which gave the approximate relationship  $\delta(\Delta_1 r) = -9\delta l$ . None of the refined values of the other parameters in Tables I and II were found to be very sensitive to the remaining assumptions. The bracketed values for the three difference parameters in Table I were obtained from molecular-mechanics calculations and that for C=C-H is similar to values in other molecules. Small changes in any of these quantities should not significantly affect the refinement results.

The two sets of results in Table I are in pleasing agreement and are each fair statements of the COD structure. We choose the set based on the OSU data as our preferred model because of the way in which the backgrounds were removed to generate the molecular intensities on which the refinements were based: the computer-generated backgrounds used with the OSU data are presumably less subject to bias than are the hand-drawn backgrounds used with the Oslo data. Table II is a more complete set of distances and amplitudes for the preferred model, and Table III is an abbreviated correlation matrix.

## Discussion

As may be seen from Table IV, our structure for COD agrees well with the results of molecular-mechanics calculations, particularly those of Ermer<sup>7</sup> and Anet and Kozerski.<sup>18</sup> Table IV also shows that the conformation of the COD ring is not affected by the presence of pseudoequatorial substituents: the ring parameters of the two COD derivatives have values very similar to those for COD itself.

The carbon-carbon bond lengths in COD are quite similar to those found in aliphatic chains and in other low-strain ring systems. They require no special comment. The two types of bond angles (those adjacent and those not adjacent to the double bonds) are a few degrees larger than their open-chain counterparts, presumably mostly as a consequence of cross-ring repulsions which tend to flatten the carbon skeleton. The twisted-boat conformation adopted by the molecule is also consistent with an important role for repulsive interactions. For example, in both the chair and symmetric-boat forms vicinally situated pairs of carbon atoms are eclipsed, as are pairs of hydrogen atoms on adjacent methylene groups. The strains arising from these energetically unfavorable geometries are par-

(18) Anet, F. A. L.; Kozerski, L., private communication.

tially relieved in the twisted boat. Quantitative evidence for this qualitative picture is available from the molecular-mechanics calculations,<sup>7,8</sup> especially those of Ermer where the individual components of the potential are tabulated for several conformations of the molecule. The twisted-boat form was found to be lower in potential energy than the regular boat by 7 kcal/mol and the chair by 4 kcal/mol. The calculations are also consistent with our conclusion that large-amplitude torsional vibration is not present in COD, a crude estimate based upon the potential-energy profiles for twisting suggesting that more than 85% of the molecules are to be found within 15° of the equilibrium values of  $\angle C_3 - C_4 - C_5 = C_6$  and  $\angle C_2 - C_3 - C_4 - C_5$ .

Our final remarks concern the possible presence of other conformers in our gaseous samples. Although our tests for the chair form were negative, they can only be interpreted as ruling out substantial amounts of that form. When small amounts of chair were included in compositionconstrained calculations, the structural results and agreement with experiment did not differ significantly from those obtained with the twisted boat as the only form present. From these calculations we estimate that more than about 10% of the chair in our samples would be incompatible with the electron-diffraction data but that smaller amounts cannot be excluded. Although forms other than the chair were not tested, the same statements may be assumed to apply to them. These conclusions are consistent with the free energies of formation calculated from molecular mechanics which, for example, in the case of the chair and twisted-boat forms, corresponds to only about 1% of the former in an equilibrium mixture.

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Supplementary Material Available: Tables of the leveled total intensities (Table V), calculated backgrounds (Table VI), average curves from each camera distance (Table VII), symmetry coordinates (Table VIII), and observed and calculated wave numbers (Table IX) (23 pages). Ordering information is found on any current masthead page.

# Rate Constant and Possible Pressure Dependence of the Reaction $OH + HO_2$

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The technique of laser-induced fluorescence has been used to measure steady-state OH concentrations in the photolysis of water vapor at 184.9 nm and 298 K, with  $O_2$  added in trace amounts. He or Ar was present at total pressures in the range 75–730 torr. The results were used to derive the rate-constant ratio  $k_1/k_5^{1/2}$ , where  $k_1$  and  $k_5$  are the rate constants for the reactions OH + HO<sub>2</sub>  $\rightarrow$  H<sub>2</sub>O + O<sub>2</sub> and HO<sub>2</sub> + HO<sub>2</sub>  $\rightarrow$  O<sub>2</sub>, respectively. When currently available values for  $k_5$  are used, the results give  $k_1 = (1.2 \pm 0.4) \times 10^{-10}$  cm<sup>3</sup> s<sup>-1</sup> at 1-atm pressure, with evidence of a decline of  $k_1$  at lower pressures. No water-vapor effect on  $k_1$  was observed.

