

# Spark Plasma Sintering of Nanosized Amorphous Silicon Nitride Powder with a Small Amount of Sintering Additive

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**Dense and fine-grained  $\beta$ - $\text{Si}_3\text{N}_4$  ceramics were successfully obtained with a small amount of sintering additives, 1.5 mass%  $\text{Y}_2\text{O}_3$  and 0.5 mass%  $\text{Al}_2\text{O}_3$ , using nanosized amorphous  $\text{Si}_3\text{N}_4$  powder by spark plasma sintering at temperatures of 1500–1800°C and a pressure of 30 MPa under  $\text{N}_2$ . The  $\beta$ - $\text{Si}_3\text{N}_4$  ceramics were composed of equiaxed grains with an average size of 300 nm. A higher sintering temperature was required for the densification of submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powder with the small amount of the additives. The use of nanosized amorphous  $\text{Si}_3\text{N}_4$  powder accelerated the densification and the transformation to the  $\beta$ -phase.**

## I. Introduction

SILICON NITRIDE ( $\text{Si}_3\text{N}_4$ ) ceramics are one of the most promising materials for structural applications at high temperature. However,  $\text{Si}_3\text{N}_4$  is very difficult to densify by solid-phase sintering because of its strong covalent nature and low self-diffusion coefficients of Si and N. In general, the conventional densification of  $\text{Si}_3\text{N}_4$  ceramics is achieved by liquid-phase sintering with metal oxides additives such as  $\text{MgO}$ ,  $\text{Al}_2\text{O}_3$ , and  $\text{Y}_2\text{O}_3$ . In contrast, the grain-boundary phase derived from the sintering additives degraded the high-temperature mechanical properties, and the corrosion and oxidation resistance of  $\text{Si}_3\text{N}_4$  ceramics.<sup>1</sup> Therefore, in order to improve these properties, it is necessary to minimize the amount of sintering additives used for dense  $\text{Si}_3\text{N}_4$  ceramics. The densification of  $\text{Si}_3\text{N}_4$  using conventional sintering techniques such as gas-pressure sintering and hot pressing typically required the total amount of sintering additives of 5–10 mass%.<sup>2,3</sup>

Spark plasma sintering (SPS) technique can heat specimens rapidly because the pulsed direct current used in this technique is possible to pass through the graphite die and punch rods.<sup>4</sup> Thus, the entire sintering process can be completed in a short time, leading to suppression of grain growth during sintering at high temperature. Accordingly, densification of low-sinterable materials was accelerated and a fine-grained microstructure was formed by SPS.<sup>5–10</sup> The SPS technique is sometimes called as pulse electric current sintering (PECS),<sup>11–13</sup> field-assisted sintering technique,<sup>14</sup> and plasma-assisted sintering,<sup>15</sup> because the generation of spark discharge and/or plasma during SPS process has not been verified. By using the SPS process, low-sinterable oxides, nitrides, and carbides, which are difficult to densify by conventional sintering techniques, have been fabricated as fully dense materials. With regard to  $\text{Si}_3\text{N}_4$  ceramics, there were re-

ports on the fabrication by SPS.<sup>10,12,15</sup> The total amount of the sintering additives of > 5 mass% was used for the densification of  $\text{Si}_3\text{N}_4$  powders by the SPS technique, which was the same amount of additive as that by conventional sintering techniques.

We reported that fine-grained  $\beta$ - $\text{Si}_3\text{N}_4$  ceramics were prepared with a general amount of sintering additive of 6 mass%  $\text{Y}_2\text{O}_3$  and 2 mass%  $\text{Al}_2\text{O}_3$  using submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  and nanosized amorphous  $\text{Si}_3\text{N}_4$  powders by SPS.<sup>5</sup> Furthermore, at the amount of the sintering additives, the densification of the nanosized amorphous  $\text{Si}_3\text{N}_4$  powder was easier to proceed than that of the submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$ .<sup>5</sup> The use of nanosized amorphous  $\text{Si}_3\text{N}_4$  is expected to fabricate nanostructured  $\text{Si}_3\text{N}_4$  ceramics that reduce the amount of sintering additives for the densification.

