# Selective Catalytic Reduction of NO by NH<sub>3</sub> over MoO<sub>3</sub> Promoted Fe<sub>2</sub>O<sub>3</sub> Catalyst<sup>1</sup>

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Abstract—A series of MoO<sub>3</sub> doped Fe<sub>2</sub>O<sub>3</sub> catalysts prepared by the co-precipitation method were investigated in the selective catalytic reduction of NO by NH<sub>3</sub> (NH<sub>3</sub>-SCR). The catalysts displayed excellent catalytic activity from 225 to 400°C and high tolerance to SO<sub>2</sub>/H<sub>2</sub>O poisoning at 300°C. To characterize the catalysts the N<sub>2</sub>-BET, XRD, Raman, NO-TPD, NH<sub>3</sub>-TPD and in situ DRIFTS were carried out. It was found that the main reason explaining a high NH<sub>3</sub>-SCR performance might be the synergistic effect between Fe and Mo species in the catalyst that could enhance the dispersion of Fe<sub>2</sub>O<sub>3</sub> and increase NH<sub>3</sub> adsorption on the catalyst surface.

*Keywords:* NO, NH<sub>3</sub>-SCR, MoO<sub>3</sub> modified catalysts, synergistic effect **DOI:** 10.1134/S002315841805018X

## **INTRODUCTION**

Nitrogen oxides  $NO_x$ , produced by the combustion of fossil fuel, could cause many environmental issues, such as acid rain, ozone depletion and photochemical smog [1, 2]. The selective catalytic reduction of NO by NH<sub>3</sub> (NH<sub>3</sub>-SCR) is the state-of-art technology for the NO<sub>x</sub> abatement. For the coal fired power plants, the  $V_2O_5$ -WO<sub>3</sub> (MoO<sub>3</sub>)/TiO<sub>2</sub> has been put into real application for many years due to its high  $De-NO_x$  efficiency and excellent tolerance to SO<sub>2</sub> poisoning. However, a narrow reaction temperature window of 300-400°C and the biological toxicity of vanadium species to the environment and human beings are some drawbacks of these catalysts [3, 4]. The development of the environmentally benign NH<sub>3</sub>-SCR catalyst that can maintain promising catalytic performance has received increased attention in recent years.

The investigation of iron based oxide catalysts remains an active area of research because these materials exhibit a high level of the NH<sub>3</sub>-SCR activity, high resistance to the SO<sub>2</sub> poisoning, environmentally friendly and relatively high redox properties. However, the NO conversion over pure Fe<sub>2</sub>O<sub>3</sub> is far from satisfactory at low temperatures since iron oxide shows a relatively low surface area and acidity. To improve its NH<sub>3</sub>-SCR performance, iron oxides have been doped with different promoters such as Fe–Ti [5], Fe–V [6], Fe–W [7, 8], Fe–Mn [9, 10], Fe–V–Ti [11] and Fe–Ce [12], all of which showed high NH<sub>3</sub>-SCR performance.

Alternatively,  $MoO_3$  has been used as a promoter to improve the NH<sub>3</sub>-SCR activity. MoO<sub>3</sub> modified  $CeAlO_x$  showed high denitration efficiency and the redox ability with the total acidity of the catalyst enhanced by the introduction of Mo [13]. It was found that by adding  $MoO_3$  into  $CeO_2/TiO_2$  it is possible not only to increase the population of Brønsted acid sites but also reduce the thermal stability of the inactive nitrate species on the catalyst surface [14]. Meanwhile, Ding et al. reported that the introducing Mo to Ce–Zr mixed oxide catalyst could inhibit the growth of the  $CeO_2$  particle size, improve the redox ability and increase the amount of surface Lewis acidity [15]. Based on the idea that iron based mixed oxide are highly active in the NH<sub>3</sub>-SCR and MoO<sub>3</sub> exerts a positive promoting effect of in the denitration reaction the MoO<sub>3</sub> we have initiated the synthesis of modified Fe<sub>2</sub>O<sub>3</sub> catalysts by co-precipitation method in order to compare the catalytic performance of these materials.

