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### Targeting a Mirabegron Precursor by BH<sub>3</sub>-Mediated Continuous Flow

### **Reduction Process**

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Graphical abstract



CATTOD Highlight

- Flow chemistry set up for pharmaceutical applications
- Continuous flow reduction using BH3 solutions
- Straightforward and green preparation of Mirabegron precursor

### Abstract

A continuous-flow reduction of (R)-2-hydroxy-N-[2-(4-nitrophenyl)ethyl]-2-phenylacetamide, involved in the synthetic pathway of Mirabegron, has been developed. This study demonstrated the possibility to safely handling BH<sub>3</sub> complexes within microfluidic reactors using 2-MeTHF as greener alternative to traditional solvents, and without requiring any additive such as DMI. In addition, NMR and HPLC purity analysis revealed that the sole by-product of this process is the diamine **3**, which wouldn't affect the following synthetic steps towards Mirabegron.

### 1. Introduction

The phenylethanolamine core occurs in important molecules such as neurotransmitter noradrenaline and it is also contained in many naturally occurring molecules such as several alkaloids and compounds of pharmaceutical interest with different activities ranging from bronchodilation to antifungal activity (Fig. 1). [1,2]

Among pharmaceutical molecules containing the phenylethanolamine scaffold, 2-(2-aminothiazol-4-yl)-*N*-[4-(2-{[(2*R*)-2-hydroxy-2-phenylethyl]amino}ethyl)phenyl]acetamide, commonly known as Mirabegron®, is a  $\beta$ -3 adrenergic agonist for the treatment of overactive bladder (OAB) with symptoms of urge urinary incontinence and urinary frequency. The main synthetic pathways leading to Mirabegron, reported as patents, are summarized in Scheme 1. Whichever pathway is followed for the production of Mirabegron, a key building block is represented by amine **3** (Scheme 1). Amine **3** can be targeted by reduction of amide **1** to amine **2** using BH<sub>3</sub>·THF in THF and 1,3-dimethyl-2-imidazolidinone (DMI) (Scheme 1, path a). [3] Alternatively, other reducing agents, such as BH<sub>3</sub>·DMS, BH<sub>3</sub>·THF, NaBH<sub>4</sub>, NaBH<sub>4</sub>/BF<sub>3</sub>Et<sub>2</sub>O, LiBH<sub>4</sub>, LiAlH<sub>4</sub>, in suitable solvents (alcohols, ethers and polar aprotic mixtures of solvents) have been proposed. [4] As different approach to amine **3**, the nucleophilic ring-opening of toxic and harmful stireneoxide (Scheme 1, path b), provides derivative **5** which in turn can be converted to derivative **3** upon reductive conditions.

Nevertheless, from a safety and green perspective, either the use of borane as reducing agent, or the use of toxic chemicals (i.e. stireneoxide) should be carefully evaluated when planning an industrial production. As far as safety and toxicity are concerns, it is worth pointing out that flow chemistry is emerging as a green technology for handling of toxic and potentially hazardous chemicals. [5-7] In fact, in recent years the "flow chemistry" and the development of new microfluidic devices are playing an important role, both in academic and industrial research, as viable alternative to batch processing, offering in many cases sustainable synthetic routes. [8-12] The continuous flow production attracted the interest of chemical and pharmaceutical industry, ensuring lower costs, and effectively tackling out safety concerns. [13-15] The use of continuous flow processing allowed also exploring reaction conditions not accessible using traditional batch chemistry. [16] The high surface area in a microflow reactor allows for very fast heat transfer, and precise temperature control, decreasing the risk for runaway reactions. Another important point is the higher efficiency in mixing, realized in flow microreactor compared to batch, thus eliminating or considerably reducing concentration gradients that could negatively affect a fast reaction.

