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# Aminopropyl-silica-supported Cu nanoparticles: An efficient catalyst for continuous-flow Huisgen azide-alkyne cycloaddition (CuAAC)



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#### ABSTRACT

Cu nanoparticles prepared by metal vapor synthesis (MVS) were immobilized on 3-aminopropyl-functionalized silica at room temperature. HRTEM analysis of the catalyst showed that the copper nanoparticles are present with mean diameters limited in the range 1.0–4.5 nm. TPR analysis was performed in order to study the oxidation state of the supported copper nanoparticles. The supported catalyst was used both in batch and in a packed-bed reactor for continuous-flow CuAAC reaction. The activation of the copper catalyst by reduction using phenyl hydrazine in continuous-flow conditions was demonstrated. Along with the high catalytic activity (productivity up to 1689 mol/mol), the catalyst can be used several times with negligible Cu leaching in the product (<9 ppm), less than allowed Cu contaminant in pharmaceuticals. The applicability of packed-bed flow reactor was showed by sequentially converting different substrates in their corresponding products using same column.

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#### 1. Introduction

The regioselective Cu(I) catalyzed 1,3-dipolar azide-alkyne cycloaddition leading to 1,4-disubstituted-1,2,3-triazoles (CuAAC) was independently introduced by the groups of Meldal and Sharpless [1-3]. Since then, the broad applicability, ease reliability, and high efficiency of this reaction stimulated an increasing interest for a wide range of synthetic applications, from drug discovery to material science and chemical biology [4-12]. Different copper sources have been described for the CuAAC, including simple halide salts and coordination complexes in homogeneous or heterogeneous form [13-22]. From the last decade, nanostructured Cu systems are being explored in both homogeneous and heterogeneous form in CuAAC reactions [13,14,23-30]. The combination of supported Cu-based catalysts and flow reactor technologies represents a step forward in terms of reliability, time, safety, and costs over traditional batch reaction conditions. Recently, considerable efforts in this direction have been devoted to the preparation of innovative Cu-based catalysts by using different strategies to perform CuAAC in flow [31–38]. However, the development of highly recyclable heterogeneous systems with a copper contamination content into the final product at the acceptable levels still remains a challenge [35].

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Here we report the preparation of Cu nanoparticles supported on 3-aminopropyl-functionalized silica (APSiO<sub>2</sub>) by metal vapor synthesis (MVS) technique and their use as catalyst both in batch and in continuous-flow Huisgen azide-alkyne cycloaddition (CuAAC). Supported Cu catalyst showed remarkable activity and stability in continuous-flow CuAAC with a very low Cu leaching in the product. In addition, the activation and regeneration of the catalyst by flowing phenyl hydrazine as a reducing agent for copper were demonstrated. In order to better understand the morphology and the active phase of the supported copper nanoparticles, high-resolution electron microscopy and temperature-programmed reduction (TPR) analysis, both in the pristine state and after use in catalysis, were performed.

#### 2. Experimental

#### 2.1. General

All the reactions involving sensitive compounds were carried out under dry argon by using conventional Schlenk technique. All anhydrous solvents were either purchased in Sure/Seal<sup>TM</sup> bottles or dried by standard procedure. Cu shots, 2–8 mm, 99.999% trace metals basis, were purchased from Strem Chemicals. Acetone (Aldrich product) was dried over molecular sieves and stored under dry argon. 3-Aminopropyl-functionalized silica gel (40–63  $\mu$ m, extent of labeling:  $\sim$ 1 mmol/g NH<sub>2</sub>) was purchased from

