



Pergamon

Materials Research Bulletin 37 (2002) 2043–2053

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Materials  
Research  
Bulletin

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## Effect of preparative parameters on the electrical conductivity of $\text{Li}_2\text{SO}_4\text{--Al}_2\text{O}_3$ composites

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(Refereed)

Received 10 July 2000; accepted 16 May 2001

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### Abstract

The effect of various preparative parameters, such as the size and form of alumina and also the time of sintering, on the electrical conductivity of the  $\text{Li}_2\text{SO}_4\text{--Al}_2\text{O}_3$  composite system has been investigated. The sintering time appears to be an insignificant preparative parameter. The role of different phases of  $\text{Al}_2\text{O}_3$  on the electrical conductivity of the composite clearly establishes that the maximum enhancement is achieved for  $\gamma\text{-Al}_2\text{O}_3$ . The 50 m/o  $\text{Al}_2\text{O}_3$  composition was found to exhibit the highest conductivity, an enhancement of three orders of magnitude at  $500^\circ\text{C}$ . The experimental data indicates higher conduction in the space charge layer near the surface to be the possible mechanism of conductivity enhancement.

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**Keywords:** A. Composites; A. Interfaces; B. Sol–gel chemistry; C. X-ray diffraction; C. Impedance spectroscopy; D. Ionic conductivity

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### 1. Introduction

In recent times, heterogeneous doping has been employed to enhance the conductivity of solid electrolytes. It involves the dispersal of submicron insulating particles in the host matrix, thereby forming a composite. In general, in most of these systems, it is also believed that no chemical reaction is found to occur between

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the matrix and the dispersoid. Following the discovery of the phenomenon by Liang in 1973 [1], enhancements in conductivity, between one and three orders of magnitude, have been effected for a number of composite systems by the dispersal of an insulating second phase [2–6].

A number of theoretical models on this subject have evinced sufficient attention [6–14], and continue to be worked upon. It is widely accepted that unlike homogeneous doping, local deviation from electroneutrality plays an important role in heterogeneous doping [7].

Various mechanisms have been reviewed in literature in recent times to explain the “composite effect” [6,7,12]. The interface mechanisms involve one or more of the following scenarios: space charge layer formation at the matrix–particle interface, enhanced conduction at the core of the interface, or an interfacial phase formation and effects of adsorbed surface moisture and impurities. By a similar token, the matrix mechanisms, on the other hand, involve enhanced charge transportation along grain boundaries and dislocations, the stabilization of highly conducting metastable phases due to the addition of the dispersoid, or a homogeneous doping of the matrix.

As for the host system, the focus has changed from past studies involving mainly halides of alkali metals or silver to recent investigations predominantly on sulfates, carbonates, nitrates, tungstates, and other salts of alkali metals [15–22]. These investigations have led to new features in the conductivity–composition and conductivity–temperature behavior. Increasingly, materials like  $\text{BaTiO}_3$  and other ferroelectric phases with the perovskite structure [18–22] are being used as dispersoids. Much of the literature, however, comprises of work involving alumina (in the  $\gamma\text{-Al}_2\text{O}_3$  form) and silica, though, to a lesser extent. Surprisingly, very recently, we have reported that even the use of  $\alpha\text{-Al}_2\text{O}_3$  as a dispersoid has been responsible for a significant enhancement in conductivity of  $\text{Na}_2\text{SO}_4\text{-Al}_2\text{O}_3$  composite system [23].

Of greater interest among the alkali sulfates is the high-temperature form of lithium sulfate that offers an exceptionally large conductivity. Lithium sulfate exists at room temperature in a monoclinic form and undergoes a phase transition at  $575^\circ\text{C}$  to a fcc structure ( $Fm3m$ ) having a high degree of rotational disorder. The ionic conductivity of the high-temperature phase,  $\alpha\text{-Li}_2\text{SO}_4$ , is of the order of  $\sim 1 \Omega^{-1} \text{cm}^{-1}$  at  $610^\circ\text{C}$  [24]. Forland and Krogh-Moe [25] have investigated the structure of  $\alpha$ -phase and found that a molten sublattice-type mechanism is responsible for the large conductivity in  $\alpha\text{-Li}_2\text{SO}_4$ .

