Low Temperature Silicon Nitride and Silicon Dioxide Film Processing by Inductively Coupled Plasma Chemical Vapor Deposition

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High-density plasma technology is becoming increasingly attractive for the deposition of dielectric films such as silicon nitride and silicon dioxide. In particular, inductively coupled plasma chemical vapor deposition (ICPCVD) offers a great advantage for low-temperature processing over plasma-enhanced chemical vapor deposition (PECVD) for a range of devices including compound semiconductors and magnetic heads. In this paper, the development of low temperature ($< 200^{\circ}$ C) silicon nitride and silicon dioxide films utilizing ICP technology is discussed. The material properties of these films have been investigated as a function of ICP source power, radio-frequency chuck power, chamber pressure, gas chemistry, and temperature. The ICPCVD films are compared to PECVD films in terms of wet etch rate, stress, and other film characteristics. Two different gas chemistries, SiH₄/N₂/Ar and SiH₄/NH₃/He, were explored for the deposition of ICPVD silicon nitride. The ICPCVD silicon dioxide films were prepared from SiH₄/O₂/Ar. The wet etch rates of both silicon nitride and silicon dioxide films are significantly lower than films prepared by conventional PECVD. This implies that ICPCVD films prepared at these low temperatures are of higher quality. The advanced ICPCVD technology can also be used for efficient void-free filling of high aspect ratio (3:1) sub-micrometer trenches. (© 2000 The Electrochemical Society. S0013-4651(99)06-103-X. All rights reserved.

Manuscript submitted June 21, 1999; revised manuscript received December 15, 1999.

There is a growing interest in high-density plasma processing in both the semiconductor and the magnetic thin film head industry.¹⁻⁷ In particular, much research has been conducted on dry etching with inductively coupled plasma (ICP) sources because they provides advanced processes for pattern transfer.⁸⁻¹⁰ A great deal of research has been reported for dielectric film deposition using remote or high-den-sity plasmas.¹¹⁻¹⁴ However, relatively little work has been done on deposition technology for dielectric materials using ICP.^{15,16} Using an ICP source, we explored high-density plasma (> 10^{11} cm⁻³) chemical vapor deposition (HDPCVD) of SiN_x and SiO_2 . In comparing HDPCVD technology with conventional plasma-enhanced chemical vapor deposition (PECVD), some potential advantages are lower hydrogen content films, higher quality films at lower process temperatures (<200°C), void-free gap filling of high aspect ratio features, and self-planarization. Low temperature SiN_x film deposition of low hydrogen content by HDPCVD is of special interest for cap and capacitor layers in III-V semiconductor devices.¹⁷⁻²¹ Due to the relatively low dissociation efficiency of N2, typical process recipes for SiN_x deposition by PECVD use NH₃ as the source of nitrogen. Therefore, some portion of hydrogen incorporation from NH₃ in deposited SiN_x films is inevitable. However, HDPCVD technology enables us to deposit SiN_r with a NH₃-free recipe because high-density plasma sources have typically one order of magnitude higher ion dissociation efficiency (*i.e.*, $\sim 0.1\%$ for PECVD and $\sim 1\%$ for HDPCVD).

Some advantages of an ICP source over other types of high-density sources include easier scale up, advanced automatic tuning for the source, and lower cost of ownership. In addition, with a hybrid ICP configuration, such as used in this work, it is possible through the addition of radio-frequency (rf) power to the wafer chuck, to control ion flux and ion energy independently. This expands the applications for dielectric film deposition by ICP. For example, gapfilling techniques require simultaneous high ion bombardment by an inert gas such as Ar during deposition to prevent void formation. To achieve high ion bombardment, high ion energy can be induced by controlling the rf power on the wafer chuck in HDPCVD without change to the ion density in the source. In PECVD, that approach is not feasible and alternating sequences of deposition and sputter etch are usually required. This requires extra steps and more process time. For damage sensitive devices, such as the high electron mobility transistor (HEMT), it is essential to use a very low ion energy

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process because ion energy is a major factor causing ion damage to the device.²² With HDPCVD, the ion energy can be reduced to minimize damage to the devices. The process pressures for PECVD and HDPCVD are quite different. More than 500 mTorr is common for PECVD. The pressure range of HDPCVD is 1-30 mTorr. We report on the effect of rf chuck power and pressure for SiN_x films deposited by HDPCVD with an ICP source.