#### Introduction

Reliable measurement of the rate constant for the reaction

$$OH + HO_2 \xrightarrow{k_1} H_2O + O_2 \tag{1}$$

has been a long-standing problem in kinetics.<sup>1-4</sup> The

difficulty in measuring this rate is related to several factors, such as the radical-radical nature of the reaction, the problem of monitoring the radical concentrations (especially  $HO_2$ ), and the tendency of the reactants to undergo complicating side reactions or self-reactions. The situation is further complicated by the possibility that this reaction, usually assumed to be strictly bimolecular, may proceed by a complex mechanism involving an intermediate adduct such as  $H_2O_3$ <sup>2,5</sup> This question is referred to later in the Discussion section dealing with possible pressure dependence of the reaction.

Earlier measurements of  $k_1$  in low-pressure systems (i.e., a few torr) have fallen in the range of about  $3 \times 10^{-11}$  cm<sup>3</sup>  $s^{-1}$  (ref 6 and 7) to 5.1 × 10<sup>-11</sup> cm<sup>3</sup> s<sup>-1</sup> (ref 8). However, more recent results under these conditions by Keyser<sup>9</sup> have given the somewhat higher value of  $6.5 \times 10^{-11}$  cm<sup>3</sup> s<sup>-1</sup>. By contrast, measurements near 1 atm<sup>3,4,10-13</sup> have consistently yielded  $k_1$  values of  $\geq 1 \times 10^{-10}$  cm<sup>3</sup> s<sup>-1</sup>. This discrepancy has led to the suggestion<sup>4</sup> of a possible pressure dependence for the reaction. However, additional systematic studies of the possible pressure dependence are needed.

The present work has had two principal objectives: first, to obtain further measurements of  $k_1$  at pressures near 1 atm, and, second, to examine the pressure dependence. The experiments involved steady-state photolysis of H<sub>2</sub>O in the presence of a small amount of  $O_2$ , under which conditions  $[OH]_{ss}$  is sensitive to  $k_1$ . The  $[OH]_{ss}$  was measured by laser-induced fluorescence, which was calibrated on an absolute basis.

# **Experimental Methods**

Mechanism. The basic photochemical mechanism used in these experiments can be given as follows:

$$H_2O \xrightarrow{184.9 \text{ nm}} H + OH$$
 (2)

$$H + O_2 + M \rightarrow HO_2 + M$$
(3)

$$OH + HO_2 \rightarrow H_2O + O_2 \tag{1}$$

 $OH \rightarrow products$ (4)

$$\mathrm{HO}_{2} + \mathrm{HO}_{2} \rightarrow \mathrm{H}_{2}\mathrm{O}_{2} + \mathrm{O}_{2} \tag{5}$$

$$OH + H_2O_2 \rightarrow H_2O + HO_2$$
 (6)

Addition of  $H_2$  in measured concentrations served to convert OH to  $HO_2$ , by reaction 7 followed by reaction 3.

$$OH + H_2 \rightarrow H_2O + H \tag{7}$$

This has the effect of changing the  $OH/HO_2$  ratio, and introduces a variable but controllable first-order OH loss

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rate which can be made to dominate reaction 4.

The rate constant  $k_4$  represents the effective first-order loss of OH by several possible paths, including reaction with trace impurities and diffusive loss to the walls. In the calibration procedure (described later), it was found that  $k_4$  usually was in the range 3-5 s<sup>-1</sup>. Radical-radical reactions (with  $HO_2$  absent) are not fast enough to account for these rates under the conditions of the experiments, although the reactions

$$OH + OH + M \rightarrow H_2O_2 + M \tag{8}$$

$$OH + OH \rightarrow H_2O + O \tag{9}$$

could give loss rates approaching 1 s<sup>-1</sup> at the highest OH concentrations used, about 10<sup>11</sup> cm<sup>-3</sup>. It is believed that  $k_4$  was due mainly to reaction of OH with hydrogenous impurities in the reaction mixtures. Hydrocarbon impurities of a few tenths of a ppm would be adequate, assuming a rate constant for reaction with OH of about 10<sup>-12</sup>  $cm^3 s^{-1}$ . Diffusive loss was relatively unimportant, except possibly at the lowest pressures used. With added  $H_{2}$ , first-order loss of OH by reaction 7 dominated  $k_4$  in many of the experiments, with no effect on the results. Thus, the precise nature of  $k_4$  is not critical to the interpretation of the results.

To produce HO<sub>2</sub> in the mixtures, oxygen was added at pressures in the range of about 0.1-0.3 torr, which was found to be sufficient to convert all H into  $HO_2$  by reaction 3. The effect of increasing conversion of H to  $HO_2$  upon addition of  $O_2$  could be seen by monitoring the OH signal as O<sub>2</sub> was added, showing a rapid fall in [OH] due to the appearance of  $HO_2$ . The [OH] eventually leveled off at a constant value when the scavenging of H was complete, and additional  $O_2$  had no further effect. Because of the low  $O_2$  cross section at 184.9 nm compared to that of  $H_2O$ (factor of 7),<sup>3</sup> these small  $O_2$  pressures did not affect the OH concentration by the processes

$$O_2 + 184.9 \text{ nm} \rightarrow O + O$$
 (10)

$$0 + 0H \rightarrow 0_{2} + H \tag{11}$$

$$0 + HO_2 \rightarrow OH + O_2 \tag{12}$$

Further, the  $O_2$  quenching rate for OH fluorescence is not large enough compared to that of  $H_2O$  to affect the fluorescence efficiency,<sup>14,15</sup> as was verified in the present work.