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Silicycle. If not noted otherwise, the other compounds were used as received. TLC analyses were carried out with Macherey-Nagel ALOX-25 UV254 plates (0.25 mm) and chromatography purifications with Merck 9385 flash grade silica gel (230-400 mesh). Unless noted otherwise, <sup>1</sup>H and <sup>13</sup>C NMR spectra were recorded as CDCl<sub>3</sub> solutions on a Varian INOVA-600 spectrometer operating at 600 MHz and 150 MHz for <sup>1</sup>H and <sup>13</sup>C, respectively. Chemical shifts are reported in ppm relative to TMS (<sup>1</sup>H) or to the solvent (13C, CDCl<sub>3</sub> at 77.16 ppm). Data are summarized as follows: chemical shift, multiplicity (s = singlet, d = doublet, t = triplet, q = quartet, m = multiplet, dd = doublet of doublets, ddd = doublet of doublet of doublets, dt = doublet of triplets, td = triplet of doublets and br = broad), coupling constants, and integration. Electrospray mass analyses were carried out in the positive [MS(ESI+)] or negative [MS(ESI-)] ion mode on methanolic solutions, with a Perkin-Elmer-Sciex Api 3000 spectrometer. Inductively Coupled Plasma-Optical Emission Spectrometer (ICP-OES: iCAP 6200 Duo upgrade, Thermo Fischer Scientific). For ICP-OES, a sample (1 mL) of solution was heated over a heating plate in a porcelain crucible in the presence of aqua regia (2 mL) for four times, dissolving the solid residue in 0.5 M aqueous HCl. The limit of detection (lod) calculated for copper was 0.01 ppm. Electron micrographs were obtained with a Zeiss LIBRA 200FE, equipped with: 200 kV FEG, in column second-generation omega filter for energy selective spectroscopy (EELS) and imaging (ESI), HAADF STEM facility, EDS probe for chemical analysis, integrated tomographic HW and SW. Before introduction in the instrument, the samples were ultrasonically dispersed in isopropyl alcohol, and a drop of the suspension was deposited on a holey carbon gold grid (300 mesh). The histograms of the metal particle size distribution for the Cu samples were obtained by counting at least 500 particles onto the micrographs. The mean particle diameter  $(d_m)$ was calculated by using the formula  $d_m = \sum d_i n_i / \sum n_i$ , where  $n_i$  is the number of particles with diameter  $d_i$ . Temperature-programmed reductions (TPR) profiles were recorded with a modified version of the Micromeritics Pulse Chemisorb 2700 apparatus. The catalysts (50 mg) were diluted with quartz, pretreated under Ar at 150 °C, and reduced at 8 °C/min with a 8% H<sub>2</sub>/Ar mixture at 15 mL/min.

### 2.2. Preparation of Cu nanoparticles supported on 3-aminopropyl-silica (Cu/APSiO<sub>2</sub>)

The synthesis of Cu/acetone-solvated metal atoms (SMA) was carried out in a static MVS reactor, similar to those previously described [39,40]. In a typical experiment, copper vapors, generated by resistive heating of an tungsten-alumina crucible filled with ca. 500 mg of copper shots, were co-condensed at liquid nitrogen temperature with acetone (100 mL) in the glass reactor chamber of the MVS apparatus in ca. 2 h ( $P = 5 \times 10^{-4}$  mBar). The reactor chamber was warmed to the melting point of the solid matrix (ca. -80 °C), and the resulting brown solution was siphoned at low temperature in a Schlenk tube and kept in a refrigerator at -40 °C. The content of the copper in SMA was 0.4 mg/mL, as determined by ICP-OES analysis. A portion of 50 mL (20 mg of Cu) was added to a suspension of 3-aminopropyl-functionalized silica support (2 g. previously degassed for three times at 25 °C and kept under dry argon atmosphere) in acetone (20 mL). The mixture was stirred for 12 h at room temperature. The colorless solution was removed, and the light-brown solid, containing 1 wt.% of Cu, was washed 3 times with n-pentane (20 mL) and dried under reduced pressure. The same procedure was used to prepare Cu/APSiO<sub>2</sub> system containing 0.55 wt.% of Cu. The catalysts were stored under dry argon atmosphere by using standard Schlenk techniques.

#### 2.3. CuAAC reaction in batch conditions: general procedure

A 25-mL Schlenk tube fitted with a glass frit and stopcock side arm, was charged under argon with Cu/APSiO<sub>2</sub> (65 mg, 1 wt.% of Cu, 0.01 mmol, 0.02 equiv.) and with dry THF (2 mL), followed by benzyl azide (62.5  $\mu$ L, 0.5 mmol, 1 equiv.) and phenyl acetylene (65.9  $\mu$ L, 0.6 mmol, 1.2 equiv.). The flask was closed under argon and kept stirring at 25 °C, for the time t (Table 1). Then, the mixture was filtered through the enclosed frit, collecting the filtrate and catalyst rinses with THF (2  $\times$  2 mL). For the regeneration, the catalyst was treated with the solution of PhNHNH<sub>2</sub> (34  $\mu$ L, 0.35 mmol) in THF (5 mL) for 15 h at room temperature. Then, catalyst was washed with THF (2  $\times$  5 mL), dried under argon flow, and used in next run.