Experimental

Both SiN_x and SiO₂ films were deposited in a Plasma-Therm HDPCVD Versalock system on 4 in. Si wafers. Figure 1 shows a schematic of the ICP chamber configuration. The load module of the system can handle up to about 50 wafers at a time. For the SiN_x deposition, two different gas chemistries, SiH₄/N₂/Ar and SiH₄/ N_{H₃/He, were explored. A gas chemistry of SiH₄/O₂/Ar was used for the SiO₂ film deposition. Electronic mass flow controllers regulated all gas flows. The SiH₄ was fed through a lower gas ring (gas inlet 2). All other gases entered the chamber via a showerhead in the ICP source (gas inlet 1). The process chamber is a hybrid configuration consisting of an ICP source and an rf powered wafer chuck. An oil recirculating heat exchanger connected to the chuck controls the wafer temperature. Helium back-side cooling of the wafer is used for efficient heat transfer. For this work, the ICP source power and chuck temperature.}







Figure 2. (a) Ion density and (b) negatively induced dc bias as a function of rf chuck power in an ICP chamber for Ar plasmas.

ature were fixed at 800 W and 150°C, respectively. We found that lower deposition temperatures lead to poor quality dielectrics with relatively high wet etch rates. The rf chuck power and chamber pressure were varied from 25 to 150 W and 1 to 20 mTorr, respectively.

Langmuir probe measurements of ICP Ar plasmas were used to determine the ion density characteristics of the process chamber. *In situ* optical emission spectroscopy (OES) was also used to characterize the ICP SiH₄/N₂/Ar plasmas.

Deposition rate and uniformity were determined by a NanoSpec model 4150 metrology system. Refractive index measurements were made on a Gaertner model L116D-PC ellipsometer. Film stress



Figure 3. Optical emission spectrum of an ICP $SiH_4/N_2/Ar$ plasma at 800 W ICP, 120 W rf, and 10 mTorr.

measurements were done with a Tencor model P-2 profilometer. A buffered oxide etch (BOE) solution of 7:1 NH_4 : HF was used for the wet-etch rate measurements.

Results and Discussion

ICPCVD plasma characterization.—Figure 2 shows ion density and negatively induced dc bias as a function of ICP source power and rf chuck power for Ar plasmas at a fixed pressure of 10 mTorr. These data were obtained from a design of experiment simulation, which we developed with experimental data obtained on the ICP process chamber. As shown in Fig. 2a, the ion density of the Ar plas-



Figure 4. Detailed optical emission spectra for an ICP $SiH_4/N_2/Ar$ plasma for rf chuck powers of 20 and 120 W. The ICP power and pressure were 800 W ICP and 10 mTorr, respectively.

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Figure 5. SiN_x deposition rate as a function of rf chuck power.

ma can be controlled by ICP source power and is almost independent of rf chuck power. The Ar ion density is about 2×10^{11} cm⁻³ with 800 W ICP power, 20 sccm Ar, 10 mTorr chamber pressure, and 100 W rf chuck power. As illustrated in Fig. 2b, the dc bias on the chuck was a strong function of ICP source power and rf chuck power. The dc bias increased with rf chuck power and decreased with ICP source power.

Silicon nitride: optical emission spectra.—In Fig. 3, a typical optical emission spectrum (OES) is presented for an ICP SiH₄/N₂/Ar plasma. This spectrum was recorded during a SiN_x deposition. All N₂, SiH, H₂, and Ar related peaks were identified. Figure 4 shows more detailed OES data taken at different rf powers. Many N₂ related peaks were detected between 300 and 400 nm. A N₂⁺ peak is also noticed at 391.4 nm. A SiH and two H₂ peaks are observed at 414.2, 486.1, and 656.2 nm, respectively. The peak intensities of both SiH and H₂ increased with increasing rf power.

Silicon nitride: film properties.—Results for SiH₄/N₂/Ar.—In Fig. 5, the dependence of deposition rate on rf chuck power is shown. The deposition rate decreases with increasing rf chuck power. At high rf power, it is expected that more ion bombardment during deposition will occur. High rf power increases the dc bias and consequently the ion energies of the bombarding species, *e.g.*, Ar⁺ and N₂⁺, will increase. This will enhance the sputtering of Si and N reactive neutrals before and during the formation of the SiN_x film. This accounts for the observed reduction in deposition rate with rf power.



Figure 6. Refractive index of ICPCVD SiN_x as a function of rf chuck power.



Figure 7. BOE rate of ICPCVD SiN_x as a function of rf chuck power.

The typical deposition rate was in the range 400-600 Å/min. This is comparable to conventional PECVD using the same precursors at much higher pressures.