Thus far, there has been only a single investigation on the  $\text{Li}_2\text{SO}_4\text{-Al}_2\text{O}_3$  composite system. It has been established clearly by Zhu et al. [26] that the  $\text{Li}_2\text{SO}_4\text{-Al}_2\text{O}_3$  composites exhibit much higher conductivity relative to pure  $\text{Li}_2\text{SO}_4$ . However, the role of the form of alumina, size, and sintering characteristics remain undetermined.

In the present work, we have experimented with the role of the preparatory parameters and the role of the phase of  $\text{Al}_2\text{O}_3$ . Through a fitting of various existing theoretical models to our experimental data, we have also aimed to identify a possible mechanism of conductivity for this system. This work also unambiguously establishes

the effect of the phase and content of  $\text{Al}_2\text{O}_3$  on the conductivity of  $\text{Li}_2\text{SO}_4\text{--Al}_2\text{O}_3$  composite. While investigating the role of preparative parameters, we have been able to analyze the effect of factors like the time and temperature of sintering, as well as the size and form of alumina on the electrical conductivity of the composite.

## 2. Experimental

Lithium sulfate was procured from Loba Chemie (India) and Aldrich (Milwaukee, WI, USA). By employing the sol–gel process, very fine size alumina ( $\sim 40 \text{ \AA}$ ) was prepared in the laboratory. Initially, ultrafine Boehmite,  $\text{AlO}(\text{OH})$  was synthesized by the action of deionized water on amalgamated aluminum. A stable aqueous suspension (sol) was formed by adding a few drops of acetic acid and peptizing at  $80^\circ\text{C}$  for 15 min. The sol was gelled with a dehydrating agent (2-ethyl hexanol) in the presence of a surfactant (Span 80). The gel was dried and calcined at different temperatures to obtain alumina. The inevitable particle size distribution in the product was narrowed down considerably by a size fractionation procedure using a pipette centrifuge (Ladal Analysette Model 21.002). This instrument, normally used for the measurement of particle size distribution, consisted of a shallow stainless steel bowl that holds the sample in the form of a suspension. The bowl was rotated about its central axis at speed up to 1500 rpm, and size separation occurred during the centrifugal motion. Samples were sucked out at specified time intervals from points at a fixed distance from the axis. The samples collected at different times were dried and analyzed for particle size using TEM and surface area measurement techniques.

Dispersal Sol-P3 ( $\text{Al}_2\text{O}_3 \sim 70\%$ , acetic acid  $\sim 6\text{--}7.5\%$ ), a water dispersible alumina hydrate, obtained from Condea Chemie (Germany), was also processed to obtain alumina with a particle size of about  $1 \text{ }\mu\text{m}$ . The alumina sol was prepared by pouring dispersal Sol-P3 powder into water and subjecting it to intensive stirring. After stirring for 15 min, the sol was synthesized and was then characterized to determine its particle size.

Lithium sulfate and alumina were mixed in appropriate mole percentages and stirred thoroughly in deionized water. The mixtures were then dried to achieve a fine dispersion of second phase particles. The samples were then ground into fine powders and pelletized at pressure of around  $32 \text{ kN cm}^{-2}$ . The resulting pellets were sintered at different temperatures for 12 h and furnace cooled. They were then gold coated to provide good contact with the Pt electrodes for the impedance measurements.

The DSC measurements were made using DuPont 9900 calorimeter at a heating rate of  $10^\circ\text{C min}^{-1}$ . The room temperature XRD patterns were recorded with a PW1820 Philips diffractometer using  $\text{Cu K}\alpha$  ( $\lambda = 1.54 \text{ \AA}$ ) radiation. The impedance measurements were carried out as a function of temperature using a computer controlled Solartron impedance gain/phase analyzer, Model Schlumberger SI 1260. The measurements were made in the frequency range of 1 Hz–32 MHz, with a signal amplitude of 100 mV.

### 3. Results and discussion

#### 3.1. Effect of preparative parameters

It is observed that the pelletizing pressure does not affect the electrical conductivity of the composite in a significant manner. To investigate the effect of sintering time, the  $\text{Li}_2\text{SO}_4$ –43 m/o  $\text{Al}_2\text{O}_3$  composition, that exhibited the maximum conductivity in an earlier study [26], was treated at 2, 6, 12, and 20 h, respectively. Fig. 1 exhibits the plot of  $\log \sigma$  versus  $1000/T$  for the  $\text{Li}_2\text{SO}_4$ – $\text{Al}_2\text{O}_3$  composite sintered for different durations at  $800^\circ\text{C}$ . Among these, the conductivity of the composite treated at 12 h was found to be marginally higher. However, the sintering time does not appear to be a significant preparative parameter.