In the present study, nanosized amorphous  $\text{Si}_3\text{N}_4$  powder was sintered with a relatively small amount of  $\text{Y}_2\text{O}_3$  and  $\text{Al}_2\text{O}_3$  additives by SPS, and densification, phase transformation, and microstructure of the  $\text{Si}_3\text{N}_4$  sintered bodies were studied. Also, these results were compared with those of the products prepared using submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powder.

## II. Experimental Procedure

Nanosized amorphous  $\text{Si}_3\text{N}_4$  powder was prepared by a vapor-phase reaction from  $\text{SiCl}_4$  and  $\text{NH}_3$  gases. The amorphous  $\text{Si}_3\text{N}_4$  powder consisted of spherical particles with an average size of 80 nm (number mean diameter via SEM analysis). The total oxygen content of the nanosized amorphous  $\text{Si}_3\text{N}_4$  powder was 4.8 mass%. As a reference, submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powder ( $\beta$ -phase: < 5%, total oxygen content: 1.2 mass%, SN-E10 grade, Ube Industries Ltd., Ube, Japan) with an average particle size of 170 nm (number mean diameter) was also used as a starting material. 1.5 mass%  $\text{Y}_2\text{O}_3$  (average particle size: 300 nm, UU-HP grade, Shin-Etsu Chemical Co. Ltd., Tokyo, Japan) and 0.5 mass%  $\text{Al}_2\text{O}_3$  ( $\alpha$ -phase, average particle size: 500 nm, AKP-20 grade, Sumitomo Chemical Co. Ltd., Tokyo, Japan) powders were added to  $\text{Si}_3\text{N}_4$  powders as sintering additives. These powders were mixed with a small amount of ethanol, dried, and then sieved with a pore-opening size of 300  $\mu\text{m}$ . The powder mixture was filled in a graphite die of 15 mm in inner diameter and sintered at a temperature of 1500–1700°C for a holding time of 30 min and at 1800°C for 1 min under a uniaxial pressure of 30 MPa in  $\text{N}_2$  atmosphere by SPS (SPS-515S, SPS Syntex Inc., Kanagawa, Japan). The mixed powder was heated at rates of 150 and 300°C/min. The overshoot of the temperature of about 15°C occurred at the rapid heating rate of 300°C/min, although little overshoot of the temperature was monitored at 150°C/min. The heating temperature on the surface of the die was measured with a radiation thermometer. The relative densities of the sintered samples were determined by the Archimedes method. The phase composition and phase transformation of the samples were evaluated using X-ray diffractometry (XRD; MiniFlex, Rigaku Corp., Tokyo, Japan) with  $\text{CuK}\alpha$  radiation for sintered samples. The content ratio of the  $\alpha$ - and  $\beta$ - $\text{Si}_3\text{N}_4$  phases in the samples was estimated from the peak intensities using the

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equation proposed by Gazzara and Messier.<sup>16</sup> The sintered specimens were polished with a 3- $\mu\text{m}$  diamond slurry, and then etched by plasma in  $\text{CF}_4$  and  $\text{O}_2$  gases. The etched surfaces were observed by scanning electron microscopy (SEM; S-5200, JEOL Ltd., Tokyo, Japan). The average grain size (number mean diameter) of the  $\text{Si}_3\text{N}_4$  bodies was determined from the linear intercept length of 100 grains in the SEM pictures.

### III. Results and Discussion

In the products prepared from nanosized amorphous  $\text{Si}_3\text{N}_4$  powder at  $1500^\circ\text{C}$ – $1700^\circ\text{C}$  for a holding time of 30 min at a heating rate of  $150^\circ\text{C}/\text{min}$ ,  $\text{Si}_2\text{N}_2\text{O}$  was slightly detected as a secondary phase by XRD analysis. The formation of  $\text{Si}_2\text{N}_2\text{O}$  may be due to a reaction of  $\text{Si}_3\text{N}_4$  with the surface oxide in amorphous  $\text{Si}_3\text{N}_4$  particles during the long sintering process at high temperatures, i.e.,  $1700^\circ\text{C}$  for 30 min.<sup>2</sup> In a previous study of the sintering of nanosized amorphous  $\text{Si}_3\text{N}_4$  powder with a typical amount of  $\text{Y}_2\text{O}_3$  and  $\text{Al}_2\text{O}_3$  additives,<sup>3</sup>  $\text{Si}_2\text{N}_2\text{O}$  was not observed in the products.