Figures 6 and 7 show the variation of refractive index and buffered oxide etch (BOE) rate with rf chuck power. At 25 W rf chuck power, a refractive index of 1.95 was achieved. The combination of decrease of deposition rate and BOE rate, and increase of refractive index with rf chuck power indicates that deposited films become slightly Si-rich (Si fraction increased from 0.51 to 0.57). This was confirmed by Auger electron spectroscopy (AES) measurements.

One possible explanation for the increase of refractive index with rf power is that the dissociation of SiH₄ into reactive neutrals in the SiH₄/N₂/Ar plasma increased relative to that of N₂ with rf chuck power (in other words, ion energy). Another possible explanation is that high rf power brings more Si-related species than N to participate in the film growth. Table I shows the dissociation energy of related diatomic molecules for SiN_x deposition. Note that the N–N bond has a much higher bond strength (945.33 kJ/mol) than that of Si–H (≤299.2 kJ/mol). Dissociation of N₂ requires more energy than that of SiH₄. This data suggests that more SiH₄ species are brought to the substrate than N₂ with increase of rf chuck power.

It is worthwhile commenting further on the BOE data presented in Fig. 7. Considering the low deposition temperature of 150°C, the typical BOE rate of 1000 Å/min is very low. At 150°C, the BOE rate of PECVD SiN_x is greater than 5,000 Å/min. This implies that the ICPCVD SiN_x films are denser and contain less hydrogen.²⁵

As indicated in Fig. 8, the stress of all ICPCVD SiN_x films prepared from SiH₄/N₂/Ar was compressive. At 25 W rf chuck power, the film stress was as high as 900 MPa. Raising the rf chuck power lowers the film stress. A stress of 300 MPa is achieved at 120 W. Film stress of less than 500 MPa is acceptable for many applications. We speculate that incorporated hydrogen relieves the stress in the SiN_x film, although the correlation with rf chuck power is not fully understood. The typical H content in our SiN_x films ranged from 15-20 atom %. compared to 25-30 atom % for PECVD films deposited at the same temperatures. In PECVD, the film stress increases with rf power regardless of whether it is compressive or tensile. This is diametrically opposite to the current observations with ICPCVD.

Table I. Dissociation	energies of	diatomic	molecules.

Bond	Dissociation energy at room temperature (kJ/mol)
Si_H	<299.2
N–H	≤339
N–N	945.33
H–H	435.99

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Figure 8. Compressive stress of ICPCVD SiN_x as a function of rf chuck power.

Figure 9 shows deposition uniformity *vs.* rf chuck power. The typical uniformity was <4%. The uniformity becames somewhat worse as the rf chuck power was increased. It was observed that the center of the deposited films was thicker than edge of the wafer.

As presented in Fig. 10 and 11, raising the chamber pressure increased both the deposition rate and refractive index. The deposition rate increases from 350 Å/min at 1 mTorr to 600 Å/min at 20 mTorr. Over this pressure range, the refractive index increases from 1.92 to 2.32. As shown in Fig. 12, the BOE rate decreases from 1200 to 400 Å/min as the pressure is increased. At high pressure, the residence time of gas species increases by

$$\tau = PV/Q$$
[1]

where τ , *P*, *V*, and *Q* are the residence time, pressure, volume, and throughput, respectively. With longer residence time and higher Ar ion density at high chamber pressure, more SiH₄ may be dissociated into neutrals, which will be incorporated in the films and cause a Sirich composition at high pressure. Increased residence time or higher Ar ion density may contribute to preferential sputtering of the lighter N atoms from the film. It is well known that increased refractive index with Si-rich composition reduces the BOE rate of the films.

As shown in Fig. 13, the stress of the deposited films is constant at about 400 MPa, compressive over the pressure range of 1-15 mTorr. However, at higher pressure (>15 mTorr), stress increased rapidly and reached 1300 MPa at 20 mTorr. This correlated with the



Figure 9. Deposition uniformity of ICPCVD SiN_x as a function of rf chuck power.



Chamber Pressure (mTorr)

Figure 10. Deposition rate of ICPCVD SiN_x as a function of chamber pressure.



Figure 11. Refractive index of ICPCVD SiN_x as a function of chamber pressure.

increase in refractive index, *i.e.*, Si-enrichment. This change in film stoichiometry increases the compressive stress.

Results for $SiH_4/NH_3/He$.—ICPCVD SiN_x deposition from $SiH_4/$ NH₃/He was also investigated. Table II summarizes some of data ob-



Figure 12. BOE rate of ICPCVD SiN_x as a function of chamber pressure.

