonstrated that it is the real binary system where the Ni₂CrV₃O₁₁ compound is formed.

The studies on the three intersections, $MgV_2O_6-MgCr_2O_4$, $Mg_2V_2O_7-CrVO_4$ and $Mg_3V_2O_8$, [3] allowed the determination of the partial division of the components concentration triangle of the MgO-V_2O_5-Cr_2O_3 system into subsidiary subsystems (Fig. 1b.) The figure implies that the MgV_2O_6-MgCr_2O_4 system is not the real binary one. In the samples containing up to 50.00% mol MgV_2O_6, $Mg_2V_2O_7$, Cr_2O_3 and $MgCr_2O_4$ coexist at equilibrium, while within the concentration range from 50.00 up to 75.00% mol MgV_2O_6 the products of Mg_2CrV_3O_{11}, $Mg_2V_2O_7$ and Cr_2O_3 reactions coexist at equilibrium, whereas above 75.00% mol MgV_2O_6: MgCrV_3O_{11} and

^{*}Corresponding author.

E-mail address: bossm@ps.pl (M. Bosacka).

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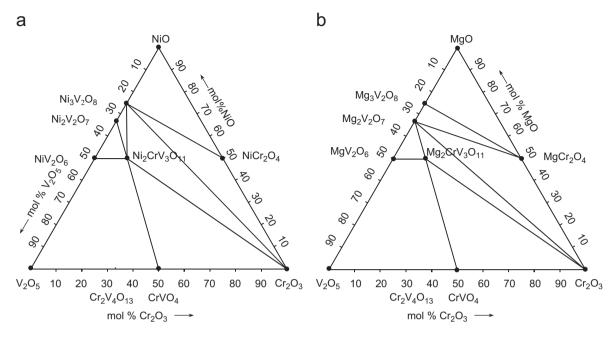


Fig. 1. Preliminary division of the investigated ternary systems into subsidiary subsystems: a-NiO-V₂O₅-Cr₂O₃, b-MgO-V₂O₅-Cr₂O₃.

 MgV_2O_6 [3]. However, the $Mg_2V_2O_7$ -CrVO₄ is the real binary system where the $Mg_2CrV_3O_{11}$ compound is formed [3]. Also, the $Mg_3V_2O_8$ -MgCr₂O₄ system is binary, in which the components do not react with one another [4].

The aim of this work was to complete the phase relations determined so far, settling to the solidus line in two ternary systems: $MO-Cr_2O_3-V_2O_5$, where M = Ni, Mg all over their components concentration range. On the basis of this data, a division of these two systems into subsidiary subsystems was carried out. Another objective was to obtain samples, at equilibrium, of the compositions belonging to particular subsidiary subsystems and binary intersections of the investigated ternary systems, and next determining the melting temperatures of both the subsidiary subsystems and the binary intersections.

2. Experimental

The following compounds were used in the investigations:

- V₂O₅, analytically pure, Riedel-de Haën, Germany manufacturer;
- Cr₂O₃, analytically pure, Aldrich, Germany—manufacturer;
- 2NiCO₃ · 3Ni(OH)₂ · H₂O, analytically pure, POCh Gliwice; Poland—manufacturer;
- $3MgCO_3 \cdot Mg(OH)_2 \cdot 3H_2O$, analytically pure, POCh Gliwice, Poland—manufacturer.

Also, MV_2O_6 , $M_2V_2O_7$, $M_3V_2O_8$, MCr_2O_4 , where M = Ni, Mg as well as $CrVO_4$ and $Cr_2V_4O_{13}$ were used as reacting substances in the conducted studies. The

syntheses of the mentioned compounds have been related in works [3,5-8].

Adequate weighed amount of substrates were homogenized by grinding, forming into pellets and heating in air atmosphere in several stages, until the state of equilibrium was obtained. After each heating stage, the samples were homogenized and examined by the X-ray diffraction (XRD) method and later formed into pellets and heated once again. The conditions of heating particular samples, depending on the composition of the initial mixtures, differed by both the heating temperature and the time of heating at a given temperature.

After the final heating stage, all samples and the furnace were slowly cooled down to ambient temperature. Next, they were ground and tests were applied by means of the DTA and XRD methods. The samples were then pelletized again and further heated at the temperature of the last stage of the synthesis within 24 h. Later, they were rapidly cooled down to room temperature and, after grinding, were DTA tested. Their composition was determined with the XRD method. This procedure allowed the establishment of types of phases being generated in the investigated system and also the ranges of their coexistence in the concentration solid state.