Both experiment and computer simulation (discussed later) showed that reaction 6 can be neglected on the time scale over which the [OH]<sub>ss</sub> measurements were made, which was about 5 s after onset of photolysis. This is because of the relatively slow rate of  $H_2O_2$  formation in the mixture, combined with the known rate constant<sup>16,17</sup> for reaction 6 which is considerably slower than the rate constant for reaction of OH with HO<sub>2</sub>.

Steady-state considerations show that

$$(k_4 + 2k_7[H_2])[OH]_{ss} = 2k_5[HO_2]_{ss}^2$$
(13)

because loss of OH by reaction 4 and 7 must be balanced by loss of  $HO_2$  through reaction 5.

Additionally, the steady-state OH concentration is given bv

$$[OH]_{ss} = I_{a}^{H_{2}O} / (k_{4} + k_{1}[HO_{2}]_{ss} + k_{7}[H_{2}])$$
(14)

where  $I_{a}^{H_{2}O}$  is the rate of H<sub>2</sub>O photolysis.

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Figure 1. Schematic of apparatus.

Combination of eq 13 and 14 yields the following relationship between the measured steady-state OH concentrations and the rate constants  $k_1$  and  $k_5$ :

$$\frac{k_1}{k_5^{1/2}} = \frac{I_a^{H_2O} - (k_4 + k_7[H_2])[OH]_{ss}}{[OH]_{ss}^{3/2} \left[\frac{k_4 + 2k_7[H_2]}{2}\right]^{1/2}}$$
(15)

In the application of eq 15,  $[H_2]$  was varied, but conditions were always chosen such that  $I_a^{H_2O} \gg k_7[H_2][OH]_{ss}$ . This was to ensure that most of the OH reacted with HO<sub>2</sub> rather than with H<sub>2</sub>, which thereby retained a high sensitivity of  $[OH]_{ss}$  to  $k_1$ . This condition was possible because  $k_4$  was small.

 $I_a^{H_2O}$  was calculated from the expression

$$I_{a}^{H_{2}O} = I_{0}\sigma_{H_{2}O}n_{H_{2}O}$$
(16)

where  $I_0$  is the 184.9-nm intensity (quanta cm<sup>-2</sup> s<sup>-1</sup>),  $\sigma_{H_2O}$ is the cross section for H<sub>2</sub>O at 184.9 nm (7.8 × 10<sup>-20</sup> cm<sup>2</sup>),<sup>3</sup> and  $n_{H_2O}$  is the H<sub>2</sub>O concentration in particles cm<sup>-3</sup>. The quantity  $I_0$  was determined actinometrically by measuring the rate of O<sub>2</sub> photolysis to produce O<sub>3</sub> in small quartz cells which were placed inside the fluorescence cell. Corrections for window absorption were made on the basis of measured absorbances of the empty cells and the assumption of equal absorbances by the front and back windows. The resulting corrections were in the range of 15–20%. Results in cells of path lengths 1 and 5 cm were identical to within 5%, suggesting reasonable uniformity of light intensity. Thus

$$I_{a}^{O_{2}} = \frac{1}{2} \frac{\Delta[O_{3}]}{\Delta t} = I_{0} \sigma_{O_{2}} n_{O_{2}}$$
(17)

where  $\sigma_{O_2} = 1.08 \times 10^{-20} \text{ cm}^{2.3}$  The actual absorbed light intensities were in the range  $1 \times 10^{11}$ – $7 \times 10^{11}$  quanta cm<sup>-2</sup> s<sup>-1</sup>, depending on the H<sub>2</sub>O pressure used. It should be pointed out that the results are sensitive only to approximately the square root of  $I_a^{\text{H}_2\text{O}}$ , because the quantity  $[\text{OH}]_{\text{as}}$  in eq 15 is proportional to  $I_a^{\text{H}_2\text{O}}$ .