**Table 1**CuAAC reaction in batch reaction conditions using Cu/APSiO<sub>2</sub> catalyst.

Entry	Catalyst	Time (h)	Conversion (%) <sup>a</sup>	Specific activity ( $\textbf{SA}$ ) $(h^{-1})^b$	Leaching (%) <sup>c</sup>
1	Cu/APSiO <sub>2</sub>	2	38	9.5	0.005
	1.0 wt.%	6	100		
2	Recycled from run 1	2	21	5.25	<li>limit</li>
		6	100		
3	Recycled from run 2	2	9	2.25	0.05
		24	99		
4	Recycled from run 3	24	79	1	0.06
5 <sup>d</sup>	Cu/APSiO <sub>2</sub>	2	70	17.5	1.9
	1.0 wt.%	4	100		
6	Recycled from run 5	2	50	12.5	1.5
		6	100		
7	Recycled from run 6	2	15	3.75	1.3
		4	30		
		12	100		
8	CuI/APSiO <sub>2</sub>	2	71	17.7	16
	1.0 wt.%	6	93		
9	Recycled from run 8	2	22	5.5	14
		6	76		
10 <sup>d</sup>	Recycled from run 9	2	29	7.3	5
		6	66		

Reaction conditions; Cu/APSiO<sub>2</sub> 1.0 wt.% (65 mg, 0.01 mmol of Cu) benzyl azide (0.5 mmol, 1 equiv.), phenyl acetylene (0.6 mmol, 1.2 equiv.), THF (2 mL), T = 25 °C.

<sup>&</sup>lt;sup>a</sup> Determined by <sup>1</sup>H NMR.

<sup>&</sup>lt;sup>b</sup> Calculated as moles of benzyl azide converted/moles of Cu per hour (calculated after 2 h).

<sup>&</sup>lt;sup>c</sup> Determined by ICP-OES, on the basis of the total available copper.

 $<sup>^{\</sup>rm d}$  Catalyst pre-activated using PhNHNH<sub>2</sub> (34  $\mu$ L, 0.35 mmol) in THF (5 mL).

#### 2.4. Control experiments for catalytic activity in solution

Each of two 25-mL Schlenk tubes (A and B) fitted with a medium porosity glass frit and stopcock side arm was charged under argon with  $\text{Cu/APSiO}_2$  (65 mg, 1 wt.% of Cu, 0.01 mmol, 0.02 equiv.). The catalyst in Schlenk-A was pre-activated with PhNHNH2 (9.8  $\mu$ L, 0.1 mmol), washed with THF, and dried as above, while the catalyst in Schlenk-B was used in its pristine form. Each tube was charged with THF (2 mL), benzyl azide (0.5 mmol, 1 equiv.), and phenyl acetylene (0.6 mmol, 1.2 equiv.), sealed under argon, and kept stirring at 25 °C, for 2 h. Then, the mixtures were filtered through the enclosed frit under argon into another Schlenk tube. NMR analysis of small amount of mixture from Schlenk-A and Schlenk-B at this stage showed 50% and 35% conversion, respectively. Keeping reaction mixture at 25 °C under argon for additional 4 h showed only slight increase in conversion of benzyl azide to 1,2,3-triazol product (see Fig. 2S).

#### 2.5. Preparation of Cu/APSiO<sub>2</sub> packed-bed reactor

Packed-bed reactor was prepared in a commercially available PTFE tubing with Luer-lock fitting (Fig. 1S,  $161 \times 1$  mm i.d.). As shown in Fig. 1, glass wool and a piece of smaller PTFE tube (o.d. 1/16'') were used as a frit at the tubing end devoid of the Luer-lock fitting. Catalyst was packed by sucking Cu/APSiO<sub>2</sub> from Schlenk tube with the help of vacuum. In order to keep the catalyst bed in place, glass wool and a short piece of 1/16'' o.d. PTFE tubing were also placed at the other end of the reactor.

