

# RADIOACTIVE STUDIES OF DIFFUSION IN POLYMER SYSTEMS

## PART 2.—THE SYSTEM ISOPENTANE + POLYISOBUTENE

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A method for measuring the self-diffusion coefficient in mixtures of polymer with volatile liquids is given. The synthesis of tritioisopentane is described. The self-diffusion coefficients of isopentane in polyisobutene + isopentane mixtures at 25° C and 35° C have been obtained at a few concentrations of the isopentane. These coefficients are much larger than the integrated mean of the chemical diffusion coefficient but agree well with the intrinsic diffusion coefficient. The experiments are not accurate enough to indicate whether a thermodynamic correction should be applied.

In recent years there have been many studies of the diffusion of liquids or vapours into polymers from which the so-called chemical diffusion coefficients  $D$  have been obtained. It has been shown that in many cases this coefficient increases rapidly with increase in the concentration of the small molecular species.<sup>1</sup> To correlate these concentration-dependent diffusion coefficients with molecular motions it is necessary to obtain an independent measure of these motions in the absence of the complicating factors due to the gradient in chemical composition.

In part 1<sup>2</sup> of this series a technique was described for using a radioactive tracer to measure diffusion coefficients in polymer systems in the absence of changes in chemical composition. It is convenient to call this the self-diffusion coefficient,  $\mathcal{D}^*$ , though strictly this term should be used only for single component systems. The technique involved the welding together of two slabs of polymer + solvent mixtures of the same chemical composition. Radioactive labelled solvent was used in one slab and its migration to the other slab was obtained from the change in  $\beta$  radiation strength at the face of the second slab.

Unfortunately this method is only suitable for non-volatile substances. A new method had to be developed for measuring  $\mathcal{D}^*$  in polymer + volatile solvent mixtures and for this work it was decided to investigate the polyisobutene + isopentane system. The chemical diffusion coefficients<sup>3,4</sup> and the vapour pressure-composition curves<sup>5</sup> had already been determined and this provided data helpful to the planning of the self-diffusion experiments as well as being useful for the interpretation of the results obtained. *iso*Pentane was chosen rather than one of the other hydrocarbons because its boiling point is reasonably low (28° C) which makes experimentation easier by enabling vapour pressures of the order of  $\frac{1}{2}$  atm to be used.

## EXPERIMENTAL

### MATERIALS

**POLYISOBUTENE.**—This was a specimen obtained from I.C.I., Billingham. Its quoted molecular weight was 92,000. It was dissolved in a mixture of benzene and carbon tetrachloride and precipitated in the form of a fine filament in cold acetone to remove low molecular weight impurities. Films were made by casting a solution in the benzene + carbon tetrachloride mixture on a mercury surface.

**TRITIOISOPENTANE.**—*iso*Pentane labelled with tritium was prepared by reaction of tritiated water, obtained from Harwell, with *iso*amyl magnesium bromide. About 40 g of this Grignard compound was made in ether solution. The ether was removed by heating at 120° C for 2 h in a 3-l. vessel connected to the vacuum system. 2 cm<sup>3</sup> of tritiated water having an activity of about 20 millicuries were distilled into the vessel which was next closed off and heated at 120° C for a further period of 2 h. This gave a 70 % yield of tritio*isopentane* based on the water. It was purified from *isopentene*, ether and water by treatment with concentrated sulphuric acid, acid potassium permanganate, and alkali. The final product, after outgassing had a vapour pressure against temperature relationship in good agreement with that given by the American Petroleum Institute.<sup>6</sup> Less active samples of *isopentane* were made by dilution with inactive *isopentane*.

**INACTIVE ISOPENTANE.**—This was made by a similar method to the above but an excess of dilute acid was used instead of tritiated water to decompose the Grignard compound.