Figure 1 shows the effect of sintering temperature on the relative density and  $\alpha$ -phase ratio of specimens sintered at  $1500^\circ\text{C}$ – $1700^\circ\text{C}$  for 30 min and at  $1800^\circ\text{C}$  for 1 min at  $150^\circ\text{C}/\text{min}$  using nanosized amorphous  $\text{Si}_3\text{N}_4$  and submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powders. In the submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powder, with sintering at  $1500^\circ\text{C}$ , the relative density of the specimen was about 60%. When the temperature increased to  $1700^\circ\text{C}$ , the density increased to 93%. At  $1800^\circ\text{C}$  for 1 min, the specimen with a high density of  $>98\%$  was obtained. The transformation from  $\alpha$ - to  $\beta$ -phase occurred with the increasing density of the specimens. With sintering at  $1800^\circ\text{C}$ , only the  $\beta$ -phase formed. In nanosized amorphous  $\text{Si}_3\text{N}_4$  powder, on the other hand, only  $\beta$ -phase was observed even at  $1500^\circ\text{C}$  and the amorphous phase directly transformed into the crystalline  $\beta$ -phase. The density of the specimens reached 95% even at  $1500^\circ\text{C}$ , although the densification of the submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powder required a high temperature of  $1800^\circ\text{C}$ . This suggested that the densification of nanosized amorphous  $\text{Si}_3\text{N}_4$  powder was achieved at a lower temperature than that of the submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powder with a relatively small amount of sintering additive. The high sinterability of nanosized amorphous  $\text{Si}_3\text{N}_4$  powder might be caused by a smaller particle size and a larger amount of total oxygen content of the nanosized amorphous  $\text{Si}_3\text{N}_4$  powder. The transformation from  $\alpha$ - to  $\beta$ -phase for  $\text{Si}_3\text{N}_4$  ceramics is mainly dependent on the densification.<sup>3</sup> Consequently, because nanosized amorphous  $\text{Si}_3\text{N}_4$  powder was fully densified at a lower temperature than the submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powder, the transformation to  $\beta$ -phase might be completed at a lower temperature.

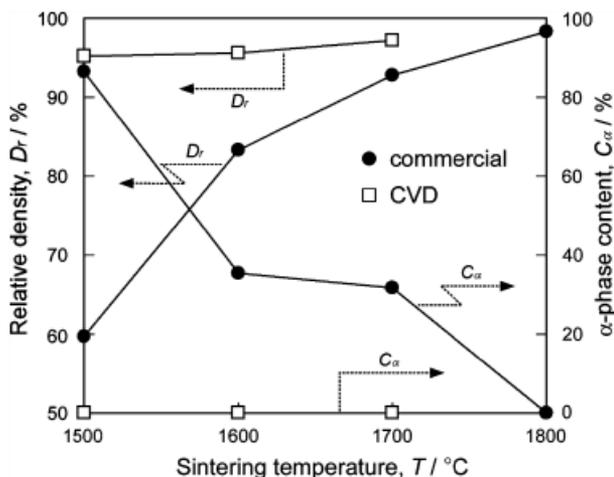


Fig. 1. The effect of sintering temperature on the relative density and  $\alpha$ -phase ratio of  $\text{Si}_3\text{N}_4$  ceramics prepared at  $1500^\circ\text{C}$ – $1700^\circ\text{C}$  for a holding time of 30 min and at  $1800^\circ\text{C}$  for 1 min at a heating rate of  $150^\circ\text{C}/\text{min}$ .