Based on these premises, we report in this work the development of a continuous flow process for the preparation of intermediate **2** (Scheme 1) by reduction of (*R*)-2-hydroxy-*N*-[2-(4-nitrophenyl)ethyl]-2-phenylacetamide **1** using BH<sub>3</sub>·DMS as reducing agent in a greener solvent such as 2-MeTHF. [17]

#### 2. Material and methods

#### 2.1 General (Standard techniques)

Nuclear magnetic resonance spectra were recorded on 300 and 500 MHz spectrometers. Chemical shifts for <sup>1</sup>H NMR spectra were recorded in parts per million from tetramethylsilane with the solvent resonance as the internal standard (chloroform, d = 7.26 ppm).

#### 2.2 General (HPLC analysis)

Each sample has been diluted to final concentration of 0.1 mM in HPLC grade MeOH, filtered, and injected for analysis. Samples were analyzed on Waters HPLC 1525 binary pump system, integrated with Water 2487 UV-Vis dual wavelength detector and an autosampler. Chromatographic conditions: UV detection,  $\lambda_1 = 290$  nm;  $\lambda_2 = 270$  nm; Column: Kinetex 5 $\mu$  C18 100A, 150 × 4.6 mm (Phenomenex), equipped with C18 precolumn; column temperature: 25 °C; injection volume: 10  $\mu$ L; flow rate 0.5 mL/min. Mobile phase composition: linear gradient in 10 min, from 90% 10 mM Ammonium formate (AF) (pH 5)/10% MeOH v/v to 30% 10 mM AF (pH 5)/70% MeOH v/v; then reset to start conditions in 5 min. Total analysis time 20 min.

#### 2.3 Reagents

(*R*)-2-hydroxy-N-(4-nitrophenethyl)-2-phenylacetamide,  $BH_3 \cdot THF 1M$  in THF,  $BH_3 \cdot DMS 2M$  in THF,  $BH_3 \cdot DMS 1M$  in 2-MeTHF were commercially available (Sigma Aldrich, Merck, TCI Europe, Alfa Aesar). THF and 2-MeTHF solutions of  $BH_3 \cdot THF$  and  $BH_3 \cdot DMS$  complexes were prepared from commercial solutions and their concentrations were determined by <sup>1</sup>H NMR analysis using  $BF_3 \cdot Et_2O$  as internal standard. [18]

### 2.4 Flow set up

All experiments were planned by Vapourtec Flow Commander Software in order to set-up solution flow rates and residence time of each experiment (Table 3). The following solutions were prepared and loaded in two different 2 mL PTFE loops: **solution A**: solution of (*R*)-2-hydroxy-N-(4nitrophenethyl)-2-phenylacetamide **1** (0.2M in dry 2-MeTHF) and **solution B**: solution of BH<sub>3</sub>·DMS in dry 2MeTHF (Table 3, 0.6M, entry 7, 1M, entry 2), obtained by diluting commercially available 2M solutions. The solutions were pumped in a 10 mL PTFE coil reactor at a flow rate of 125  $\mu$ L/min (entry 7) at 90 °C with a residence time of 40 minutes, and at a flow rate of 167  $\mu$ L/min (Table 3, entry 2) at 90 °C with a residence time of 30 minutes. The resulting solution was collected under steady state conditions, after 40 minutes and after 30 minutes (Table 3, entry 7 and 2 respectively). The output was quenched with H<sub>2</sub>O and extracted with ethyl acetate.

#### 3. Results and Discussion

Inspired by our previous work concerning the safe handling of  $BH_3$  in a microfluidic reactor, we decided to investigate the reduction step of amide 1 to amine 2 directly in a flow system. [19-27] The first set of reactions were conducted in a flow reactor consisting of a 4 mL coil reactor, a 5 mL coil loop fed with HPLC pumps. Table 1 collects the output of this investigation.