**ARGON.**—Cylinder argon obtained from the British Oxygen Company was dried but no further purification was attempted.

#### THE DIFFUSION APPARATUS

The apparatus is shown diagrammatically in fig. 1. The principle of the apparatus is simple. A polymer specimen S, cemented to a glass plate P, is equilibrated with a fixed pressure of radioactive vapour in the chamber C. The vapour in C is then replaced with "chemically identical" inactive vapour at the same pressure. The rate at which this vapour becomes radioactive by diffusional exchange is then obtained by taking samples of the vapour as it is circulated through the sampling tap T<sub>1</sub>. Three features of the apparatus require special mention.

**THE SAMPLING TAP T<sub>1</sub>.**—A tap is arranged so that the contents of the bore (about 2 cm<sup>3</sup>) can be isolated and distilled into a sampling tube J. While this is occurring all the ports of the tap are closed and so vapour circulation is continued through the by-pass tap T<sub>2</sub>. After taking a sample, T<sub>3</sub> can be closed and the bore of the tap can be refilled with inactive vapour from G. On turning the tap back to the open position the pressure of vapour in the circulating system is maintained by the inactive vapour and allowance can be made for the slight change in specific activity that this causes. With T<sub>1</sub> in the open position another tube J can be evacuated through the barrel of the tap ready for the next sample.

**THE CIRCULATING PUMP E.**—The vapour is circulated through the specimen chamber and sampling tap by means of an all-glass circulating pump. The design of this pump is not very different from the one given by Brenschede.<sup>7</sup> The soft iron core is, however, shorter and fatter and only one coil working against gravity is used for oscillating the piston. The coil is made of P.V.C. insulated flexible wire so that the whole pump can be immersed in the thermostat bath without fear of electrical shortage. Forced cooling of the pump is provided by drawing a current of thermostat water through the annulus between the coil and the glass tube which forms the barrel of the pump.

**THE SPECIMEN CHAMBER C.**—This is so arranged that mercury from the bulb B can be used to cut off the lower end by closing the valve O. By letting more mercury in the whole gaseous contents of the chamber can be pushed out through the two-way tap T<sub>3</sub>. On lowering the mercury level either active or inactive vapour can be drawn in through T<sub>3</sub> and by lowering the mercury right out of the U-tube an open path for the circulation of vapour can be provided. It is necessary to break down the barrier to diffusion caused by the stagnant layer of vapour above the polymer surface and so the polymer specimen S which is cemented to the glass plate P can be rotated rapidly by suitable rapid switching of the 3 electromagnets, M, from a multiple commutator driven by an electric motor.

#### RADIOACTIVE ASSAY

The radioactive assay of tritium is made difficult by the low energy of the  $\beta$  particles that are given off. A method based on the filling of a special Geiger tube (20th Century Electronics Tube, GA. 10/M) with tritio*butane* has been developed by Glascock.<sup>8</sup> We have tried these tubes with fillings of tritio*isopentane* but though we could get results the high voltages needed (about 3,500 V) often caused electrical leakages leading, amongst other things, to Geiger plateaux with very steep slopes. Since we did not need to put

as much hydrocarbon as possible into the tubes, we found that in our work satisfactory results could be obtained from a normal argon filling using about 5% addition of the active hydrocarbon which also acts as a quenching agent. As an example of the action of such a filling 160 mm of argon with 6 mm of *isopentane* counted at about 1100 V and gave a plateau longer than 200 V with a slope of less than 4% per 100 V. Pressures of