The DTA tests were carried out with the help of the F. Paulik—L. Paulik—L. Erdey derivatograph (MOM, Budapest). The samples weighing 1000 mg each were placed in quartz crucibles. All measurements were run in air atmosphere, in the temperature range 293–1273 K, at the samples' heating rate 10 K/min. Some chosen samples were examined by DTA method using an instrument of METLER TOLEDO TGA/SDTA 851. Samples of 5 mg each, measured by DTA method in air, in the temperature

range 1173–1673 K, were placed in platinum crucibles and heated at a rate of 10 K/min.

The phases occurring in the samples were identified on the basis of the results of the XRD investigations (DRON—3 diffractometer, $CoK\alpha$ radiation Fe filter), and the information included in the PDF cards [9] and works [3,5]. When a diffraction pattern was being worked on, a package of computer programs DHN/PDS (Program Packing for Powder Diffraction) was used.

3. Results and discussion

3.1. The NiO- Cr_2O_3 - V_2O_5 system

In order to carry out the studies, 22 samples of compositions exhibited in Table 1 were prepared. Table 1 demonstrates the heating conditions of particular samples and the phases detected in the equilibrium state as well. The information obtained by means of the XRD method, concerning the samples with compositions lying within the area of a polygon characterized by the $CrVO_4$, $Cr_2V_4O_{13}$, V_2O_5 , NiV_2O_6 and $Ni_2CrV_3O_{11}$ compounds (samples 1–5), implies that reaction:

$$2CrVO_{4(s)} + V_2O_{5(s)} = Cr_2V_4O_{13(s)}$$
(1)

does not occur, while other components of the examined polygon react with one another according to the following reaction:

$$V_2O_{5(s)} + Ni_2CrV_3O_{11(s)} = CrVO_{4(s)} + 2NiV_2O_{6(s)}.$$
 (2)

The results of these studies allowed to determine the division of the polygon into two subsidiary subsystems, NiV_2O_6 -NiCrV₃O₁₁-CrVO₄ and NiV_2O_6 -CrVO₄-V₂O₅, and finally state that, in the solidus area of the investigated

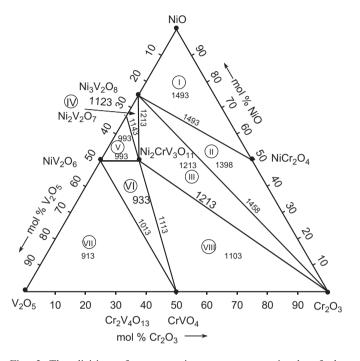


Fig. 2. The division of concentration components triangle of the NiO–V₂O₃–Cr₂O₃ system into subsidiary subsystems and the melting temperatures (K) of the subsidiary subsystems and binary systems.

Table 1

The composition of initial mixtures per system's components, heating stages and phases detected in the samples in the state of equilibrium in binary and ternary systems belonging to the NiO- $Cr_2O_3-V_2O_5$ system