Apparatus. A schematic diagram of the apparatus is shown in Figure 1. The carrier gases He or Ar were passed through an H<sub>2</sub>O bubbler which was temperature controlled in order to establish the desired H<sub>2</sub>O pressure. The carrier gases were HP or GC grades and, in some cases, were first passed through a Matheson Hydrox purifier to remove traces of O<sub>2</sub>, followed by a molecular sieve trap at -78 or -196 °C to minimize other impurities. Total pressure ranged from 75 to 730 torr, with water pressures of 1-5 torr. Flow rates were varied but usually were near 300 sccm, corresponding to cell flushing times of 1-2 min. Flow rates were measured by means of calibrated flowmeters (Hastings-Teledyne), and cell pressures were monitored with a calibrated Baratron gauge. The photolysis source was a low-pressure mercury lamp, combined with a 184.9-nm interference filter to limit radiation to that wavelength. Gases such as  $O_2$  or the calibrating gases  $H_2$ and  $CH_4$  were added to the flowing stream from bulb reservoirs. Two fluorescence cells were used; one was of stainless steel coated on the inside with Teflon, and the other was of uncoated Pyrex. Each cell had Suprasil quartz windows for the laser beam and for the fluorescence signal. The object of using two cell types was to test for possible surface effects. The cells were approximately cylindrical, with diameter 10 cm and depth 10 cm.

The laser-induced fluorescence system was similar to that previously described by Davis and co-workers.<sup>18</sup> The fluorescence excitation source was a dye laser (Quantel TDL-111) pumped by a Quantel 481a Nd:YAG laser. The system was operated at 10 pulses s<sup>-1</sup> with an average pulse energy of  $0.425 \pm 0.025$  mJ pulse<sup>-1</sup>. The pulse width was 7 ns. Pulse energies were monitored with a Laser Precision Corp. meter, type Rj-7100. The laser beam width was approximately 2 mm.

To minimize background signal arising from source scatter, the Q<sub>1</sub>(1) line near 281.9 nm in the  ${}^{2}\pi(v''=0) \rightarrow$  ${}^{2}\Sigma(v'=1)$  system was excited and nonresonant emission near 309 nm ( $v'' = 0 \rightarrow v' = 0$ ) was observed. As illustrated in Figure 1, an optical collection system consisting of two 5-cm focal length quartz lenses was used to focus an image of the fluorescence beam onto the face of the photomultiplier tube (EMI 9659). A slit on the face of the photomultiplier tube limited the transmitted radiation to that of the beam image. An interference filter with transmission centered at 309 nm was used to minimize background fluorescence. The photomultiplier output was observed with a Tektronix 475 oscilloscope, and the intensity was measured with a PAR 162 boxcar analyzer, equipped with the Model 165 integrator module. A gate width of 15 ns was used.

The background fluorescence signal with zero OH concentration was about 1% of the maximum signal obtained for  $[OH] \sim 10^{11}$  cm<sup>-3</sup>. The background signal was found to vary somewhat, depending mainly on how long the photolytic lamp had been on. This is believed to be due to cleaning up of wall contaminants (by OH) which fluoresce upon absorption of scattered laser light.

# Results

Calibration of the Fluorescence Signal. Absolute OH concentrations were determined by use of a calibration factor relating concentration to fluorescence intensity

$$[OH] = \alpha(cm^{-3} mV^{-1}) \times S(mV)$$
(18)

where S was the observed boxcar signal in mV for a given OH concentration. A linear relationship between OH concentration and fluorescence signal was verified in the calibration procedure, which involved addition of known concentrations of the calibrating gas, G (usually CH<sub>4</sub> or H<sub>2</sub>), to the photolysis of H<sub>2</sub>O in pure carrier gas. Thus

$$[OH]_{ss}^{cal} = I_a^{H_2O} / (k_4 + k_G[G])$$
(19)

where [G] is the concentration of calibrating gas and  $k_{\rm G}$  is the rate constant for the reaction of OH with the gas G. Combined with eq 18, the following linear relationship

<sup>(18)</sup> D. D. Davis, W. S. Heaps, D. Philen, M. Rodgers, T. McGee, A. Nelson, and A. J. Moriarty, *Rev. Sci. Instrum.*, **50**, 1505 (1979).



Figure 2. Example of calibration data.

is predicted for the reciprocal of the fluorescence intensity and [G]:

$$1/S = (\alpha/I_a^{H_2O})(k_G[G] + k_4)$$
(20)

Thus, a plot of 1/S vs. [G] yields  $\alpha$  from the slope and  $k_4$  from the intercept.

Figure 2 shows an example of calibration data for a mixture with 400 torr of He and 5 torr of H<sub>2</sub>O, with added CH<sub>4</sub> and H<sub>2</sub>. As predicted from eq 20, the reciprocal of the fluorescence signal was found to be linear with concentration (pressure) of the added gas. Furthermore, the ratio of slopes (0.91) was found to agree very well with recommended rate constants<sup>19</sup> for the reactions of OH with H<sub>2</sub> and CH<sub>4</sub>,  $k_{\rm H_2} = 7.1 \times 10^{-15}$  cm<sup>3</sup> s<sup>-1</sup> and  $k_{\rm CH_4} = 8.0 \times 10^{-15}$  cm<sup>3</sup> s<sup>-1</sup>. A few experiments were also carried out with CO as the calibrating gas. The relative slope obtained with CO corresponded to the rate constant  $k_{\rm CO} = 1.5 \times 10^{-13}$  cm<sup>3</sup> s<sup>-1</sup>, which is consistent with the recommended rate constant for this reaction at low pressure.<sup>19</sup> This result therefore agrees with the finding of Biermann et al.<sup>20</sup> that  $k_{\rm CO}$  exhibits no pressure enhancement when O<sub>2</sub> is absent.