Initially, the effect of temperature and residence time was evaluated (Table 1, entries 1-3). Modest yields were observed with higher residence time using  $BH_3 \cdot DMS$  as the reducing agent. Similar results were observed using  $BH_3 \cdot THF$  as reducing agent (Table 1, entry 4), whereas increasing the temperature up to 60 °C (Table 1, entry 5) a doubling of the yield was obtained, highlighting a key role of the temperature. However, using  $BH_3 \cdot DMS$  at 60 °C, furnished only 25% yield of the desired amine **2** (Table 1, entry 6). Interestingly, reintroducing the solution obtained under the conditions of entry 6 into the loop, and reacted with additional 5 equivalents of  $BH_3 \cdot DMS$  resulted in 70% yield of **2** (Table 1, entry 7). This last result suggested that longer residence times and higher loading of reducing agent would provide better yields. Eventually, temperature could be considered as critical parameter. Nevertheless, the decomposition of the reducing agent need to be taken into account working at higher temperatures.

#### 3.1 Analysis of the reduction process under batch conditions

Building on our previous <sup>11</sup>B NMR experiments [18] on the stability of ethereal solutions of BH<sub>3</sub> complexes, we planned to test the reduction of **1** to **2** using BH<sub>3</sub>•DMS and BH<sub>3</sub>•THF complexes in batch conditions, and with different solvents (Table 2). Under batch conditions, full conversion was observed in THF after 90 and 60 minutes using BH<sub>3</sub>•THF and BH<sub>3</sub>•DMS respectively (Table 2, entries 1, 2). According to our NMR, evidences suggesting a higher stability of BH<sub>3</sub> complexes in 2-MeTHF, [18] a faster reaction was observed in this solvent with both BH<sub>3</sub>•THF and BH<sub>3</sub>•DMS complexes (Table 2, entries 3,4). Nicely, the use of the more stable BH<sub>3</sub>•DMS complex in 2-MeTHF provide full conversion in 15 min reaction time.

With these evidences in hand, the reduction process was reinvestigated using a different flow reactor, and different reaction conditions. In particular, 2-MeTHF was employed as the solvent for two main reasons: a) its higher boiling point; b) the higher stability of the BH<sub>3</sub> complexes. In addition, it is worth pointing out that 2-MeTHF is a greener alternative to other ethereal solvents; it has a higher boiling point with respect to THF (bp 2-MeTHF = 80 °C; bp THF = 67 °C), a lower solubility in water (14 g per 100 g at 23 °C), and it is obtained by renewable feedstocks. [28,29] The new flow set-up used two 2 mL loops, a 10 mL PTFE coil reactor, and a back pressure regulator all connected to a Vapourtec system (Fig. 2). This flow system allowed using temperatures close or even higher than the boiling point for the reaction solvent.

By using this new flow set-up (Table 3, entries 1, 2), high conversions were observed with both reducing agents (87% with  $BH_3 \cdot THF$ , and 92% with  $BH_3 \cdot DMS$  respectively) even if the reaction with  $BH_3 \cdot DMS$  proceeded to full conversion using 2-MeTHF as the solvent, 5 equiv of  $BH_3$  complex, at 90 °C and with 30 minutes residence time. Interestingly, under these conditions, the product of double reduction **3** was also observed though in very low yields (Table 3, entries 1, 2). Moreover, being derivative **2** just the precursor of diamine **3**, its presence in the reaction mixture wouldn't represent a problem for further processing, according to Scheme 1. In order to further improve the process, after optimizing the reaction conditions in terms of temperature, solvent and reducing agent, we tackled the problem of the lowest number of equivalents of  $BH_3 \cdot DMS$  required for full conversion (Table 3, entries 3-8).

As reported in Table 3, reducing the amount of  $BH_3 \cdot DMS$  from 4 equiv. to 2 equiv., while maintaining the same residence time, resulted in lower conversion and lower yield of amine 2 (Table 3, entries 2-6). The best compromise was obtained using 3 equiv of  $BH_3 \cdot DMS$  with 40 minutes of residence time (Table 3, entry 7). Under these conditions, a 94% yield of amine 2 was obtained jointly to 4.6% of diamine 3, so reaching 98.6% of useful compounds for further processing. Increasing the residence time, and reducing the amount of  $BH_3 \cdot DMS$  resulted in lower yield and conversion (Table 3, entry 8).