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Figure 13. Compressive stress of ICPCVD SiN_x as a function of chamber pressure.

tained. The process conditions were 800 W ICP power, 30 W rf chuck power, 10 mTorr, and 150°C. Compared with SiH₄/N₂/Ar, the deposition rates were slightly lower, and the stress was higher. In general, Ar is a superior choice compared with He, due to lower stress in the deposited films.

Deposition rate was not a strong function of rf chuck power (Fig. 14) while stress was controlled by rf chuck power (Fig. 15). The film stress was compressive at low rf chuck power and it became tensile with more rf chuck power.

Silicon dioxide: gap filling.—Processing of some electronic devices, for example, III-V semiconductors and magnetic heads have a limit on the temperature. Conventional high-temperature PECVD silicon dioxide processing is not suitable for those materials. The application of ICPCVD SiO₂ for void-free filling of 1 μ m gap features was investigated. The deposition temperature was 100°C. Table III summarizes some of the main properties of these films.

Figure 16 shows an SEM micrograph of a gap-filled Si trench. The aspect ratio of the trench was about 3:1. Note that there is no void after gap filling is completed. A similar technique was applied on an electroplated metal which had an irregular shaped sidewall. Figure 17 shows self-planarization after gap filling. Note that there were small voids after the process was completed. The origin of the void is from the irregularity of sidewall at the bottom of the trench. As illustrated in Fig. 18, with modified process conditions to compensate for the sidewall problem of the control samples, the trench can be filled with ICPCVD SiO₂ without any void. Further processing (either deposition, or alternatively, chemical mechanical polishing) would bring self-planarization after gap filling.

Conclusions

We investigated low-temperature deposition (150°C) of ICPCVD SiN_x prepared from $SiH_4/N_2/Ar$ and $SiH_4/NH_3/He$. For SiN_x films prepared from $SiH_4/N_2/Ar$, rf chuck power increased refractive index and deposition uniformity while it decreased deposition rate, stress, and BOE rate. Increasing rf chuck power may bring more Si species than N species to the wafer surface leading to Si-rich films. Raising the chamber pressure resulted in higher deposition rate, refractive index, and film stress. The BOE rate of ICPCVD SiN_x , prepared from either $SiH_4/N_2/Ar$ or $SiH_4/N_3/He$, is much lower com-



Refractive index2.0BOE Rate1200 Å/minDeposition rate300 Å/minUniformity±2.5%Film stress200 MPa, (compressive)



Figure 14. Deposition rate of ICPCVD SiN_x as a function of rf chuck power.



Figure 15. Compressive stress of ICPCVD SiN_x as a function of rf chuck power.

pared to PECVD SiN_x deposited at the same low temperature. This implies that the ICPCVD SiN_x films are denser and contain less hydrogen. An ICPCVD SiN_x process for adjustable film stress was demonstrated using $SiH_4/NH_3/He$.

ICPCVD SiO₂ films were prepared from SiH₄/O₂/Ar. Void-free gap filling of high aspect ratio trench was demonstrated with ICPCVD SiO₂.

In conclusion, high-density ICPCVD technology clearly has many advantages compared to PECVD for dielectric film deposition in a broad range of advanced processes for electronic device fabrication, especially at low temperatures.

Acknowledgments

The authors appreciate Dr. J. Donohue, R. Westerman, and Wei Pen for fruitful discussions and assistance. We also thank R. McAfee and L. Heckerd for their technical support. The work at the University of Florida is partially supported by a DOD MURI, monitored by AFOSR (H. C. DeLong), contract no. F49620-96-1-0026.

Table III. Characteristics of ICPCVD SiO₂ film.

Gas chemistry	SiH ₄ /O ₂ /Ar
Deposition rate	~ 1000 Å/min
Film stress	300 MPa, (compressive)
Refractive index	1.46

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Journal of The Electrochemical Society, **147** (4) 1481-1486 (2000) S0013-4651(99)06-103-0 CCC: \$7.00 © The Electrochemical Society, Inc.



Figure 16. SEM micrograph showing a Si trench filled with ICPCVD SiO₂.



Figure 17. Gap-filled and self-planarized SiO₂ on metal coils by ICPCVD.

Plasma-Therm assisted in meeting the publication costs of this article.

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Figure 18. Partially gap-filled metal coils by ICPCVD SiO₂. No voids are evident. The SiO₂ film is planarized.

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