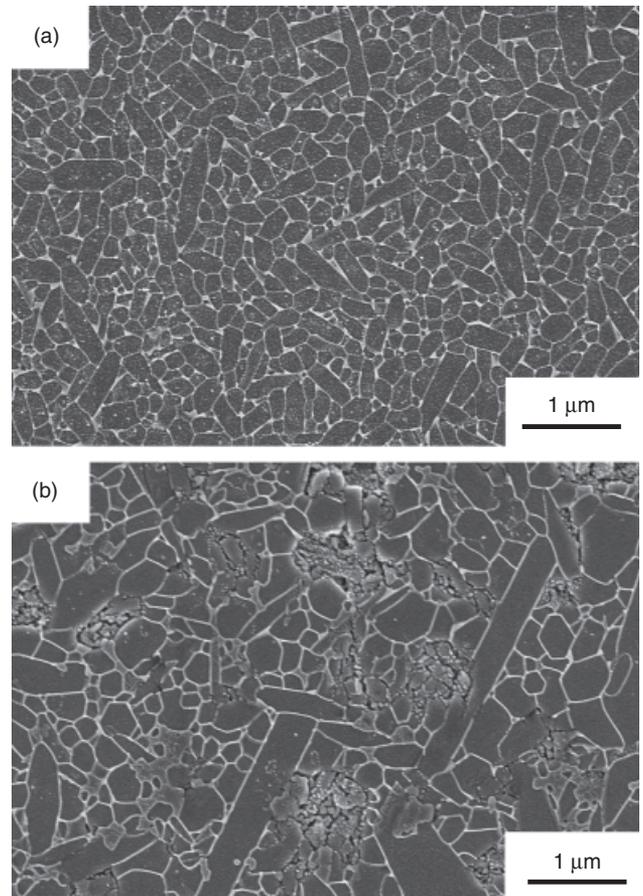
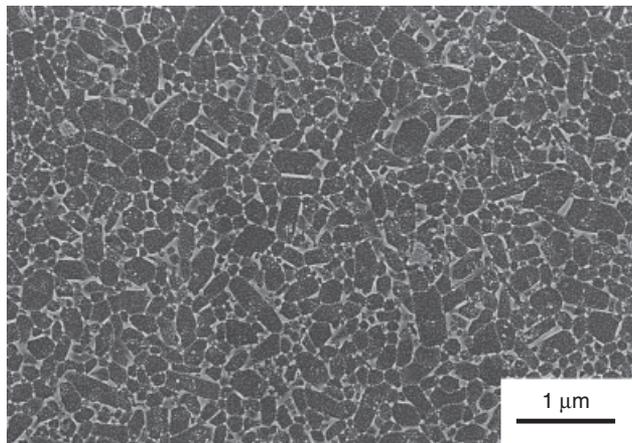


Fig. 2. Scanning electron micrographs of the etched surfaces of  $\text{Si}_3\text{N}_4$  ceramics prepared at  $1700^\circ\text{C}$  for 30 min at  $150^\circ\text{C}/\text{min}$  using nanosized amorphous  $\text{Si}_3\text{N}_4$  (a) and submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powders (b).

Figure 2 shows SEM micrographs of the etched surfaces of the  $\text{Si}_3\text{N}_4$  ceramics prepared at  $1700^\circ\text{C}$  for 30 min at  $150^\circ\text{C}/\text{min}$  using nanosized amorphous  $\text{Si}_3\text{N}_4$  and submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powders. The  $\text{Si}_3\text{N}_4$  ceramics obtained from nanosized amorphous  $\text{Si}_3\text{N}_4$  powder were composed of finer equiaxed and elongated grains, compared with those from submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powder. The growth of elongated  $\text{Si}_3\text{N}_4$  grains was quite noticeable in  $\text{Si}_3\text{N}_4$  ceramics prepared using submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powder. In addition, a residual pore was clearly observed in the  $\text{Si}_3\text{N}_4$  ceramics obtained from the submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powder. This supported that the densification of submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powder was not achieved at  $1700^\circ\text{C}$  as shown in Fig. 1. The use of nanosized amorphous  $\text{Si}_3\text{N}_4$  powder enables to achieve densification at a lower temperature, because nanosized amorphous  $\text{Si}_3\text{N}_4$  had a higher sinterability compared with the submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$ . Therefore, the grain growth was inhibited during sintering, resulting in the production of fine-grained  $\text{Si}_3\text{N}_4$  ceramics.