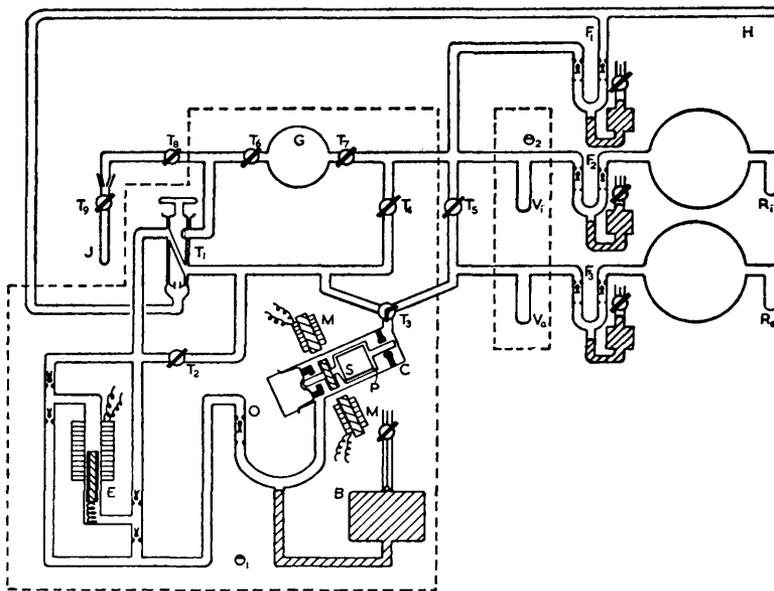


FIG. 1.—The diffusion apparatus.

- |   |   |                |   |
|---|---|----------------|---|
| B | bulb of mercury used to displace vapour from C,                   | R <sub>a</sub> | storage reservoir for active liquid,  |
| C | specimen chamber,   | R <sub>i</sub> | storage reservoir for inactive liquid,                                      |
| E | electromagnetic glass circulating pump,                           | S              | polymer specimen with one face exposed to vapour,                           |
| G | bulb of inactive vapour for filling bore of T <sub>1</sub> ,      | T <sub>1</sub> | sampling tap for isolating samples of circulating vapour,                   |
| H | high vacuum line,   | T <sub>2</sub> | by-pass tap for T <sub>1</sub> ,  |
| J | sample tube for removing specimens of radioactive vapour,         | V <sub>a</sub> | vapour source for active vapour,  |
| M | system of three electromagnets for rotating the plate P,          | V <sub>i</sub> | vapour source for inactive vapour,  |
| O | cut-off valve to enable sealing of lower end of specimen chamber, | $\theta_1$     | all within the dotted line maintained at $\theta_1$ °C by water thermostat, |
| P | glass plate with soft iron bar for rotation,                      | $\theta_2$     | all within the dotted line maintained at $\theta_2$ °C by water thermostat. |

these magnitudes were easily obtained by transferring the whole of the contents of the sampling tap into the Geiger tube and letting the argon expand in from a bulb.

#### GENERAL PROCEDURE

A sheet of polyisobutene of suitable thickness was cemented to the glass plate P by gentle pressure. Care was taken to avoid the inclusion of air bubbles between the film and the plate and film projecting beyond the edge of the plate was removed with moist scissors. Traces of casting solvent were removed by heating in a vacuum oven overnight and the thickness of the polymer was obtained by weight and area measurement. The whole plate and film were then mounted in the chamber C which was next evacuated

and O was closed with the mercury from B. The temperatures  $\theta_1$  and  $\theta_2$  were adjusted to give the required equilibrium of *isopentane* in the polyisobutene and  $T_3$  was turned to the active *isopentane* in  $V_a$ . The time for equilibrium to be established in the polymer was calculated from the data of Prager, Bagley and Long,<sup>3, 4</sup> and after this time the rest of the apparatus was filled with inactive vapour from  $V_i$ . The active vapour was displaced with mercury,  $T_3$  was turned and inactive vapour drawn in by lowering the mercury with  $T_4$  open. When all the mercury had run out  $T_4$  was closed and the rotation of P and the pumping by E were started. At known intervals from the start, samples were withdrawn into J and their activities were determined. An average experiment continued for 24 h after closing  $T_4$ , most of the readings being taken in the first 4-5 h.