Rigorous exclusion of  $O_2$  from the calibration mixtures was necessary in order to obtain accurate and consistent results for the various calibration gases. This was because the presence of  $O_2$  impurity led to the partial conversion of H to HO<sub>2</sub>, which then introduced a source of OH by the reaction

$$H + HO_2 \rightarrow OH + OH$$
 (21)

For high ratios of H to OH, such as are obtained when only a trace amount of  $O_2$  is present, and gases such as  $H_2$  or CO have been added, reaction 21 dominates OH loss from reaction 1 and a net gain in OH is realized. The effect of reaction 21 was seen clearly in  $H_2$  and CO calibration experiments in which  $O_2$  was present as an impurity at the ppm level. Under these circumstances the calibration plots were nonlinear and did not show the correct relative slopes with respect to CH<sub>4</sub>. The  $O_2$  effect was demonstrated experimentally as follows. In the presence of sufficient added  $H_2$  to reduce the OH signal by a factor of about 8, deliberate addition of  $O_2$  at 5 ppm caused a threefold increase in the OH signal. In contrast to  $H_2$  and CO, CH<sub>4</sub>

**TABLE I:** Summary of Results for  $k_1/k_5^{1/2}$ 

			$10^{5}k_{1}/k_{5}^{1/2}$ , cm <sup>3/2</sup> s <sup>-1/2</sup>					
press	[H.O]	carrier	metal cell		glass cell			
torr	torr	gas	no H <sub>2</sub>	$H_2$	no H <sub>2</sub>	H <sub>2</sub>	av	
730	5	Ar				6.2	6.2	
400	5	He	6.1	5.2	6.9	5.6	6.0	
400	5	Ar	6.8	5.2			6.0	
200	2.5	He	5.2	4.0	5.1	4.0	4.6	
200	2.5	Ar	6.3	5.0		5.0	5.4	
75	0.94	He	4.6	4.0			4.3	
75	0,94	Ar	5.8	5.8			5.8	
75	4.6	He	4.0	4.6			4.3	
75	4.6	Ar	5.2	4.6			4.9	

did not show a high sensitivity to  $O_2$  contamination, since reaction of OH with CH<sub>4</sub> does not produce H, as is the case with both H<sub>2</sub> and CO. Other factors may be involved, such as the scavenging of  $O_2$  by CH<sub>3</sub> radicals. In general, CH<sub>4</sub> was found to be preferable as the calibrating gas, largely for this reason.

The calibration factors depended mainly on the  $H_2O$  concentration and not on the pressure of carrier gas, because  $H_2O$  dominated the quenching efficiency of the mixtures. Calibration factors were measured immediately before each experiment, although the results were usually quite reproducible from one experiment to the next.

The quantity  $k_4$  was in the range of about 9–10 s<sup>-1</sup> in the earliest experiments in the metal cell but subsequently declined to about 3–5 s<sup>-1</sup>. This change with time is believed to have resulted from gradual removal of hydrogenous contaminants from the apparatus. The glass cell, which was introduced at a later stage of the experiments, did not show the initially high  $k_4$  values.

The approximate correctness of  $k_4$  as measured in the calibration procedure was verified by following the time decay of the OH fluorescence upon turning off the 184.9nm lamp source. For this purpose a recording oscilloscope was used to follow several successive fluorescence traces (0.1-s intervals), which were triggered to coincide with each laser pulse. Although the accuracy of this approach was limited because of variation in laser-pulse power (roughly 25% pulse-to-pulse), the observed decay was in good agreement with the calibration values.

Steady-State Measurements of [OH]. Photolysis of pure water vapor in the carrier gas gave OH concentrations of the order of  $10^{11}$  cm<sup>-3</sup>, with the exact value depending on the water-vapor concentration. Upon addition of  $O_2$ , the OH concentration fell to the range  $1 \times 10^{10} - 3 \times 10^{10}$ and declined further as H<sub>2</sub> was added. The OH reached (quasi-) steady state within about 1 s after opening of the photolysis lamp shutter. To avoid significant OH loss due to buildup of H<sub>2</sub>O<sub>2</sub>, we made the measurements within about 5–10 s. Because of the slow rate of H<sub>2</sub>O<sub>2</sub> formation, the actual rate of change in [OH] was quite small. Some decrease with time was observed, as expected.