## EXPERIMENTAL

## Catalyst Preparation

MoO<sub>3</sub> modified Fe<sub>2</sub>O<sub>3</sub> catalysts were synthesized by the co-precipitation method using Fe(NO<sub>3</sub>)<sub>3</sub>  $\cdot$ 9H<sub>2</sub>O and (NH<sub>4</sub>)<sub>6</sub>Mo<sub>7</sub>O<sub>24</sub>  $\cdot$  5H<sub>2</sub>O as precursors and 25 wt % NH<sub>3</sub>  $\cdot$  H<sub>2</sub>O as precipitator. The aqueous solu-

mance under the conditions used in the catalytic testing. Therefore, it could be a good choice to introduce the suitable additive into the pure  $Fe_2O_3$  to enhance its NH<sub>3</sub>-SCR performance.

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tions of  $(NH_4)_6Mo_7O_{24} \cdot 5H_2O$  with equal weight  $H_2C_2O_4 \cdot 2H_2O$  were added to deionized water. After the  $(NH_4)_6 Mo_7O_{24} \cdot 5H_2O$  was dissolved completely, the  $Fe(NO_3)_3 \cdot 9H_2O$  was added into the aqueous solution with required molar ratio (Fe/Mo = 1 : 1, 2 : 1, 4 : 1 and 8 : 1). Excessive 25 wt %  $NH_3 \cdot H_2O$  solution was dropped into the mixed solution under vigorous agitation until pH 10. The precipitated solids were collected by filtration and washed with distilled water, followed by drying at 105°C for 12 h and subsequently calcination at 500°C for 5 h in the static air atmosphere. Finally, the catalyst pellets were crushed and sieved and an aliquot of the 40–60 mesh fraction was used in further experiments. For comparison purpose, pure  $Fe_2O_3$  and  $MoO_3$  were also prepared using the same synthetic method.

## Characterization of Catalysts

The specific surface area, pore volume and the average pore size of the samples were obtained by  $N_2$ adsorption/desorption at 77 K using a Micromeritics Tristar-3000 system (Micromeritics, US). The crystallinity of the catalysts were measured by means of powder XRD patterns obtained on a Rigaku D/max 2500 X-ray diffractometer (Rigaku, Japan) with  $CuK_{\alpha}$  radiation. Visible Raman spectra were registered at room temperature on a Spex 1877 D triplemate spectrograph (HORIBA Jobin Yvon, France) with spectral resolution of 2 cm<sup>-1</sup>. NO-TPD and NH<sub>3</sub>-TPD profiles were measured by the Autosorb-iQ-C chemisorption analyzer (Quantachrome Instruments, US). Prior to NO-TPD the sample was first pretreated in a flow of He at 400°C for 1 h and then cooled to 100°C. Afterwards, the sample was exposed to a flow of 500 ppm NO for 1 h, followed by He purge for 1 h. Finally, NO-TPD was run by heating the samples in He from 100 to  $600^{\circ}$ C at  $10^{\circ}$ C/min. In the case of NH<sub>3</sub>-TPD, the samples were pretreated at 400°C under He for 1h, then cooled to 50°C and saturated with 10% NH<sub>3</sub>/He for 1 h, followed by purging with He for 30 min. Finally, the samples were heated from 50 to 600°C at a rate of 10°C/min. The in situ DRIFTS experiments were performed on a Fourier transform infrared (FT-IR) spectrometer (Nicolet Nexus 670, (Nicolet, US) equipped with an in situ diffuse reflection chamber and high sensitivity mercury-cadmium-telluride (MCT) detector.

## Activity Test

A fixed bed reactor was used to evaluate the NH<sub>3</sub>-SCR activity. The flue composition was as follows: 500 ppm NO, 500 ppm NH<sub>3</sub>, 5% O<sub>2</sub>, 5 vol % H<sub>2</sub>O (when used), 100 ppm SO<sub>2</sub> (when used), N<sub>2</sub> flow into balance and a total flow rate of 500 mL/min. To maintain the GHSV at 50000 h<sup>-1</sup> a fixed volume of the catalyst (0.6 mL) was used. The concentrations of NO and NO<sub>2</sub> in the inlet and outlet gas were quantitatively measured with an online chemiluminescent  $NO/NO_x$ analyzer (KM9106, Kane Inc., UK) and the N<sub>2</sub>O concentration was analyzed by a gas chromatograph (FULI 9790, Zhejiang Wenling Inc., China) with a porapak Q column. NO conversion and N<sub>2</sub>O selectivity were calculated by using:

NO conversion = 
$$\frac{[NO_x]_{in} - [NO_x]_{out}}{[NO_x]_{in}} \times 100\%,$$
$$N_2O \text{ selectivity} = \frac{2[N_2O]_{out}}{[NO_x]_{in} - [NO_x]_{out}} \times 100\%,$$
$$[NO_x] = [NO] + [NO_2].$$

### **RESULTS AND DISCUSSION**

## Activity Test

The NO conversion and N<sub>2</sub>O selectivity in the selective catalytic reduction of NO by NH<sub>3</sub> as a function of temperature over Fe<sub>2</sub>O<sub>3</sub>, MoO<sub>3</sub> and MoO<sub>3</sub> modified  $Fe_2O_3$  catalysts are shown in Fig. 1. It can be readily seen that pure MoO<sub>3</sub> exhibited negligible SCR activity and N<sub>2</sub>O selectivity over the whole temperature range. Pure Fe<sub>2</sub>O<sub>3</sub> also showed poor NH<sub>3</sub>-SCR catalytic performance with the maximum NO conversion at 250°C not exceeding 32.6%. However, the NH<sub>3</sub>-SCR activity could be improved markedly upon adding  $MoO_3$  to  $Fe_2O_3$ . At the Fe/Mo molar ratio = 1 : 1, more than 40% of NO was converted and  $N_2O$ selectivity below 5% was achieved in the temperature range from 250 to 450°C. When the Fe/Mo molar ratio reached a value of 2: 1, the SCR activity and N<sub>2</sub>O selectivity was further improved over the whole temperature range used in the test. When the Fe/Mo molar ratio was increased to 4 : 1, the highest activity was attained in the tested temperature range, with the NO conversion >90% and N<sub>2</sub>O selectivity <5%. However, further increasing the Fe/Mo molar ratio decreased the NO conversion at both low and high temperatures. Therefore, the activity was probably associated with the Fe/Mo molar ratio and the optimal ratio was 4 : 1.

For the purposes of evaluating the anti-poisoning tolerance to SO<sub>2</sub> and H<sub>2</sub>O, the Fe<sub>4</sub>MoO<sub>x</sub> catalyst was selected to investigate the impact of 100 ppm SO<sub>2</sub> and/or 5 vol % H<sub>2</sub>O on its catalytic performance at 300°C with the corresponding results collected in Fig. 2. It could be seen that the Fe<sub>4</sub>MoO<sub>x</sub> catalyst maintained nearly 100% NO conversion during the tested period in the present of 5 vol % of H<sub>2</sub>O. When 100 ppm of SO<sub>2</sub> was injected into the reaction gases, the NO conversion decreased and gradually became stable. The NO conversion was recovered after removing SO<sub>2</sub>. As the 100 ppm of SO<sub>2</sub> and 5 vol % H<sub>2</sub>O were introduced into the reaction gases synchronously, the NO conversion decreased much more markedly,



**Fig. 1.** NH<sub>3</sub>-SCR activity (a) and N<sub>2</sub>O selectivity (b) as function of temperature over Fe<sub>2</sub>O<sub>3</sub>, MoO<sub>3</sub> and MoO<sub>3</sub> modified Fe<sub>2</sub>O<sub>3</sub> catalysts (■ Fe : Mo = 1 : 1, ● Fe : Mo = 2 : 1, ▲ Fe : Mo = 4 : 1, ▼ Fe : Mo = 8 : 1, ◄ Fe<sub>2</sub>O<sub>3</sub>, ► MoO<sub>3</sub>) under GHSV of 50000 h<sup>-1</sup>.

which could be attributed to the presence of  $NH_4HSO_4$  deposited on the catalyst surface [15]. However, the NO conversion exceeded values of 89% during the tested period. All these results suggest that the catalyst showed an adequate tolerance to  $SO_2/H_2O$  poisoning.