Sample no	Mixtures' composition per system's components [mol%]			Heating conditions $(K \times 24 h)$	Phases detected in the state of equilibrium
	NiO	V ₂ O ₅	Cr ₂ O ₃	_	
1	85.00	10.00	5.00	$863 \rightarrow 923 \rightarrow 973$	CrVO ₄ , NiV ₂ O ₆ , Ni ₂ CrV ₃ O ₁₁
2	60.00	15.00	25.00	$863 \rightarrow 923 \rightarrow 943$	
3	40.00	55.00	5.00	$863 \rightarrow 923 \rightarrow 943 \rightarrow 993$	NiV ₂ O ₆ , CrVO ₄ , V ₂ O ₅
4	10.00	80.00	10.00	$863 \rightarrow (\times)$	2 0, 1, 2 5
5	37.00	54.00	9.00	989 (×4)	NiV ₂ O ₆ , CrVO ₄ , V ₂ O ₅
6	60.00	35.00	5.00	973	$Ni_2V_2O_7$, $Ni_2CrV_3O_{11}$
7	45.00	35.00	20.00	$973 \rightarrow 1073$	$Ni_2CrV_3O_{11}, Cr_2O_3$
8	30.00	27.00	43.00		$Ni_2CrV_3O_{11}$, $CrVO_4$
9	65.00	15.00	20.00	$973 \rightarrow 1073 \rightarrow 1093$	$Ni_3V_2O_8$, $NiCr_2O_4$
10	53.00	17.00	30.00	$973 \rightarrow 1073$	$Ni_3V_2O_8, Cr_2O_3$
11	28.00	22.00	50.00	973	$Ni_2CrV_3O_{11}, Cr_2O_3$
12	60.00	20.00	20.00	$973 \rightarrow 1073$	$Ni_{3}V_{2}O_{8}, Cr_{2}O_{3}$
13	85.00	10.00	5.00	$863 \rightarrow 923 \rightarrow 1073 \rightarrow 1123 \rightarrow 1223$	NiO, Ni ₃ V ₂ O ₈ , NiCr ₂ O ₄
14	70.00	10.00	20.00		
15	60.00	15.00	25.00	$863 \rightarrow 923 \rightarrow 943 \rightarrow 1123$	Ni ₃ V ₂ O ₈ , NiCr ₂ O ₄ , Cr ₂ O ₃
16	35.00	20.00	45.00	$863 \rightarrow 923 \rightarrow 943 \rightarrow 1073 \rightarrow 1093$	Ni ₃ V ₂ O ₈ , Ni ₂ CrV ₃ O ₁₁ , Cr ₂ O ₃
17	15.00	10.00	75.00		
18	33.00	33.00	34.00	$863 \rightarrow 923 \rightarrow 973 \rightarrow 943$	Ni ₂ CrV ₃ O ₁₁ , Cr ₂ O ₃ , CrVO ₄
19	15.00	30.00	55.00		
20	55.00	40.00	5.00	$863 \rightarrow 923 \rightarrow 943 \rightarrow 993$	Ni ₂ V ₂ O ₇ , Ni ₂ CrV ₃ O ₁₁ , NiV ₂ O ₆
21	60.00	30.00	10.00	$973 \rightarrow 1073 \rightarrow 1093$	$Ni_2CrV_3O_{11}, Cr_2O_3, Ni_3V_2O_8$
22	25.00	42.00	33.00		Ni ₂ CrV ₃ O ₁₁ , Cr ₂ O ₃ , CrVO ₄

NiO- $Cr_2O_3-V_2O_5$ system, eight subsidiary subsystems, where three solid phases coexist, can be distinguished (Fig. 2).

$Ni_3V_2O_8$
$-Ni_3V_2O_8$
O_{11} -Ni ₃ V ₂ O ₈
$_{2}V_{2}O_{7}-Ni_{3}V_{2}O_{8}$
V_2O_6 -Ni ₂ V_2O_7
-Ni ₂ CrV ₃ O ₁₁
CrVO ₄
VO_4 – Cr_2O_3

3.2. The $MgO-Cr_2O_3-V_2O_5$ system

Fourteen samples of the compositions presented in Table 2 were prepared. Table 2 also has the heating conditions of particular samples and the phases detected in the equilibrium state. In order to determine the phase relations establishing in the quadrilateral described by the V_2O_5 , MgV_2O_6 , $Mg_2CrV_3O_{11}$ and $CrVO_4$ phases, it was necessary to investigate the mutual reactivity of $Mg_2CrV_3O_{11}$ towards V_2O_5 and $Mg_2CrV_3O_{11}$ towards $Cr_2V_4O_{13}$. Thus, two samples 1 and 2 were subjected to the reactivity investigations (Table 2). After obtaining the samples in the equilibrium state, it was concluded that substrates of sample 1 responded completely, according to equation:

$$Mg_2CrV_3O_{11(s)} + V_2O_{5(s)} = 2 MgV_2O_6 + CrVO_{4(s)},$$
(3)

whereas sample 2 responded in accordance with equation:

$$2Mg_2CrV_3O_{11(s)} + 3V_2O_{5(s)} = 4MgV_2O_{6(s)} + Cr_2V_4O_{13(s)}(4)$$

It can be concluded that the quadrilateral described by the V₂O₅–MgV₂O₆–CrVO₄ Cr₂V₄O₁₃ compounds can be divided into two subsidiary subsystems: V₂O₅–MgV₂O₆–Cr₂V₄O₁₃ and Cr₂V₄O₁₃–MgV₂O₆–CrVO₄.