Fig. 2 displays the variation of conductivity for  $\text{Li}_2\text{SO}_4$ – $\text{Al}_2\text{O}_3$  composites for two different particle sizes of  $\text{Al}_2\text{O}_3$ . There does not appear to be much variation in the conductivity of the two composites. The  $\text{Al}_2\text{O}_3$  as processed by the Sol-P3 route has a size of  $\sim 1\ \mu\text{m}$ , while the other processed by the sol–gel route has a size of  $40\ \text{\AA}$ . Although some of the early studies suggest that the conductivity of the composite increases as the size of the dispersoid decreases [6], more recent studies have emphasized the correlation of the increase in the conductivity with the increase in the effective surface area of the dispersed phase. Our results are in agreement with such a correlation. Although nothing can be said about the surface area for the alumina with the two particle sizes, it is clear that despite reducing the  $\text{Al}_2\text{O}_3$  size by almost about two orders of magnitude, the conductivity remains unaffected. One factor, often overlooked, but can help explain our results is that as-received fine size

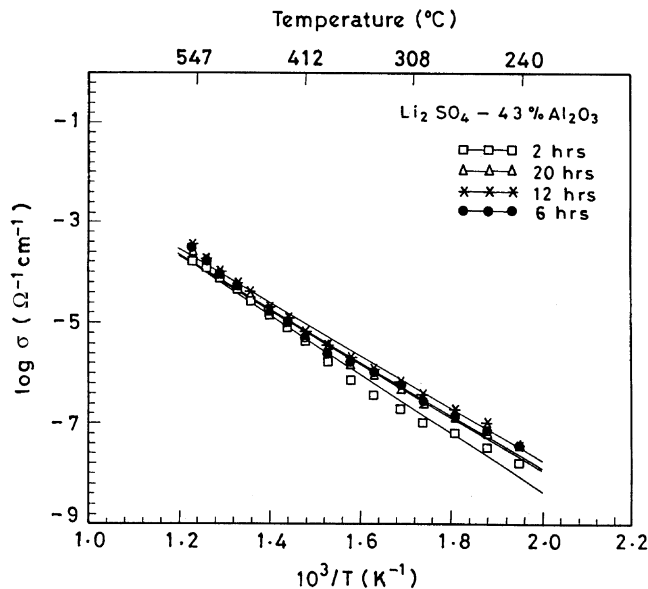


Fig. 1. Variation of  $\log \sigma$  vs.  $1000/T$  for  $\text{Li}_2\text{SO}_4$ –43 m/o  $\text{Al}_2\text{O}_3$  treated at  $800^\circ\text{C}$  for different sintering times.

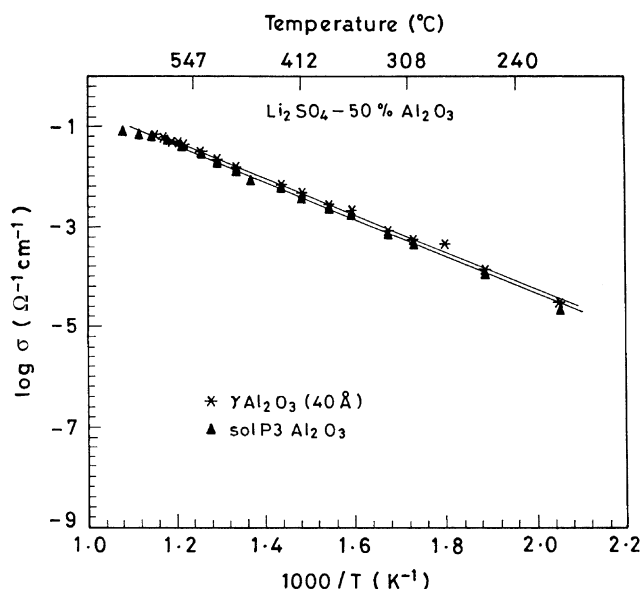


Fig. 2. Variation of  $\log \sigma$  vs.  $1000/T$  for  $\text{Li}_2\text{SO}_4$ –50 m/o  $\text{Al}_2\text{O}_3$  for 40 Å and 1  $\mu\text{m}$  sized alumina.

particles are invariably highly agglomerated. We have already reported such an agglomeration in case of the  $\text{Na}_2\text{SO}_4$ – $\text{Al}_2\text{O}_3$  composite system [23]. This agglomeration reduces the effective interface area for less than theoretically dense composites, as the matrix material is unlikely to fill the deep pores and crevices of the irregular cluster. Unless the samples are 100% dense, the actual interface area is likely to be considered less than the measured surface area of the second phase particles. Large particles having a very high surface area can also enhance the conductivity as effectively as extremely small, non-porous particles with a similar effective surface area.