## RESULTS

### ACTIVITY AGAINST TIME RELATIONSHIP

In fig. 2 the activities of the *isopentane* in the diffusion apparatus during two experiments at the same vapour pressure are plotted against the square root of time. Allowance

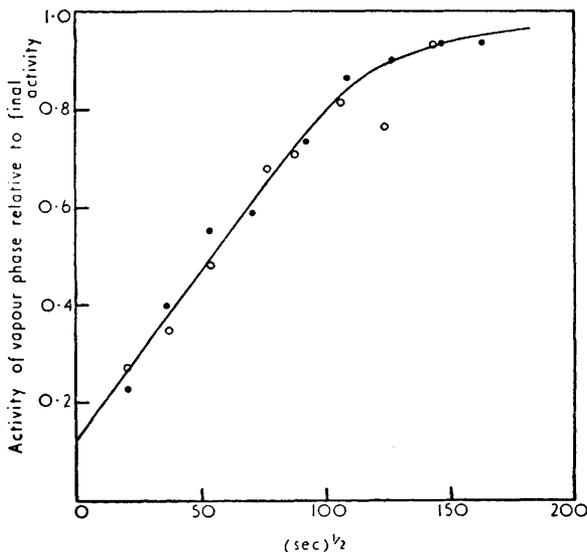


FIG. 2.—Tritiopentane desorption plot.

- high-activity *isopentane* used ( $\sim 1$  mcurie mole<sup>-1</sup>),
  - low-activity *isopentane* used ( $\sim 100$   $\mu$ curie mole<sup>-1</sup>),
- thickness of P.I.B. specimen initially = 0.077 cm,

vapour pressure of *isopentane* = 665 mm,  
 regain of *isopentane* = 18 %, *isopentane* in specimen/*isopentane* in vapour phase = 0.2,  
 specimen temperature = 35° C.

has been made for the slight dilution of activity which occurs when each sample is taken. The first part of the curve can be represented very nearly by a straight line. This line has a positive intercept on the activity axis. A blank experiment in the absence of polymer showed that the intercept represents the amount of radioactive *isopentane* left in the specimen chamber (but not dissolved in the polymer) when the bulk of this vapour is displaced by the rising mercury. To give the true measure of the amount of radioactive vapour diffused out of the polymer at any time during the experiment the intercept was subtracted from the observed activity.

### THE SELF-DIFFUSION COEFFICIENT

Since there is no overall change in *isopentane* concentration in the polymer during a diffusion experiment the motion of radioactive *isopentane* out of the polymer sheet is governed by a constant diffusion coefficient. The conditions of the experiment are that the concentration of tritio*isopentane* is initially constant throughout the polymer sheet

and at the start of the experiment it is dropped to zero at the exposed surface. If we further assume that the amount of *isopentane* in the vapour phase is so large that the equilibrium concentration of tritioisopentane at the surface remains at zero then at any time  $t$  the amount  $M_t$  of tritioisopentane diffused into the vapour phase is given by the well-known equation,

$$\frac{M_t}{M_\infty} = 2 \frac{(\mathcal{D}^* t)^{\frac{1}{2}}}{l} \left[ \frac{1}{\pi^{\frac{1}{2}}} + 2 \sum_{n=1}^{\infty} (-1)^n \operatorname{ierfc} \frac{nl}{(\mathcal{D}^* t)^{\frac{1}{2}}} \right]. \quad (1)$$

Here  $\operatorname{ierfc} x$  is related to the error function and is given by

$$\frac{2}{\pi^{\frac{1}{2}}} \int_x^{\infty} \int_y^{\infty} \exp(-z^2) dz dy.$$