## **BET Result**

The BET physical property parameters of the  $Fe_2O_3$ ,  $MoO_3$  and Mo modified  $Fe_2O_3$  catalysts are summarized in Table. It could be found that the BET surface area and pore volume of the Fe–Mo mixed oxide increased at first and then decreased with



**Fig. 2.** NH<sub>3</sub>-SCR activity over Fe<sub>4</sub>MoO<sub>x</sub> catalyst in the presence of H<sub>2</sub>O/SO<sub>2</sub>: (a) 5% H<sub>2</sub>O, ▲; (b) 100 ppm SO<sub>2</sub>, ■; (c) 5% H<sub>2</sub>O + 100 ppm SO<sub>2</sub>, ▼. At 300°C under GHSV of 50000 h<sup>-1</sup>.

increasing Fe/Mo molar ratio remaining however much larger than those found for pure  $Fe_2O_3$  and MoO<sub>3</sub>. This trend was also consistent with the variations in the NO conversion over the temperature range of 250–450°C. However, reductions in the average pore diameter associated with the addition of MoO<sub>3</sub> into the Fe<sub>2</sub>O<sub>3</sub> catalyst cannot be correlated with the amount of the dopant. It could be therefore implied that the catalyst structural parameters are hardly the key factors determining the NH<sub>3</sub>-SCR activity. Combining the NH<sub>3</sub>-SCR performance and BET analysis results, it also could be suggested that incorporation of Mo into Fe oxide results in the formation of MoO<sub>3</sub> promoted Fe<sub>2</sub>O<sub>3</sub> catalysts with properties different from a mechanical mixture of two oxides.

#### XRD and Raman Analysis

The presence of crystal phase of  $Fe_2O_3$  in the  $MoO_3$ modified  $Fe_2O_3$  catalyst is confirmed by X-ray diffraction study (Fig. 3a). XRD patterns of all samples show characteristic broad peaks at 24.3°, 33.4°, 35.8°, 41.1°, 49.6°, 54.2°, 57.8°, 62.7°, 64.2°, 72.3° and 75.6° (2 $\theta$ ) corresponding to the typical Hematite-Fe<sub>2</sub>O<sub>3</sub> (PDF33-0664). At the same time, no characteristic diffraction peaks of MoO<sub>3</sub> were observed. A weak crystallization or a good dispersion on the MoO<sub>3</sub> modified Fe<sub>2</sub>O<sub>3</sub> surface may be a reason. Table 1 shows the crystallite sizes of Hematite-Fe<sub>2</sub>O<sub>3</sub> in the tested catalysts calculated by using the Scherrer equa-

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Sample	BET surface area, m²/g	BJH pore volume, cm <sup>3</sup> /g	Average pore size, nm	Crystallite size of $Fe_2O_3^*$ , nm
Fe <sub>2</sub> O <sub>3</sub>	42.4	0.23	17.1	22.7
FeMoO <sub>x</sub>	64.9	0.36	10.3	19.6
$Fe_2MoO_x$	73.2	0.45	13.2	17.5
$Fe_4MoO_x$	82.7	0.58	14.4	14.1
$Fe_8MoO_x$	76.2	0.49	21.6	15.1
MoO <sub>3</sub>	1.6	0.02	45.8	_

**Table 1.** The BET physical parameters of the MoO<sub>3</sub> modified Fe<sub>2</sub>O<sub>3</sub> catalysts

\*Fe<sub>2</sub>O<sub>3</sub> crystallite size calculated by Scherrer equation from XRD results.

tion. The data indicate variations in the crystallite dimensions of the catalyst samples prepared with different Fe/Mo molar ratio. The lower Hematite-Fe<sub>2</sub>O<sub>3</sub> crystallite sizes were registered for the Fe<sub>2</sub>O<sub>3</sub> catalysts containing increased amounts MoO<sub>3</sub>. It can be thus inferred that the incorporation of molybdenum oxide decreases the crystallite size of Fe<sub>2</sub>O<sub>3</sub> thus enhancing the dispersion of Fe<sub>2</sub>O<sub>3</sub> on the catalyst surface.