### 3.2. Conductivity versus nature of $\text{Al}_2\text{O}_3$ phases

$\text{Al}_2\text{O}_3$  exhibits a number of phases such as  $\gamma$ -,  $\theta$ -,  $\kappa$ -,  $\delta$ -, and  $\alpha$ - $\text{Al}_2\text{O}_3$ . Table 1 shows the various phases of  $\text{Al}_2\text{O}_3$  identified from the XRD for the  $\text{Li}_2\text{SO}_4$ –43 m/o  $\text{Al}_2\text{O}_3$  composition treated at different processing temperatures.

Table 1

Temperature of treatment for the $\text{Li}_2\text{SO}_4$ –43 m/o $\text{Al}_2\text{O}_3$ composition ( $^{\circ}\text{C}$ )	Phases observed in XRD
500	$\text{Li}_2\text{SO}_4$ – $\gamma$ - $\text{Al}_2\text{O}_3$
700	$\text{Li}_2\text{SO}_4$ – $\delta$ - $\text{Al}_2\text{O}_3$
800	$\text{Li}_2\text{SO}_4$ – $\delta$ - $\text{Al}_2\text{O}_3$
1000	$\text{Li}_2\text{SO}_4$ – $\kappa$ - $\text{Al}_2\text{O}_3$ + $\theta$ - $\text{Al}_2\text{O}_3$
1200	$\text{Li}_2\text{SO}_4$ – $\theta$ - $\text{Al}_2\text{O}_3$
1400	$\gamma$ - $\text{LiAlO}_2$

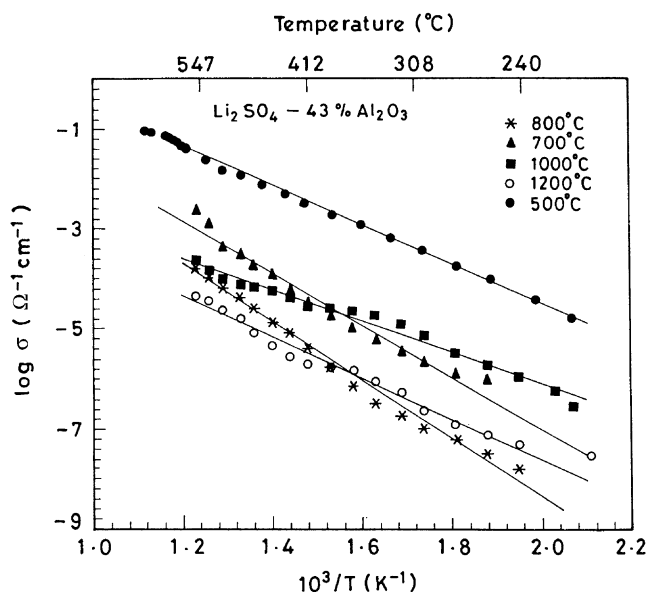


Fig. 3. Variation of  $\log \sigma$  vs.  $1000/T$  for  $\text{Li}_2\text{SO}_4$ -43 m/o  $\text{Al}_2\text{O}_3$  treated at different sintering temperatures.

Fig. 3 exhibits the variation of conductivity for the various sintering temperatures chosen in this study. Among all these phases of  $\text{Al}_2\text{O}_3$ , the composite having the  $\gamma$ - $\text{Al}_2\text{O}_3$  phase exhibits the largest enhancement in conductivity. This may be attributed to the higher surface activity of the  $\gamma$ -phase [26], relative to that for the other phases of alumina. The conductivity of the composite containing the  $\gamma$ - $\text{Al}_2\text{O}_3$  is almost an order of magnitude higher than the composites exhibiting other phases of  $\text{Al}_2\text{O}_3$ . Analyses of X-ray diffractograms of composites under investigation show that no new phase like lithium aluminates are formed during the mechanochemical treatment and sintering thereafter. The results are in agreement with the analysis of Uvarov et al. [27]. There is, however, an exception only for composites processed at temperatures in excess of  $\sim 1300^\circ\text{C}$ , the formation of lithium aluminates is observed. The phase identified in the composite treated at  $1400^\circ\text{C}$  is  $\gamma$ - $\text{LiAlO}_2$  (Table 1).