The investigations conducted resulted in isolating, in the ternary MgO– Cr_2O_3 – V_2O_5 system, nine subsidiary subsystems, where in the equilibrium state there coexist three solid phases. These are the following subsidiary subsystems:

Area I	MgO-MgCr ₂ O ₄ -Mg ₃ V ₂ O ₈
Area II	$Mg_3V_2O_8 - MgCr_2O_4 - Mg_2V_2O_7$
Area III	$Mg_2V_2O_7$ - $MgCr_2O_4$ - Cr_2O_3
Area IV	$Mg_2V_2O_7$ - Cr_2O_3 - $Mg_2CrV_3O_{11}$
Area V	Mg ₂ CrV ₃ O ₁₁ -Cr ₂ O ₃ -CrVO ₄

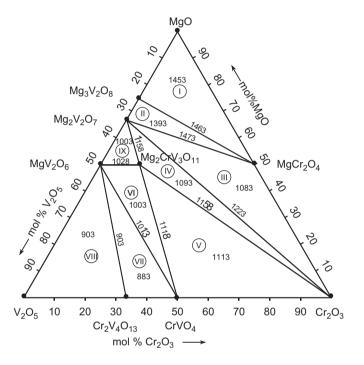


Fig. 3. The division of concentration components triangle of the $MgO-V_2O_5-Cr_2O_3$ system into subsidiary systems and the melting temperatures (K) of subsidiary and binary systems.

Table 2

The composition of initial mixtures per system's components, the heating stages and the phases detected in the samples in the state of equilibrium in binary and ternary systems belonging to the MgO– Cr_2O_3 – V_2O_5 system

Sample no	Mixtures' composition per system's components [mol%]			Heating conditions $(K \times 24 h)$	Phases detected in the state of equilibrium
	MgO	V_2O_5	Cr ₂ O ₃	_	
1	40.00	50.00	10.00	$823 \rightarrow 853 \rightarrow 873$	MgV ₂ O ₆ , CrVO ₄
2	28.57	50.00	21.43	$868 \rightarrow 893 \rightarrow 903$	
3	36.36	54.54	9.09	$868 \rightarrow 868 \rightarrow 893$	MgV_2O_6 , $Cr_2V_4O_{13}$
4	66.66	16.67	16.67	$923 \rightarrow 973 \rightarrow 1023 \rightarrow 1073$	$Mg_3V_2O_8$, $MgCr_2O_4$
5	60.00	20.00	20.00		$Mg_2V_2O_7$, $MgCr_2O_4$
6	50.00	25.00	25.00		$Mg_2V_2O_7, Cr_2O_3$
7	40.00	30.00	30.00		$Mg_2CrV_3O_{11}, Cr_2O_3$
8	80.00	10.00	10.00		MgO, Mg ₃ V ₂ O ₈ , MgCr ₂ O ₄
9	65.00	20.00	15.00		Mg ₃ V ₂ O ₈ , MgCr ₂ O ₄ , Mg ₂ V ₂ O ₇
10	55.00	40.00	5.00	$923 \rightarrow 973 \rightarrow 1023$	Mg ₂ V ₂ O ₇ , Mg ₂ CrV ₃ O ₁₁ , MgV ₂ O ₆
11	40.00	45.00	15.00		MgV_2O_6 , $Mg_2CrV_3O_{11}$, $CrVO_4$
12	20.00	65.00	15.00	$823 \rightarrow 853 \rightarrow 873 \rightarrow 883$	V_2O_5 , MgV ₂ O ₆ , Cr ₂ V ₄ O ₁₃
13	25.00	55.00	20.00		MgV_2O_6 , $CrVO_4$, $Cr_2V_4O_{13}$
14	20.00	30.00	50.00	$823 \rightarrow 873 \rightarrow 923 \rightarrow 948$	$Mg_2CrV_3O_{11}$, Cr_2O_3 , $CrVO_4$

Area VI
$$Mg_2CrV_3O_{11}$$
- $CrVO_4$ - MgV_2O_6

Area VII
 MgV_2O_6 - $CrVO_4$ - $Cr_2V_4O_{11}$

Area VIII
 MgV_2O_6 - $Cr_2V_4O_{13}$ - V_2O_5

Area IX
 MgV_2O_6 - $Mg_2V_2O_7$ - $CrVO_4$

In order to determine the melting temperatures of particular subsidiary subsystems in the ternary MO– $Cr_2O_3-V_2O_5$ systems, where M = Ni, Mg, the melting temperatures of all samples prepared for particular systems of the compositions demonstrated in Tables 1 and 2, were determined. The melting temperatures of phases, being at equilibrium in a given binary or ternary system, were marked out on the basis of the onset temperatures of first endothermic effects, not being the temperatures of polymorphous transformations, recorded on the DTA curves. The conducted measurements, completed with the results of the tests run earlier, facilitated working out complete phase diagrams of the NiO– $Cr_2O_3-V_2O_5$ systems and MgO– $Cr_2O_3-V_2O_5$ in the solidus area (Figs. 2 and 3).

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