For the purposes of further understanding of the structural characteristics, Raman spectroscopy was also employed with the corresponding results collected in Fig. 3b. As can be seen, the spectrum of MoO<sub>3</sub> showed nine Raman bands at 116, 129, 158, 284, 337, 378, 665, 819 and 995 cm<sup>-1</sup> [16, 17]. In the spectrum of Fe<sub>2</sub>O<sub>3</sub> four bands at 215, 281, 391 and  $587 \text{ cm}^{-1}$  could be observed assignable to hematite with small differences in peak positions ( $\pm 5 \text{ cm}^{-1}$ ) [18]. The band at  $215 \text{ cm}^{-1}$  is due to the Raman active  $A_{1g}$  mode of hematite and three peaks at 281, 391 and 587 cm<sup>-1</sup> are ascribed to  $E_g$  modes of hematite [19]. No MoO<sub>3</sub> species were detected in the Fe–Mo based catalysts. In addition, the band intensities due to  $Fe_2O_3$  on Fe–Mo mixed oxides decreased, indicating that doping with Mo inhibited the crystallization of  $Fe_2O_3$  phase. Given that crystalline MoO<sub>3</sub> could be otherwise easily detected on the catalyst surface by using Raman spectrum, the absence of the signals corresponding to  $MoO_3$  crystalline phase on the  $MoO_3$ modified Fe<sub>2</sub>O<sub>3</sub> catalysts suggests a high degree of dispersion of MoO<sub>3</sub> species on the catalyst surface. The corresponding analytical data are in good agreement with the XRD results.

## NO-TPD and NH<sub>3</sub>-TPD Analysis

The NO adsorption on the  $Fe_2O_3$ ,  $MoO_3$  and  $Fe_4MoO_x$  catalysts was characterized by using NO-TPD with the corresponding results presented in Fig. 4a.  $Fe_2O_3$  and  $Fe_4MoO_x$  had two desorption peaks, whereas for  $MoO_3$  no peak was observed in the spectra. Desorption peaks at 210°C for  $Fe_4MoO_x$  and

 $245^{\circ}$ C for Fe<sub>2</sub>O<sub>3</sub> can be ascribed to the decomposition of bridging nitrate. Desorption peaks at 307°C for  $Fe_4MoO_x$  and  $347^{\circ}C$  for  $Fe_2O_3$  are assigned to the decomposition of monodentate nitrate [17]. It appears that only sites associated with iron atoms are available for adsorption of NO over these three catalysts and the addition of  $MoO_3$  on the  $Fe_4MoO_x$  could inhibit the formation of nitrate species to a certain degree. The inhibition may be related to a reduced thermal stability of the inactive nitrate specie on the catalyst surface [14]. Although adsorption power of the  $Fe_4MoO_r$ towards NO is weaker than that of the pure  $Fe_2O_3$ , doping with Mo markedly improved the NH<sub>3</sub>-SCR activity. The above results imply that some synergetic effect between Mo and Fe species might exist in the catalyst and make a material contribution to the improvement of the NH<sub>3</sub>-SCR performance.

The amount of acid sites on the catalyst surface plays a crucial role in the NH<sub>3</sub>-SCR performance. The acid content on the catalysts surface is characterized by using NH<sub>3</sub>-TPD with the corresponding profiles shown in Fig. 4b. It can be seen that the desorption curve for the Fe<sub>2</sub>O<sub>3</sub> catalyst has two main peaks at 107 and 368°C. The peak at 107°C can be assigned to the weakly adsorbed  $NH_3$ , the peak at 368°C can be attributed to the strongly adsorbed NH<sub>3</sub> and the total acidity of the Fe<sub>2</sub>O<sub>3</sub> catalyst was ~9.37  $\mu$ mol g<sup>-1</sup>m<sup>-2</sup>. Notably, the intensity of the  $Fe_4MoO_x$  desorption peak was enhanced significantly by doping with Mo. The peak due to the strongly adsorbed NH<sub>3</sub> at 368°C was shifted at 409°C and the total acidity was increased to about 13.84  $\mu$ mol g<sup>-1</sup>m<sup>-2</sup>. An explanation can be offered that ammonia was coordinatively bound to Mo surface cation species or protonated as  $NH_4^+$  by interacting with Mo–OH groups on the catalyst surface [21]. It seems that the increase in the surface acidity is a key factor contributing to the improvement of the NH<sub>3</sub>-SCR activity.



**Fig. 3.** (a) XRD profiles of the catalysts: (1)  $Fe_2O_3$ , (2)  $FeMoO_x$ , (3)  $Fe_2MoO_x$ , (4)  $Fe_4MoO_x$ , (5)  $Fe_8MoO_x$ . (b) Raman spectra of the catalysts: (1)  $Fe_2O_3$ , (2)  $FeMoO_x$ , (3)  $Fe_2MoO_x$ , (4)  $Fe_4MoO_x$ , (5)  $Fe_8MoO_x$ , (6)  $MoO_3$ , ( $\lambda_{ex} = 514.5$  nm).