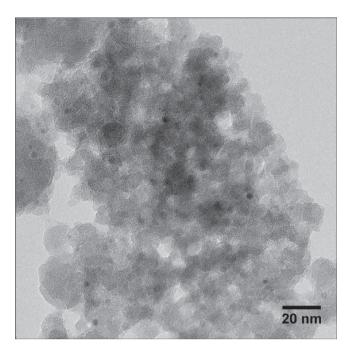
### 2.6. CuAAC reaction under continuous-flow conditions: general procedure

The Luer-lock PTFE tubing packed with Cu/APSiO<sub>2</sub> (190 mg Cu/APSiO<sub>2</sub>, 1 wt.% or 230 mg 0.55 wt.% Cu loading, respectively) was connected to a 5-mL SGE gas-tight syringe and flushed with dry THF for 30 min at 50  $\mu L\,min^{-1}$  flow rate. The CuAAC reaction was then carried out at 25 °C, by flushing the solution of reagents (benzyl azide (1), 3.75 mmol, 1 equiv.; phenyl acetylene (2), 4.5 mmol, 1.2 equiv.; solvent = THF, 15 mL) through the reactor at  $50~\mu L\,min^{-1}$  flow rate. For regeneration, the reactor was flushed with PhNHNH<sub>2</sub> (103  $\mu$ L, 1.05 mmol) in THF (5 mL) at 50  $\mu$ L min<sup>-1</sup> flow rate. For the runs carried out in presence of reducing agent, PhNHNH<sub>2</sub> (30 μL, 0.30 mmol) was used in the feed mixture. The catalyst was washed with anhydrous THF (2 × 5 mL) after each run as well as after regeneration. The copper content in the crude product was determined at this stage, by ICP-OES analysis of the combined eluates from each run. For purification purposes, the reaction mixture was treated with water (20 mL) and extracted with  $CH_2Cl_2$  (2 × 15 mL). The combined organic layers were dried over Na<sub>2</sub>SO<sub>4</sub>, the volatiles were removed with a rotary evaporator, and the residue was purified by flash chromatography ( $SiO_2$ , nhexane:AcOEt = 3:1).

#### 3. Results and discussion

## 3.1. Preparation and characterization of Cu nanoparticles supported on 3-aminopropyl-functionalized silica (Cu/APSiO<sub>2</sub>)

Cu nanoparticles were prepared by MVS technique [41,42] and supported on APSiO<sub>2</sub> (see Section 2.2). The MVS approach allowed to deposit very small copper nanoparticles (<5 nm) at room temperature directly in its reduced form, so that, calcination and activation processes, which can eventually modify the structure of hybrid organic/inorganic support, were avoided. The choice of amino-functionalized silica was dictated by the ability of primary



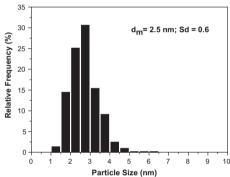


Fig. 1. Transmission electron microscopy (TEM) image of a freshly prepared Cu/  $\mbox{\sc APSiO}_2$  sample.

alkyl amines to stabilize Cu nanoparticles [43], and the strong tendency of amino-functionalized silica to bind copper species [44–48].

Transmission electron microscopy (TEM) analysis was performed in order to study the metal particle size distribution of the Cu/APSiO<sub>2</sub> samples. Copper nanoparticles turned out to be highly dispersed on the functionalized silica support and mainly present in a narrow size distribution (ranging 1.0–4.5 nm), with an average diameter close to 2.5 nm (Fig. 1). A very low amount of larger particles ranging from 10 to 15 nm in diameter was also detected.

In order to investigate the crystalline phase of starting Cu (0) nanoparticles obtained by MVS approach, high-resolution TEM analysis was performed on the Cu/APSiO<sub>2</sub> catalyst (Fig. 2) [49]. Lattice planes extend to the whole particle without any stacking faults or twins, indicating their single-crystalline nature. Lattice fringe analysis recorded on larger Cu particles (>10 nm, Fig. 2A) exhibited spots in the FFT pattern at 2.1 Å which are ascribed to the spacing of (111) planes of the face-centered cubic (fcc) structure of metallic Cu [50]. Besides, the FFT pattern of smaller Cu nanoparticles (<5 nm) showed spots at 2.5 Å which can be attributed to the (002) lattice spacing of Cu(II) oxide (Fig. 2B) [51]. Moreover, high-resolution micrographs revealed an amorphous phase bonded to the surface of the Cu particles that can be due to the presence of

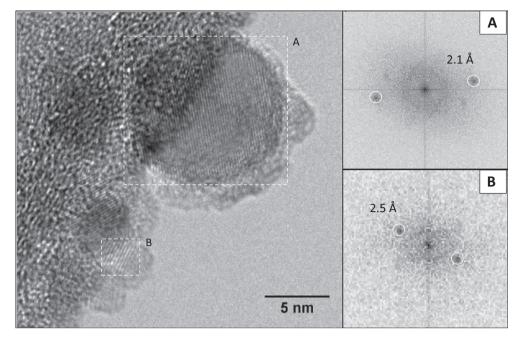


Fig. 2. HRTEM micrograph of Cu nanoparticles and inverted FFT pattern taken from A and B squared areas, respectively.