### 3.3. Conductivity versus composition

Most of the composites studied show a recognizable, uniform type of conductivity dependence on composition. Like in most other composites ( $\text{CuCl}-\text{Al}_2\text{O}_3$ ,  $\text{LiI}-\text{Al}_2\text{O}_3$ ), the conductivity in  $\text{Li}_2\text{SO}_4$ - $\text{Al}_2\text{O}_3$  composite also increases with increasing  $\text{Al}_2\text{O}_3$  content, passing through a maximum at 50 m/o  $\text{Al}_2\text{O}_3$ .

Fig. 4 exhibits the conductivity plots for the  $\text{Li}_2\text{SO}_4$ - $\gamma$ - $\text{Al}_2\text{O}_3$  system. A maximum in conductivity is observed at around 50 m/o  $\text{Al}_2\text{O}_3$ . Table 2 displays the conductivity enhancements obtained for compositions with varying contents of alumina at 300 and  $500^\circ\text{C}$ , respectively. The enhancement in conductivity for compositions containing

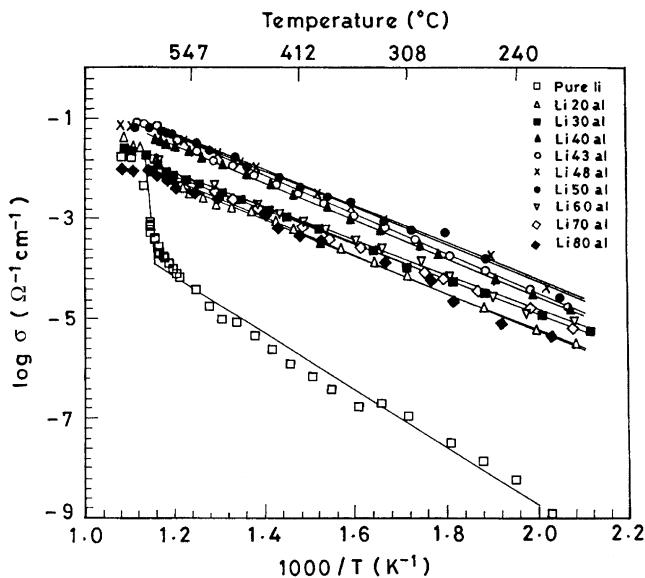


Fig. 4. Variation of log  $\sigma$  vs.  $1000/T$  for  $\text{Li}_2\text{SO}_4$ - $X$  m/o  $\text{Al}_2\text{O}_3$  ( $X = 0, 20, 30, 40, 43, 48, 50, 60, 70, 80$ ).

between 40 and 50 m/o  $\text{Al}_2\text{O}_3$  is about three orders of magnitude for this system. The conductivity plots in Fig. 4 exhibit an Arrhenius type behavior, and the activation energy derived from the slope of the log  $\sigma$  versus  $1000/T$  plot for the compositions vary between 0.74 and 0.83 eV. The activation energy for the composite is less than that of pure  $\text{Li}_2\text{SO}_4$ . However, it is independent of the alumina content, and is fairly constant. On the other hand, the preexponential factor, as a function of alumina content, exhibits a maximum for the 50 m/o  $\text{Al}_2\text{O}_3$  composition, the value for the preexponential factor being  $1.713 \times 10^6$ . Table 3 indicates the variation of activation energy and preexponential factor as a function of the composition of  $\text{Al}_2\text{O}_3$ .