$\mathcal{D}^*$  is the diffusion coefficient,  $M_\infty$  is the amount of tritioisopentane lost from the sheet after infinite time,  $l$  is the thickness of the sheet of *isopentane* + polyisobutene mixture and  $n$  is an integer.<sup>9</sup> Eqn. (1) leads to the initial linear plots of fig. 2 with no significant deviation from linearity up to  $M_t/M_\infty = 0.7$ . In our experiments where the vapour phase is not infinite in extent the concentration of tritioisopentane at the sheet surface increases with time eventually reaching a steady value at equilibrium. This leads to deviation from the behaviour predicted by eqn. (1) and the consequences of this finite bath behaviour have been worked out by several authors (e.g. ref. (9)). In the experiments reported here the ratio of the capacity of the vapour phase to that of the specimen is between 5 and 20. The main effects are to make the plots against  $t^{\frac{1}{2}}$  somewhat curved and to cause the half-way point to be reached up to 20% earlier. We have calculated our diffusion coefficients from the linear part using eqn. (1) and have corrected for the finite bath effects using the tables given by Berthier.<sup>10</sup> The concentrations of *isopentane* in the polymer have been obtained from the vapour pressures using the data of Prager, Bagley and Long.<sup>5</sup> These concentrations have been used in calculating  $l$  from the thickness of the polymer when free from *isopentane* (assuming no volume change on mixing and all swelling at right-angles to sheet surface) and in working out the deviations from infinite bath conditions. The vapour pressures were obtained from the temperatures of the liquid *isopentane* using the figures of the American Petroleum Institute.<sup>6</sup> In fig. 3 the diffusion coefficients obtained have been plotted against concentrations.

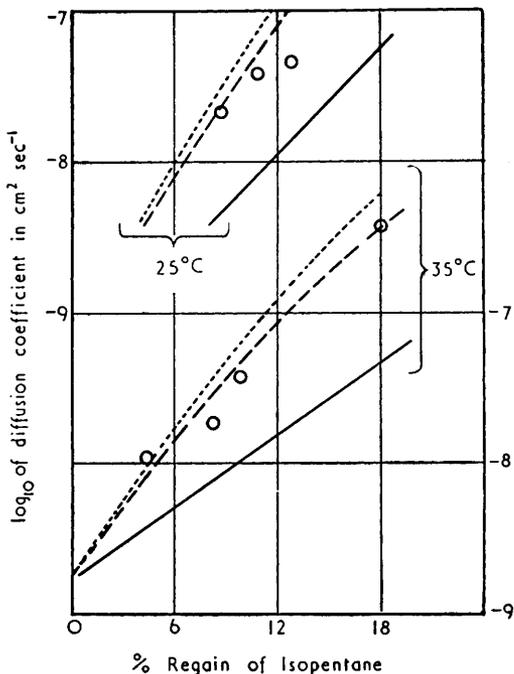


FIG. 3.—Diffusion coefficients at 25 and 35°C  
Ordinates: left-hand numerals refer to diffusion coefficients at 25°; right-hand numerals to 35°.

- self-diffusion coefficient,  $\mathcal{D}^*$
- integral diffusion coefficient  $D_{av}$ ,
- - - intrinsic diffusion coefficient  $\mathcal{D}_p$ ,
- ..... thermodynamic diffusion coefficient  $\mathcal{D}_T$ .

## DISCUSSION

### THE INTEGRAL DIFFUSION COEFFICIENT

Prager and Long<sup>3</sup> suggested that in systems where the diffusion coefficient  $D$  varies with concentration the integral diffusion coefficient is more closely related

than is  $D$  to the frequency  $\nu$  with which molecules in a region at concentration  $C$  jump to a neighbouring region. Here by integral diffusion coefficient is meant  $D_{av}$  as defined by

$$D_{av} = \frac{1}{c} \int_0^c D dC, \quad (2)$$

where  $D$  is the diffusion coefficient at concentration  $C$  obtained from concentration-gradient experiments. As a consequence of this there has been a tendency to express diffusion data for polymer + small molecule systems in terms of  $D_{av}$  and to calculate activation energies for diffusion from  $D_{av}$  rather than from  $D$ . The self-diffusion coefficient  $\mathcal{D}^*$  gives a direct measure of the jumping frequency  $\nu$  and so if Prager and Long's suggestion were correct  $\mathcal{D}^*$  should be equal to  $D_{av}$ .