### In situ DRIFTS Results Analysis

The in situ DRIFTS analysis was performed to study NH<sub>3</sub> adsorption and NO + O<sub>2</sub> adsorption on the MoO<sub>3</sub>, Fe<sub>2</sub>O<sub>3</sub> and Fe<sub>4</sub>MoO<sub>x</sub> catalysts at 200°C. According to the in situ DRIFTS information shown in Fig. 5, no bands could be observed after adsorption of NH<sub>3</sub> or NO + O<sub>2</sub> on the surface of MoO<sub>3</sub>. When the sample of Fe<sub>2</sub>O<sub>3</sub> was exposed to NH<sub>3</sub>, several bands appeared at 1205, 1429, 1602, 3160, 3255, 3347, 3579, 3648 and 3724 cm<sup>-1</sup>. The band at 1205/1602 cm<sup>-1</sup> could be attributed to NH<sub>3</sub> coordinatively bound to Lewis acid sites [21, 22], while the band at 1420 cm<sup>-1</sup>



**Fig. 4.** NO-TPD (a) and NH<sub>3</sub>-TPD (b) profiles of  $Fe_2O_3$ , MoO<sub>3</sub>, and  $Fe_4MoO_x$ .

can be assigned to ionic NH<sub>4</sub><sup>+</sup> species on Brønsted acid sites [6]. The bands at 3160, 3255 and 3347  $cm^{-1}$  due to N-H stretching vibration modes and three negative bands at 3579, 3648 and 3724  $cm^{-1}$  caused by the surface O-H stretching were also observed [23-27]. After introducing  $NH_3$  to the  $Fe_4MoO_x$  sample, the band attributable to ionic  $NH_4^+$  species disappeared. However, the affinity of Lewis acid sites to NH<sub>3</sub> molecules strengthened evidently. In the N-H stretching region, three new bands were found at 3162, 3265 and 3349 cm<sup>-1</sup>. In addition, another three negative bands appeared at 3632, 3655 and 3720 cm<sup>-1</sup>, which could be assigned to absorption of hydroxyl groups. The NH<sub>3</sub> adsorption results were consistent with the NH<sub>3</sub>-TPD testing data. After introducing NO +  $O_2$  into the DRIFT cell, some bands appeared at 1203, 1215, 1350, 1548, 1566, 1595 and 1597  $cm^{-1}$ . The bands at 1203

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(a)



Fig. 5. In situ DRIFTS of NH<sub>3</sub> adsorption (a), NO +  $O_2$  adsorption (b) on the Fe<sub>2</sub>O<sub>3</sub>, MoO<sub>3</sub>, and Fe<sub>4</sub>MoO<sub>x</sub> catalyst at 200°C.

and 1350 cm<sup>-1</sup> were assigned to chelated NO<sub>2</sub><sup>-</sup> and chelating nitrites, respectively [28, 29]. The bands at 1215, 1595 and 1597 cm<sup>-1</sup> are due to bridging nitrate species [30, 31], the bands attributable to monodentate nitrate were also found at 1548 and 1566 cm<sup>-1</sup> [22, 32]. The intensity of the bands on the Fe<sub>4</sub>MoO<sub>x</sub> catalyst was slightly compared to those of Fe<sub>2</sub>O<sub>3</sub> in agreement with the NO-TPD results. From the above analysis, the development of a certain synergistic effect between Fe and Mo species in the MoO<sub>3</sub> modified

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 $Fe_2O_3$  catalysts can be postulated, which could strengthen the adsorption power of the catalyst surface to NH<sub>3</sub> and in this way enhance the de-NO<sub>x</sub> activity.

In conclusion,  $MoO_3$  modified  $Fe_2O_3$  catalysts prepared by conventional co-precipitation method exhibited excellent  $NH_3$ -SCR activity over a relatively wide temperature range from 225 to 400°C and strong resistance to  $SO_2$  and  $H_2O$  poisoning. The existence of the synergistic effect between Fe and Mo species in the  $MoO_3$  modified Fe<sub>2</sub>O<sub>3</sub> catalyst was crucial for achieving an improved NH<sub>3</sub>-SCR performance.

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