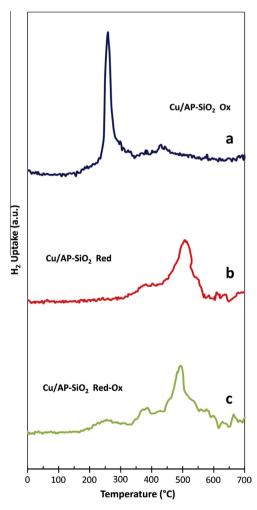
the residual  $APSiO_2$  support. The data showed that the starting small Cu nanoparticles prepared in their reduced form are readily oxidized after exposition in air.

Temperature-programmed reduction (TPR) was carried out in order to get detailed information about the nature, oxidation state, and reducibility of supported Cu catalyst [52]. The analysis consists in a reductive treatment of the catalyst under controlled temperature program and hydrogen concentration conditions. The reducibility of the supported phase strongly depends on the particles dimension, the metal oxidation state, and the interaction with the matrix used as the support. The TPR of the Cu/APSiO<sub>2</sub> (Fig. 3a) shows a narrow peak with a maximum at 260 °C, which further confirms the presence of very uniform and small particles that are easy reduce under  $H_2$  flow. The reduction temperature is in agreement with the presence of a Cu(II) oxide, as detected by HRTEM [52].

#### 3.2. Catalytic behavior of Cu/APSiO<sub>2</sub> catalyst

In order to evaluate the catalytic efficiency of the supported Cu nanoparticles, the Cu/APSiO<sub>2</sub> system was first employed under batch reaction conditions (Table 1).

We were pleased to find that full conversion of 1 to the 1,2,3-triazole product 3 was achieved in 6 h by using 2 mol.% of Cu catalyst at room temperature. Remarkably, the reaction proceeded in the absence of any basic additive, suggesting that the primary amine groups on the support could play a dual role, as a stabilizer of Cu particles and as a heterogeneous base. The recovered catalyst could be reused in next 3 runs (entries 1-4, Table 1), albeit at the expense of a steady decrease of the specific activity (SA). The ICP-OES analysis showed a very low amount of Cu species leached in the reaction mixture after each catalytic run (<0.05 wt.% of the total available Cu content, corresponding to 0.39 ppm in solution, entries 1-4, Table 1). Given the negligible metal leaching, oxidation of the Cu particles to less active Cu(II) oxide, as also evidenced by HRTEM and TPR analysis, was therefore considered as the most likely explanation of the loss of catalytic activity on recycling [53].



**Fig. 3.** TPR profiles of Cu/AP-SiO<sub>2</sub>: freshly prepared (blue line), reduced with phenylhydrazine (red line) and air-exposed after the reduction (green line). (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