#### 3.2 NMR monitoring of the flow reduction

The reaction mixtures obtained under flow conditions reported in Table 3, were analyzed by <sup>1</sup>H NMR in order to evaluate the amount of compounds **1**, **2** and **3** in such mixture (Fig. 3). By <sup>1</sup>H NMR analysis, clear signals for the aromatic protons of **1**, **2** and **3** could be recognized allowing for a quantitative evaluation. According to Table 3, entries 2 and 7 gave the best results in terms of conversions and yields.

Moreover, in the case of entry 7, where a lower amount of reducing agent was used, 1.4% of starting material could be detected, we found that acidic work up allowed for complete removal of amide **1** and full recover of reduction products **2** (96.6%) and **3** (3.4%) (see Supplementary material). [30] It is worth mentioning that such conclusions were confirmed by a HPLC quantitative analysis (see Supplementary material).

### 4. Conclusions

In conclusion, a continuous-flow reduction of (R)-2-hydroxy-N-[2-(4-nitrophenyl)ethyl]-2-phenylacetamide, involved in the synthetic pathway of Mirabegron, has been developed. This study demonstrated the possibility to safely handly BH<sub>3</sub> complexes within microfluidic reactors using 2-MeTHF as greener alternative to traditional solvents, and without requiring any additive such as DMI. In addition, NMR and

HPLC purity analysis revealed that the sole by-product of this process is the diamine **3**, which wouldn't affect the following steps towards Mirabegron.

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[30] Attempts to induce, under batch conditions, complete reduction of amine 2 to diamine 3 failed even using a large excess of  $BH_3$  DMS.



Fig. 1. Pharmaceutical molecules containing the phenylethanolamine core.



10 ml PTFE coil





Fig. 3. <sup>1</sup>H-NMR monitoring of the flow reduction



Scheme 1 Synthetic pathways leading to Mirabegron

$\begin{array}{c} OH \\ H \\ O \\ 1 \\ 0.2 M \\ THF \\ H_3 Complex \\ 1 M \end{array} \begin{array}{c} 5ml \\ V = 4ml \\ T \\ F \\ BH_3 Complex \\ 1 M \end{array} \begin{array}{c} 0 \\ F \\ OH \\ OH \\ C \\ 2 \\ NO_2 \end{array} $								
Entry	Reducing agent	Reducing agent	Flow rate <sup><i>a</i></sup>	Т	t <sub>R</sub>	Yield <sup>b</sup>		
Епцу	[mol/L]	(equiv)	(µL/min)	(°C)	(min)	(%)		
1	BH <sub>3</sub> ·DMS [1M]	5	66.67	25	30	14		
2	BH <sub>3</sub> ·DMS [1M]	5	66.67	50	30	14		
3	BH <sub>3</sub> ·DMS [1M]	5	33.33	25	60	22		
4	BH <sub>3</sub> ·THF [1M]	5	66.67	25	30	20		
5	BH <sub>3</sub> ·THF [1M]	5	66.67	60	30	38		
6	BH <sub>3</sub> ·DMS [1M]	5	66.67	60	30	25		
7	BH <sub>3</sub> ·DMS [1M]	$10(2 \text{ runs})^{c}$	66.67	60	$60 (2 \text{ runs})^c$	70		

Table 1 Optimization study of the reduction of 1 with BH<sub>3</sub> in a continuous flow microreactor.

<sup>*a*</sup> Flow rates for solutions of **1** and BH<sub>3</sub>. <sup>*b*</sup> Determined by <sup>1</sup>H-NMR using the internal standard. <sup>*c*</sup> The solution resulting from entry 6 was reintroduced into the loop and reacted with additional 5 equiv. of BH<sub>3</sub>·DMS with a  $t_R$  of additional 30 min.

**Table 2** Batch study of the reduction of amide 1 to amine 2.



Table 3 Optimization study of the reduction of 1 (0.2 M) in 2-MeTHF and BH<sub>3</sub>DMS (2M in THF)



<sup>a</sup> Flow rate of **1** and BH<sub>3</sub> Complex <sup>b</sup> Determined by <sup>1</sup>H-NMR using internal standard