The conductivity isotherms (Fig. 5) show a drop in conductivity beyond 50 m/o  $\text{Al}_2\text{O}_3$ . For low  $\text{Al}_2\text{O}_3$  containing compositions, the conductivity increases sharply

Table 2

m/o Dispersoid	$\sigma_{300} (\Omega^{-1} \text{ cm}^{-1})$	$\sigma_{500} (\Omega^{-1} \text{ cm}^{-1})$	$\sigma_{300}/\sigma_{\text{pure}}$	$\sigma_{500}/\sigma_{\text{pure}}$
Pure $\text{Li}_2\text{SO}_4$	$1.02 \times 10^{-7}$	$1.05 \times 10^{-5}$	1	1
20% $\text{Al}_2\text{O}_3$	$6.31 \times 10^{-5}$	$1.78 \times 10^{-3}$	617	170
30% $\text{Al}_2\text{O}_3$	$8.91 \times 10^{-5}$	$4.26 \times 10^{-3}$	871	407
40% $\text{Al}_2\text{O}_3$	$2.63 \times 10^{-4}$	$1.26 \times 10^{-2}$	2571	1202
43% $\text{Al}_2\text{O}_3$	$3.16 \times 10^{-4}$	$1.41 \times 10^{-2}$	3091	1349
48% $\text{Al}_2\text{O}_3$	$4.47 \times 10^{-4}$	$2.14 \times 10^{-2}$	4366	2042
50% $\text{Al}_2\text{O}_3$	$5.49 \times 10^{-4}$	$2.34 \times 10^{-2}$	5371	2239
60% $\text{Al}_2\text{O}_3$	$1.51 \times 10^{-4}$	$4.79 \times 10^{-3}$	1479	457
70% $\text{Al}_2\text{O}_3$	$1.02 \times 10^{-4}$	$3.24 \times 10^{-3}$	100	309
80% $\text{Al}_2\text{O}_3$	$6.30 \times 10^{-5}$	$2.57 \times 10^{-3}$	616	245

Table 3

Composition	$\sigma_0$ ( $\Omega^{-1} \text{ cm}^{-1}$ )	$E_a$ (eV)	Temperature range ( $^{\circ}\text{C}$ )
Pure $\text{Li}_2\text{SO}_4$	$3.3515 \times 10^7$	1.38	220–570
	$4.68 \times 10^2$	0.357	580–650
20% $\text{Al}_2\text{O}_3$	$7.764 \times 10^5$	0.845	220–570
30% $\text{Al}_2\text{O}_3$	$3.676 \times 10^5$	0.773	220–570
40% $\text{Al}_2\text{O}_3$	$1.876 \times 10^6$	0.808	220–570
43% $\text{Al}_2\text{O}_3$	$4.242 \times 10^6$	0.836	220–570
48% $\text{Al}_2\text{O}_3$	$1.483 \times 10^6$	0.76	220–570
50% $\text{Al}_2\text{O}_3$	$1.713 \times 10^6$	0.77	220–570
60% $\text{Al}_2\text{O}_3$	$2.242 \times 10^5$	0.744	220–570
70% $\text{Al}_2\text{O}_3$	$2.186 \times 10^5$	0.753	220–570
80% $\text{Al}_2\text{O}_3$	$2.260 \times 10^5$	0.783	220–570

with increasing alumina content. However, the rate of increase of conductivity decreases with a further increase in  $\text{Al}_2\text{O}_3$  content. The conductivity peak is a broad one, and there is no sharp jump in enhancement for any particular threshold  $\text{Al}_2\text{O}_3$  composition.

The decrease of conductivity at higher concentrations (>50 m/o) of  $\text{Al}_2\text{O}_3$  appears to be due to the “blocking effect”. Alumina itself is non-conducting. If a fraction,  $f$ , of the area of plane through the electrolyte consists of alumina, only a fraction  $(1 - f)$  is free to conduct, irrespective of any enhancement near an alumina particle, thereby accounting for the lower conductivity of the compositions containing greater than 50 m/o  $\text{Al}_2\text{O}_3$ .

To ascertain the mechanism for conductivity enhancement, different theoretical models were analyzed [6,28–30]. A higher conduction in the space charge layer near

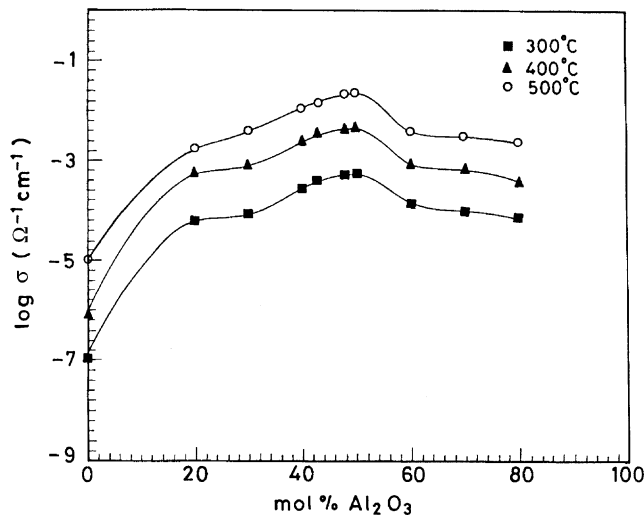


Fig. 5. Conductivity vs. composition isotherms for the  $\text{Li}_2\text{SO}_4\text{--Al}_2\text{O}_3$  composite system.