Table I shows a summary of results for the ratio  $k_1/k_5^{1/2}$  obtained under various conditions of total pressure, mixture composition, and cell type. Each entry for added H<sub>2</sub> represents the average of about four separate measurements for different H<sub>2</sub> concentrations, all of which were sufficiently high to dominate the effect of  $k_4$ . No trend in the results with H<sub>2</sub> concentration was observed, although the results with no H<sub>2</sub> ( $k_4$  important) were on the average slightly higher than those obtained with added H<sub>2</sub>. Essentially identical values were obtained in the Tefloncoated cell and in the Pyrex cell, thus tending to argue against any role of surface effects or surface impurities. At lower pressures, the results obtained in Ar were slightly higher than in He. Individual values for the ratio  $k_1/k_5^{1/2}$ 

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<sup>(21) &</sup>quot;Chemical Kinetics and Photochemical Data for Use in Atmospheric Modelling", Evaluation No. 4, NASA Panel for Data Evaluation, Jet Propulsion Laboratory Publication 81-3, Jet Propulsion Laboratory, California Institute of Technology, Pasadena, CA.

TABLE II: Results for  $k_1$ 

press., torr	[H <sub>2</sub> O], torr	carrier gas	$10^{12}k_{5}^{a},a_{5}^{a}$ cm <sup>3</sup> s <sup>-1</sup>	$k_1,  \mathrm{cm}^3  \mathrm{s}^{-1}$
730	5	Ar	3.8	$1.2 \times 10^{-10}$
400	5	He	2.7	$1.0 \times 10^{-10}$
400	5	Ar	3.2	$1.1 \times 10^{-10}$
200	2.5	He	2.1	$6.7 \times 10^{-11}$
200	2.5	Ar	2.4	$8.4 \times 10^{-11}$
75	0.94	He	1.8	$5.8 \times 10^{-11}$
75	0.94	Ar	1.9	$8.0 \times 10^{-11}$
75	4.6	He	2.4	$6.7 \times 10^{-11}$
75	4.6	Ar	2.6	$7.9 \times 10^{-11}$

<sup>a</sup> Based on measurements of  $k_s$  in He and Ar by S. P. Sander et al. (to be submitted for publication) combined with an enhancement of  $k_s$  by water vapor as reported by Hamilton and Lii.<sup>23</sup>

for a series of measurements with different  $H_2$  concentrations varied randomly by about 20%. The major source of variation is believed to have been the zero correction of the boxcar reading, which included both the background fluorescence level (about 10% of signal) and the zero setting of the boxcar, which drifted slightly.

To obtain absolute values of  $k_1$ , it is necessary to estimate the rate constant  $k_5$  for the particular conditions of pressure and mixture composition used. There is currently some question about the exact pressure dependence of  $k_5$ . The values for the present comparison, shown in Table II, are based on recent measurements by Sander et al.,<sup>22</sup> combined with an additional factor to account for the water-vapor effect as reported by Hamilton and Lii.<sup>23</sup>

The  $[HO_2]_{ss}$  concentrations as calculated from eq 13 were usually about 1 order of magnitude greater than  $[OH]_{ss}$ , and for different H<sub>2</sub> concentrations the ratio  $[HO_2]/[OH]$ varied by a factor of about 5. As mentioned above,  $k_1/k_5^{1/2}$ was independent of this variation, which tends to support the validity of the results.

Computer Simulations. Computer simulations of a typical reaction mixture were conducted on the basis of the reaction set 1–7. The purposes were to examine the steady-state behavior of OH and to assess the role of  $H_2O_2$  as a loss path for OH. Literature values<sup>19,21</sup> were used for all reaction rate contants except for  $k_4$  and  $k_1$ . For  $k_4$  an experimental value of 4 s<sup>-1</sup> was used, and  $k_1$  was varied from  $6 \times 10^{-11}$  to  $1.2 \times 10^{-10}$  cm<sup>3</sup> s<sup>-1</sup>. The results showed that OH reached its (quasi-) steady-state value within about 1 s following onset of irradiation, in agreement with the experimental observation. The HO<sub>2</sub> also reached steady state in about 1 s. In the time period in which the OH steady-state measurements were made,  $H_2O_2$  accounted for only about a 5% loss of OH, thus confirming the validity of neglecting reaction 6 for the derivation of eq 16.

#### Discussion

Magnitude of  $k_1$ . At pressures near 1 atm, the calculated value of  $k_1$  is  $1.2 \times 10^{-10}$  cm<sup>3</sup> s<sup>-1</sup>, with an estimated uncertainty of  $\pm 30\%$ . The major sources of error are believed to be the calculation of  $[HO_2]_{ss}$  (which involves the reference rate constant  $k_5$ ), possible errors in the rate constants for the calibration gases, small mechanistic effects such as the neglect of  $H_2O_2$ , and random errors involved in the background fluorescence signal.

The above value of  $k_1$  is in excellent agreement with our previous measurement for 1 atm of an  $N_2/O_2$  mixture, using a different technique.<sup>3,4</sup> The best values from the

previous work were  $1.2 \times 10^{-10}$ – $1.3 \times 10^{-10}$  cm<sup>3</sup> s<sup>-1</sup>. The present result is also in good agreement with other recent measurements near 1 atm,<sup>11–13</sup> which give  $k_1$  of about  $1 \times 10^{-10}$  cm<sup>3</sup> s<sup>-1</sup>.