In fig. 3 we have plotted the values given by Prager and Long<sup>3</sup> and by Prager, Bagley and Long<sup>4</sup> for the coefficient  $D_{av}$  as obtained from measurements on the rate of sorption of vapour. Both at 25° C and 35° C the  $\mathcal{D}^*$  values are much larger than  $D_{av}$  and at 35° C the 18 % regain value is greater by about 10 times. It should be pointed out that there are possibilities of systematic experimental error in the tracer experiments due to a stagnant vapour layer on the polymer surface and to a finite rate of circulation of the vapour. Allowance for such errors if they occurred would, however, increase the difference between  $D_{av}$  and  $\mathcal{D}^*$ .

#### THE THERMODYNAMIC DIFFUSION COEFFICIENT

The relationship between  $D_{av}$  and  $\mathcal{D}^*$  suggested by Prager and Long is obtained when one assumes that the frequency of jumping of molecules from a region at concentration  $C_1$  to a neighbouring region at concentration  $C_2$  is a function of  $C_1$  only. Prager<sup>11</sup> has considered the situation arising from a jump frequency depending on both  $C_1$  and  $C_2$ . His conclusion can be expressed in the form,

$$\mathcal{D}^* = \mathcal{D}_p d \ln C / d \ln a \equiv \mathcal{D}_T, \quad (3)$$

where  $\mathcal{D}_p$  is the intrinsic diffusion coefficient as defined by Hartley and Crank,<sup>12</sup>  $a$  is the penetrant activity and  $C$  is the penetrant concentration.  $\mathcal{D}_T$  can be called the thermodynamic diffusion coefficient.

We have calculated  $\mathcal{D}_p$  and  $\mathcal{D}_T$  from  $D_{av}$  using the data of Prager, Bagley and Long<sup>9</sup> and assuming no volume change on mixing. The resultant plots are given in fig. 3. It will be seen that  $\mathcal{D}_T$  is in reasonable agreement with  $\mathcal{D}^*$ . Though the values are somewhat closer to  $\mathcal{D}_p$  than to  $\mathcal{D}_T$  we consider that, owing to the systematic errors already mentioned and to the general scatter of the results this is not significant.

The author's thanks are due to Dr. B. A. Toms for suggestions leading to the design of the sampling tap, to Dr. R. F. Glascock for discussion on the gas counting of tritium and to Mr. R. E. Hester for experimental assistance.

<sup>1</sup> see, for instance, King, *Trans. Faraday Soc.*, 1945, **41**, 479. Park, *Trans. Faraday Soc.*, 1950, **46**, 684. Kokes and Long, *J. Amer. Chem. Soc.*, 1953, **75**, 6142.

<sup>2</sup> Park, *Radioisotope Conference*, 1954 (Butterworths), vol. 2, p. 11.

<sup>3</sup> Prager and Long, *J. Amer. Chem. Soc.*, 1951, **73**, 4072.

<sup>4</sup> Prager, Bagley and Long, *J. Amer. Chem. Soc.*, 1953, **75**, 1255.

<sup>5</sup> Prager, Bagley and Long, *J. Amer. Chem. Soc.*, 1953, **75**, 2742.

<sup>6</sup> *American Petroleum Institute Research Project 44* (Selected values of properties of hydrocarbons and related compounds), table 1k. (Dec. 31, 1952. Carnegie Institute of Technology, Dept. of Chemistry, Pittsburg, Pennsylvania.)

<sup>7</sup> Brenschede, *Z. physik. Chem. A*, 1936, **178**, 74.

<sup>8</sup> Glascock, *Isotopic Gas Analysis for Biochemists* (Academic Press, New York, 1954).

<sup>9</sup> Crank, *The Mathematics of Diffusion* (Oxford, 1956).

<sup>10</sup> Berthier, *J. Chim. Phys.*, 1952, **49**, 527.

<sup>11</sup> Prager, *J. Chem. Physics*, 1953, **21**, 1344.

<sup>12</sup> Hartley and Crank, *Trans. Faraday Soc.*, 1949, **45**, 801.