the surface appears as a possible mechanism for the ionic conductivity enhancement. This mechanism has been proposed in almost all the known models [6–14]. This conduction mechanism is quite possible, because at thermodynamic equilibrium most internal interfaces and free surfaces of an ionic crystalline material have some net charge. This charged interface is compensated with a diffuse layer containing an excess of the oppositely charged ionic defects. An enhanced conductivity is attributed to the excess concentration of point defects in the diffuse layer. Therefore, dispersed ionic conductors can be regarded as three component systems, because of their distinct interfacial properties. The resistor model [28] consists of non-conducting, normal conducting, and highly conducting bonds. The bonds are distributed in space in a manner that corresponds to a random distribution of insulating material in a normally conducting matrix, with a highly conducting interface separating them. The resistor model was mapped in the conventional manner on a random walk, which in turn, was solved by means of Monte Carlo simulations. According to this model, the normalized conductivity is given by the expression

$$\frac{\Sigma_{\max}}{\Sigma_0} = K \exp(\beta \Delta E) \quad (1)$$

with the value of  $\Delta E \approx 0.66$  eV.

The calculated conductivity values at various temperatures for the  $\text{Li}_2\text{SO}_4$ –50 m/o  $\text{Al}_2\text{O}_3$  composite using the resistor model are shown in Table 4.

The theoretical data as per the resistor model also appears to be in fair agreement with the experimental data confirming the existence of a highly conducting interface between the insulating alumina particles and the normally conducting lithium sulfate matrix.

Table 4

Temperature ( $^{\circ}\text{C}$ )	$\sigma$ or $\Sigma_{\max}$ (theoretical) ( $\Omega^{-1} \text{ cm}^{-1}$ )	$\log \sigma$ (theoretical)	$\log \sigma$ (experimental)
214	$5.99 \times 10^{-5}$	–4.22	–4.44
256	$2.62 \times 10^{-4}$	–3.582	–3.841
282	$4.91 \times 10^{-4}$	–3.309	–3.516
305	$8.16 \times 10^{-4}$	–3.088	–3.249
325	$1.23 \times 10^{-3}$	–2.91	–3.035
354	$2.12 \times 10^{-3}$	–2.674	–2.749
375	$3.042 \times 10^{-3}$	–2.517	–2.558
401	$4.612 \times 10^{-3}$	–2.336	–2.338
424	$6.487 \times 10^{-3}$	–2.188	–2.157
457	$1.02 \times 10^{-2}$	–1.993	–1.917
475	$1.278 \times 10^{-2}$	–1.893	–1.795
502	$1.761 \times 10^{-2}$	–1.754	1.623
524	$2.25 \times 10^{-2}$	–1.648	–1.491
552	0.03	–1.521	–1.334

#### 4. Conclusion

Composite solid electrolytes in the  $\text{Li}_2\text{SO}_4\text{--Al}_2\text{O}_3$  composite system, obtained by mechanochemical treatment of  $\text{Li}_2\text{SO}_4$  and fine sized  $\text{Al}_2\text{O}_3$ , have been investigated, and the highest conductivity is observed for the composite containing the  $\gamma\text{-Al}_2\text{O}_3$  phase. This has been attributed to the high surface activity of  $\gamma\text{-Al}_2\text{O}_3$ . Conductivity measurements show that the sintering time does not have a significant effect on the conductivity of the composite.

The composite containing 50 m/o  $\text{Al}_2\text{O}_3$  has the maximum conductivity, about three orders of magnitude higher than that of pure  $\text{Li}_2\text{SO}_4$ . The values of the conductivity for this composition are  $1.76 \times 10^{-2}$  and  $6 \times 10^{-5} \Omega^{-1} \text{cm}^{-1}$  at 500 and 200°C, respectively, with activation energy being  $0.78 \pm 0.05 \text{ eV}$ . A higher conduction in the space charge layer near the surface appears to be the possible mechanism for the enhancement in ionic conductivity.

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