In order to test this hypothesis, the effect of the treatment of the Cu/APSiO<sub>2</sub> catalyst with phenyl hydrazine (PhNHNH<sub>2</sub>) was evaluated. The use of this reducing agent for selectively obtaining Cu(I) species has been reported in different reactions [54,55]. Interestingly, the SA of the PhNHNH2-treated system was almost doubled with respect to the non-activated catalyst (entry 5 vs. entry 1). TPR analysis of the PhNHNH<sub>2</sub>-treated system (Fig. 3b) exhibited a shift of the reduction peak at higher temperature (500 °C) and a shoulder at around 400 °C. This change in the TPR profile confirms that a new copper phase appears after the treatment with phenyl hydrazine, which can be attributed to formation of Cu<sub>2</sub>O phase [56]. Recycling this catalyst showed similar decreasing trend of activity as that of first set of reaction; nonetheless, pre-activation allowed a more effective use of supported catalyst, as higher SA values were noticed (entries 5-7 vs. entries 1-4). These results agree with the previously reported evidences on the role of Cu(I) as catalytically active species in CuAAC reaction. Indeed, as demonstrated by theoretical and experimental studies, the reaction mechanism involves the initial formation of Cu(I) acetylide species followed by the azide attack [41,57,3,58-67]. On the other hand, the ICP-OES data showed comparatively larger amounts of copper species released in the reaction mixture under these conditions. From the above results, it was clear that PhNHNH<sub>2</sub> is able to reduce the oxidized surface layer of copper particles and keep it in the active state, but at the same time it favors to some extent the release of the metal in the reaction mixture [68]. In order to establish the nature of the catalytic systems, we monitored two test reactions performed in batch conditions with the Cu/APSiO2 system untreated and pre-treated with phenyl hydrazine, respectively (Fig. 2S). After conducting the reaction of phenylacetylene and benzyl azide for 2 h, 1,2,3-triazole was produced in a yield of 35% (untreated Cu/APSiO<sub>2</sub>) and 50% (pre-activated Cu/APSiO<sub>2</sub>), respectively. After that, the catalysts were removed from the reaction vessels, the reaction was stirred for further 4 h at 25 °C, and in absence of the catalysts, a further conversion of less than 5% was observed. The results point out the significant heterogeneous contribution of the copper-based catalyst confirming that the click reaction can occur at the surface of the supported copper particle, as recently reported [69].

The catalytic behavior of MVS-derived Cu catalyst was compared with that of previously reported CuI immobilized on APSiO<sub>2</sub> (CuI/APSiO<sub>2</sub>) [65]. For this purpose, CuI/APSiO<sub>2</sub> catalyst was prepared following the reported procedure [69]. Despite its easy preparation and high **SA** (entry 8), freshly prepared CuI/APSiO<sub>2</sub> turned out to suffer from a nearly one order of magnitude larger metal leaching (16% of total Cu content) than the MVS catalyst. Not surprisingly, this led to a significant drop of catalytic activity upon recycling CuI/APSiO<sub>2</sub> (entry 9) and the inability to recover the initial performance by treatment with PhNHNH<sub>2</sub> (entry 10).

With these promising results in hand, we set out to evaluate the performance of this system under continuous-flow conditions. The flow experiments were carried out using a home-made reactor packed with Cu/APSiO<sub>2</sub> (see Supporting Information). Given the findings in the batch runs, the catalyst was subjected to pre-activation in flow, by flushing the reactor with PhNHNH<sub>2</sub> in THF. After brief initial optimization of flow rate, 3.75 mmol of 1 was quantitatively converted in 5 h into the corresponding 1,2,3-triazole product 3 at 50  $\mu$ L min<sup>-1</sup> (Table 2, entry 1).

The same flow reactor was employed next in two additional runs, without any intermediate regeneration of the catalyst (entries 2–3). Even though the recorded *SA* values were higher than obtained in batch (Table 2, entries 1–3 vs. Table 1, entries 5–7), a steady reduction of the conversion was noted in the course of the successive cycles. Reasoning that the activity decrease could be due to the partial oxidation of the catalyst by adventitious oxygen, TPR analysis was performed on a sample of Cu/APSiO<sub>2</sub>

**Table 2**CuAAC reaction in continuous-flow reaction conditions using Cu/APSiO<sub>2</sub> catalyst.

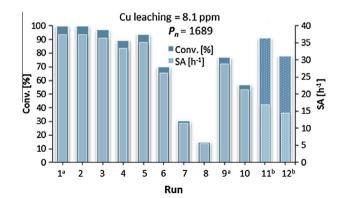
Entry	Conversion (%) <sup>a</sup>	Specific activity ( $SA$ ) $(h^{-1})^b$	Leaching (%) <sup>c</sup>
1 <sup>d</sup>	99	24.7	<0.01
2	73	18.3	0.2
3	50	12.5	0.3
$4^{d}$	85	21.2	2.7
5 <sup>e</sup>	100	25.0	1.2
6 <sup>e</sup>	94	23.5	5.2
7 <sup>e</sup>	79	19.7	4.8

Reaction conditions: Cu/APSiO<sub>2</sub> 1.0 wt.% (190 mg, 0.03 mmol of Cu), benzyl azide (3.75 mmol, 1 equiv.), phenyl acetylene (4.5 mmol, 1.2 equiv.), THF (15 mL), flow rate =  $50 \,\mu L \, min^{-1}$ ,  $T = 25 \,^{\circ}C$ ,  $t = 5 \, h$ .