Other than HO<sub>2</sub>, there is no known species which can be produced in the present reaction mixtures upon addition of O<sub>2</sub> which can account for the observed OH loss rates. If such species were present before O<sub>2</sub> addition, the effect would be detected in the measurement of  $k_4$ . Production of hypothetical oxidized species which might be more reactive to OH than their precursors cannot take place on the time scale at which the measurements were made. Thus, there appears to be no reason to doubt that the observed OH loss was in fact due to reaction 1.

Pressure Dependence of  $k_1$ . Table II shows a downward trend of  $k_1$  with decreasing pressure. These observations alone cannot be accepted as proof of a pressure dependence of  $k_1$ , because the effect is not clearly outside the experimental uncertainty. It is noteworthy, nevertheless, that the low-pressure results seem to be approaching the  $k_1$ value obtained by Keyser<sup>9</sup> at a few torr, which was  $6.5 \times 10^{-11}$  cm<sup>3</sup> s<sup>-1</sup>. This comparison lends increasing support to the hypothesis of a pressure-dependent component of the reaction.

The decrease of  $k_1$  with pressure is evidently not due to decreasing H<sub>2</sub>O pressure. To test for this possibility, experiments at 75-torr total pressure were conducted with the H<sub>2</sub>O partial pressure raised to nearly the same level as in the experiments at 730 torr. As seen in Table II, the result for  $k_1$  was unchanged.

If the pressure dependence is real, the reaction mechanism must be more complex than that of a simple bimolecular abstraction. The abstraction reaction would involve a transition state of the form  $(HO \cdot HO_2)^*$  but no long-lived intermediate.

$$OH + HO_2 \rightarrow (HO \cdot HO_2)^* \rightarrow H_2O + O_2 \qquad (22)$$

The reaction occurring by this mechanism cannot exhibit a pressure dependence. However, in addition to the abstraction path, the reaction can occur as a radical-radical association reaction, and the rate of product formation by this path can have both pressure-independent and pressure-dependent components. The mechanism of the pressure-independent component is as follows:

$$OH + HO_2 \rightleftharpoons [H_2O_3]^* \qquad (23, -23)$$

$$[H_2O_3]^* \rightarrow H_2O + O_2 \tag{24}$$

The effective rate constant is  $k_{23}k_{24}/(k_{24} + k_{-23})$ . This effective rate constant would be an additive term to the rate constant,  $k_{22}$ , for the abstraction reaction. Thus, the total low-pressure rate constant would be

$$k_1(\text{low pressure}) = k_{22} + k_{23}k_{24}/(k_{24} + k_{-23})$$
 (25)

The fact that the observed value<sup>9</sup> for  $k_1$  of  $6.5 \times 10^{-11}$  cm<sup>3</sup> s<sup>-1</sup> is faster than expected for an abstraction reaction (not greater than about  $1 \times 10^{-11}$  cm<sup>3</sup> s<sup>-1</sup>) can be taken as support for the role of the radical-radical association component of the overall reaction.

At higher pressures the possibility of vibrational quenching of  $[H_2O_3]^*$  gives rise to a pressure-dependent component of the reaction.

$$[H_2O_3]^* + M \rightarrow [H_2O_3] + M$$
 (26)

For the vibrationally relaxed (or perhaps partially relaxed) species  $H_2O_3$ , the rate-constant ratio  $k_{24}^{\text{relaxed}}/k_{23}^{\text{relaxed}}$  may be much higher than for  $[H_2O_3]^*$ , as would be the case if energy barrier for reaction -23 is greater than that for reaction 24. Thus, an apparent pressure enhancement

<sup>(22)</sup> S. P. Sander, M. Peterson, R. T. Watson, and R. Patrick, to be submitted for publication.

<sup>(23)</sup> E. J. Hamilton and R. R. Lii, Int. J. Chem. Kinet. 9, 875 (1977).

would be observed. In the limiting case where  $k_{-23}^{\text{relaxed}}$  for  $H_2O_3$  is effectively zero compared to  $k_{24}^{\text{relaxed}}$ , the overall expression for  $k_1$  becomes

 $k_1 = k_{22} + k_{23}(k_{24} + k_{26}[\mathbf{M}]) / (k_{24} + k_{-23} + k_{26}[\mathbf{M}])$ (27)

It is possible to indicate the broad ranges of parameters in eq 27 required for consistency with the observed rateconstant magnitude and apparent pressure enhancement. As previously mentioned,  $k_{22}$  is not expected to be greater than about  $1 \times 10^{-11}$  cm<sup>3</sup> s<sup>-1</sup>, so that the quantity  $k_{23}k_{24}/(k_{24} + k_{-23})$  must be at least  $5 \times 10^{-11}$  cm<sup>3</sup> s<sup>-1</sup> to account for the total low-pressure observed  $k_1$ . To explain a pressure enhancement of  $k_1$ , one must place further constraints on the individual values of  $k_{23}$ ,  $k_{24}$ ,  $k_{-23}$ , and  $k_{26}$ . The data are well fitted by the values  $k_{23} = 1.5 \times 10^{-10}$  cm<sup>3</sup> s<sup>-1</sup>,  $k_{24} = 1.5 \times 10^8$  s<sup>-1</sup>,  $k_{-23} = 3 \times 10^8$  s<sup>-1</sup>, and  $k_{26} = 2 \times 10^{-11}$  cm<sup>3</sup>  $s^{-1}$ . Small variations within this set of values would also fit the observations. The consistency of these rate constants with theoretical expectation is difficult to evaluate.