Using rapid sintering at a heating rate of  $300^\circ\text{C}/\text{min}$  and at  $1800^\circ\text{C}$  for 1 min, dense  $\beta$ - $\text{Si}_3\text{N}_4$  ceramics with a relative density of 96% were successfully fabricated without the formation of  $\text{Si}_2\text{N}_2\text{O}$  in the product. A SEM micrograph of the  $\beta$ - $\text{Si}_3\text{N}_4$  ceramics is shown in Fig. 3. The nearly equiaxed grains with an average size of 300 nm (number mean diameter via SEM images) were observed in the fully dense  $\beta$ - $\text{Si}_3\text{N}_4$  ceramics. Suganuma *et al.*<sup>12</sup> and Schneider *et al.*<sup>15</sup> reported dense  $\text{Si}_3\text{N}_4$  ceramics consisting of fine and equiaxed  $\text{Si}_3\text{N}_4$  grains from the submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powder using SPS. Nishimura *et al.*<sup>10</sup> revealed how to form a homogeneous microstructure without elongated grains using nanosized  $\beta$ - $\text{Si}_3\text{N}_4$  powder by SPS. Szépvölgyi and Mohai<sup>2</sup> reported that hot pressing of nanosized amorphous  $\text{Si}_3\text{N}_4$  powder produced  $\text{Si}_2\text{N}_2\text{O}$  as a secondary phase. For the densification of these  $\text{Si}_3\text{N}_4$  powders, the total



**Fig. 3.** Scanning electron micrograph of the etched surface of  $\text{Si}_3\text{N}_4$  ceramics prepared at  $1800^\circ\text{C}$  for 1 min at  $300^\circ\text{C}/\text{min}$  using nanosized amorphous  $\text{Si}_3\text{N}_4$  powder.

amount of sintering additives over 5 mass% was used. When the amount of additives decreases, the sintering temperature for the densification generally increases, leading to a significant grain growth. In this work, dense and fine-grained  $\text{Si}_3\text{N}_4$  ceramics were able to be fabricated with a small amount of sintering additives, 2 mass%, and using nanosized amorphous  $\text{Si}_3\text{N}_4$  powder.

#### IV. Conclusions

Nanosized amorphous  $\text{Si}_3\text{N}_4$  powder was sintered with a relatively small amount of sintering additives, 1.5 mass%  $\text{Y}_2\text{O}_3$  and 0.5 mass%  $\text{Al}_2\text{O}_3$ , by SPS. Densification, phase transformation, and microstructure of the  $\text{Si}_3\text{N}_4$  sintered bodies were investigated. The densification and phase transformation to  $\beta$ -phase in the nanosized amorphous  $\text{Si}_3\text{N}_4$  powder were completed at a lower temperature, i.e.,  $1500^\circ\text{C}$ , than those in the submicrometer-sized  $\alpha$ - $\text{Si}_3\text{N}_4$  powder.  $\text{Si}_2\text{N}_2\text{O}$  formed as a secondary phase in the long sintering at  $1500^\circ\text{C}$ – $1700^\circ\text{C}$  for 30 min at  $150^\circ\text{C}/\text{min}$

using nanosized amorphous  $\text{Si}_3\text{N}_4$  powder. When rapid sintering at a heating rate of  $300^\circ\text{C}/\text{min}$  and at  $1800^\circ\text{C}$  for 1 min was used, fully-dense  $\beta$ - $\text{Si}_3\text{N}_4$  ceramics consisting of equiaxed grains with an average size of 300 nm were prepared without forming  $\text{Si}_2\text{N}_2\text{O}$ .

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