- <sup>a</sup> Determined by <sup>1</sup>H NMR.
- <sup>b</sup> Calculated as moles of benzyl azide converted/moles of Cu per hour (calculated after 2 h).
  - <sup>c</sup> Determined by ICP-OES, on the basis of the total available copper.
  - $^{
    m d}$  Catalyst pre-activated using PhNHNH<sub>2</sub> (103  $\mu$ L, 1.05 mmol) in THF (5 mL).
- $^{\rm e}$  PhNHNH<sub>2</sub> (30  $\mu$ L, 0.30 mmol) was added to the reaction feed.

pre-reduced with PhNHNH<sub>2</sub> and then exposed to air (Fig. 3c). Interestingly, the reduction profile of the air-exposed sample showed a relatively small peak with a maximum at around 250 °C, which can be traced back to the formation of the CuO phase. At the same time, the broad peak with shoulder at higher temperature, related to Cu<sub>2</sub>O nanoparticles, was still present, thus showing that only partial reoxidation of the metal occurs when the phenylhydrazinetreated catalyst is handled in air in the dry state. Moreover, comparatively lower copper leaching was observed in continuous-flow runs than in batch. This could be explained by the reduced mechanical stress on the catalyst with respect to the stirred-flask conditions where, indeed, some grinding of silica particles by magnetic stirring was noticed. Furthermore, the catalytic activity was increased significantly if the flow reactor was regenerated before next use by flushing with PhNHNH<sub>2</sub> (1.05 mmol, 0.21 M in THF) (entry 4) and restored completely when the reducing agent (0.3 mmol, 0.02 M) was included in the reaction feed (entry 5). With this latter modification, the catalyst provided rather constant **SA** values in subsequent runs (entries 6 and 7) albeit, as already noticed in batch, at the expense of some increase in the copper leaching (entries 4–7 vs. 1–3).

Overall the packed-bed reactor could be used effectively for seven times (entries 1–7), thus obtaining higher total productivity of catalyst ( $P_n$  = 727) [70] than in batch ( $P_n$  = 200 and 150 for the two sets of reactions, Table 1 entries 1–4 and 5–7, respectively). The amount of copper present in the combined products from all the flow reactions (53 ppm) was much less than reported for other



**Fig. 4.** Continuous-flow click reaction between phenyl acetylene and benzyl azide using Cu/APSiO<sub>2</sub> (0.55 wt.%). Reaction conditions for each run: Cu/APSiO<sub>2</sub> 0.55 wt.% (230 mg, 0.02 mmol of Cu), benzylazide (3.75 mmol), phenylacetylene (4.5 mmol), THF (15 mL), PhNHNH2 (9.8  $\mu$ L, 0.1 mmol), flow rate = 50  $\mu$ L min<sup>-1</sup>, T = 25 °C. (a) Pre-activated with PhNHNH2 (69  $\mu$ L, 0.7 mmol in 5 mL THF); (b) 25  $\mu$ L min<sup>-1</sup> flow rate, pre-activated and reaction run in presence of PhNHNH2 (69  $\mu$ L, 0.7 mmol) added to the feed.

**Table 3** Substrate scope in continuous-flow CuAAC reaction using Cu/APSiO<sub>2</sub> catalyst.

Substrate 1	Substrate 2	Product	Conversion (%) <sup>a</sup>
$N_3$		N=N	99
MeO N <sub>3</sub>		MeO N=N	99
$O_2N$		$O_2N$	99
$N_3$		N N N N N N N N N N N N N N N N N N N	99

Reaction conditions: Cu/APSiO<sub>2</sub>, 0.55 wt.% (223 mg, 0.019 mmol of Cu), benzyl azide (2.5 mmol, 1 equiv.), phenyl acetylene (3.0 mmol, 1.2 equiv.), THF (10 mL), PhNHNH<sub>2</sub> (9  $\mu$ L, 0.095 mmol), flow rate = 50  $\mu$ L min<sup>-1</sup>, T = 25 °C. Before each run, the catalyst was activated with PhNHNH<sub>2</sub> (66  $\mu$ L, 0.67 mmol in 5 mL THF).

supported Cu systems [31–38]. Nonetheless, the leaching level in these initial experiments was still above the generally accepted Cu contamination in pharmaceuticals (15 mg kg<sup>-1</sup>) [35]. In order to solve this problem, we speculated that lowering the amount of Cu on APSiO<sub>2</sub> could increase the stability of supported nanoparticles, due to the availability of comparatively more amino groups on the silica surface. Moreover, decreasing the reducing agent to the minimum amount required for keeping the catalyst in the active form could help to limit the metal dissolution.