The most critical unknown factor is the entropy of the intermediate  $[H_2O_3]^*$ , which determines the equilibrium constant  $k_{23}/k_{-23}$ . The high value of  $k_{23}/k_{-23}$  implied by the individual rate constants quoted above requires postulation of an extremely "loose" structure for  $[H_2O_3]^*$ .

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# Electron Exchange between Tris(hexafluoroacetylacetonato)ruthenium(II) and -(III) and between Related Compounds. Effects of Solvent on the Rates<sup>1</sup>

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The rate constants for electron exchange between  $Ru(hfac)_3^-$  and  $Ru(hfac)_3$ , between  $Ru(me_2bpy)(hfac)_2$  and  $Ru(me_2bpy)(hfac)_2^+$ , and between  $Ru(me_2bpy)(acac)_2$  and  $Ru(me_2bpy)(acac)_2^+$  have been measured by the NMR line-broadening method, hfac representing the hexafluoroacetylacetonate ion, acac representing the acetylacetonate ion, and me<sub>2</sub>bpy representing 4,4'-dimethyl-2,2'-bipyridyl. The rate constants at 25 °C in acetonitrile are 5.0  $\times$  10<sup>6</sup>, 4.5  $\times$  10<sup>6</sup>, and 1.4  $\times$  10<sup>8</sup> M<sup>-1</sup> s<sup>-1</sup>, respectively. The rate constants for the first two reactions vary with solvent dielectric properties about as predicted by the Marcus theoretical model; however, the preexponential coefficient,  $\kappa \rho Z$ , is 1 order of magnitude smaller than the value of  $\sim 10^{11}$  M<sup>-1</sup> s<sup>-1</sup> generally assumed, possibly due to steric effects of the  $CF_3$  groups. Measured temperature dependences of rate constants are small.

# Introduction

The rates of electron exchange between Ru(hfac)<sub>3</sub> and Ru(hafc)3, hfac representing the hexafluoroacetylacetonate ion, and between other neutral and singly charged complexes in various solvents are of interest because the main deterrent to electron transfer is probably the necessity for solvent reorganization.<sup>2</sup> There is no Coulombic repulsion between reactants, so the work required to bring them together is minimal, the standard free-energy change is zero for exchange reactions, and, for the exchange systems considered, the structures of the reactants are similar, so the energy required for internal rearrangement should be small and essentially the same for exchange in different solvents. Therefore, investigations of the rates of electron-exchange reactions in various solvents should increase our understanding of solvent-reorganizational requirements.

For exchange between ferrocene and ferrocenium ion, and also for several other systems, there is little dependence on solvent properties.<sup>3</sup> For several other systems, exchange rates do vary with solvent dielectric properties. These systems include those described in this article,  $Ru(hfac)_{3}^{0,-}$  and  $Ru(me_{2}bpy)(hfac)_{2}^{0,+}$ ,  $me_{2}bpy$  representing 4,4'-dimethyl-2,2'-bipyridyl, and the recently reported<sup>4</sup> exchange between  $Cr(biph)_2^{0,+}$ , biph representing biphenyl.

#### **Experimental Section**

Ru(hfac)<sub>3</sub> was purchased from Strem Chemicals, Inc., and it was purified by vacuum sublimation. Solutions of Ru(hfac)<sub>3</sub><sup>-</sup> salts in ethanol were prepared by reducing  $Ru(hfac)_3$  with potassium iodide, tetramethylammonium iodide, or tetra-n-butylammonium iodide following the procedure by Patterson and Holm.<sup>5</sup> Solid products were obtained from the ethanolic solutions by addition of water. The salts  $K[Ru(hfac)_3]$  and  $Me_4N[Ru(hfac)_3]$  were purified by recrystallization from ethanol-water solutions.  $Bu_4N$ -[Ru(hfac)<sub>3</sub>] was purified by reprecipitation from acetonitrile by addition of carbon tetrachloride. Analyses for carbon, hydrogen, and nitrogen, as well as analysis by spectrophotometric methods, indicated that these compounds were >~99% pure.

 $Ru(me_2bpy)(hfac)_2$  was synthesized from Ru- $(me_2bpy)(H_2O)Cl_3$ , which was prepared by the method

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