To investigate the assumptions made above, a new batch of catalyst with lower Cu loading (0.55 wt.%) was prepared and second set of flow experiments was carried out (Fig. 4). Despite the comparatively lower amount of Cu immobilized in the device, the reactor was still able to quantitatively convert 1 to the 1,2,3-triazole product **3** at 50 μL min<sup>-1</sup> flow rate (run 1, Fig. 2). After the initial activation, a minute amount of PhNHNH<sub>2</sub> in the feed (0.10 mmol, 0.007 M) was able to keep the catalyst active for the next five runs. Afterward, a clear decrease in activity was noticed from run 6 to 8. Regeneration at this stage with PhNHNH<sub>2</sub> in THF permitted restoring the activity of catalyst to a large extent (runs 9 and 10), while almost the initial conversion could be attained by decreasing the flow rate to  $25\,\mu L\,min^{-1}$  and adding a larger amount of reducing agent (0.05 M) to the feed (runs 11 and 12). Comparison of the results of Fig. 4 with those obtained in the initial set of flow experiments (Table 1, entries 11-17) confirmed the anticipated advantages of using Cu/APSiO<sub>2</sub> (0.55 wt.%) instead of Cu/APSiO<sub>2</sub> (1.0 wt.%). Indeed, with proper modification of the reaction conditions, the former could be used very effectively for 12 times and provided notably higher and stable SA values than the latter. As a consequence, the total productivity obtained with Cu/APSiO<sub>2</sub> (0.55 wt.%) in flow ( $P_n = 1689$ ) was more than two times larger of that achieved with Cu/APSiO<sub>2</sub> (1.0 wt.%) under comparable conditions (vide supra) [71]. Most importantly, ICP-OES data for all the flow reactions showed now very low copper leaching in the reaction mixture (8.1 ppm) [72], which is below the maximum allowed limit for pharmaceuticals and demonstrates the unique features of the nanostructured MVS system described in this work with respect to bulk copper catalysts and devices reported to date [31,34-37].

In order to further demonstrate the applicability of our packed-bed flow reactor, the substrate scope was briefly examined (Table 3). A new device containing  $\text{Cu/APSiO}_2$  (0.55 wt.%) was prepared and employed to sequentially promote in continuo the CuAAC reaction of different substituted azides (1a-d) with phenylacetylene. Functional groups on the azide partner seem not to have a decisive effect on the catalytic activity, as benzyl azides with substituents at meta

and *para* position reacted to give the corresponding 1,2,3-triazole products **3a–d** in essentially quantitative yields. Remarkably, the same packed-bed reactor was used for running CuAAC reaction of the four different substrates, by intermediate washing of catalyst bed with THF and treatment with PhNHNH<sub>2</sub>.

#### 4. Conclusions

New 3-aminopropylsilica supported copper catalysts have been developed, which showed remarkable activity and recyclability in continuous-flow CuAAC. With respect to other immobilized Cu catalysts reported to date, including nanostructured ones [35,36,73-78], these novel systems displayed improved performances especially for what it concerns the low metal leaching and extended reuse under optimized conditions. Arguably, these unique properties can be traced back to the use of MVS-derived Cu nanoparticles and the possibility to prepare, by this technique, supported metal catalyst containing particles in the low nanometer range and without contamination by foreign substances. Moreover, the results confirmed that the 3-aminopropylsilica support is able to stabilize Cu particles without compromising the catalytic activity. As a matter of facts, the flow reactions positively compete with the batch ones, thus affording larger quantity of product (i.e., greater  $P_n$  of catalyst) and simplified separation procedures. Careful tailoring of reaction conditions and Cu loading on APSiO<sub>2</sub> allowed exploiting the supported catalyst more effectively and for longer time and also to diminish the metal leaching in the reaction medium. In this context, the feasibility of extending the catalyst's lifetime by reduction in continuo of phenylhydrazine was also demonstrated for the first time. The versatility of the flow system was also proved by sequentially converting different substrates to 1,2,3-triazole products with the same column.

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#### Appendix A. Supplementary material

Supplementary data associated with this article can be found, in the online version, at http://dx.doi.org/10.1016/j.jcat.2015.01.014.

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