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Communication

A One-Step Low Temperature Processing Route for Organolead Halide Perovskite Solar Cells

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Organolead trihalide perovskite solar cells based upon the codeposition of a combined Al₂O₃/perovskite layer at T < 110 °C are presented. We report an average PCE = 7.2 % on a non-10 sintered Al₂O₃ scaffold in devices that have been manufactured from a perovskite precursor containing 5 % wt. Al₂O₃ nanoparticles.

The spectral sensitization of n-type TiO₂ electrodes by polypyridineruthenium (II) complexes was first described by ¹⁵ Clark and Sutin in 1977⁻¹. This combined with early work on photoelectrochemical cells ² and dye-sensitization to increase the efficiency of TiO₂ photocatalysis ³, led to the realisation of dyesensitization for photovoltaic applications and eventually to the work of O' Regan and Grätzel on colloidal, high surface area ²⁰ TiO₂ films. The result was their seminal paper describing high efficiency dye-sensitized solar cells (DSSCs) in 1991⁻⁴. Further developments of screen printable polymer-organic TiO₂ pastes ⁵ and high efficiency cells built on metal substrates ⁶ has led to the realisation that it may be possible to produce DSSCs utilising ²⁵ roll-to-roll processes. Sensitizer and electrolyte developments

have recently resulted in DSSCs reaching power conversion efficiencies (PCE) of over 12 $\%^{7}$.

So far the highest performing devices have utilized dye sensitizers and liquid electrolytes, but alternative configurations ³⁰ have been extensively investigated such as the solid state dye-sensitized solar cell (ss-DSSC), with a solid organic hole transporter ⁸, and alternative sensitizers such as quantum dots ⁹. To date, ss-DSSC power conversion efficiency stands at 7.2 % ¹⁰ and the highest recorded for quantum dot devices so far is PCE = ³⁵ 7.0% ¹¹ In 2009, Kojima *et al.* published work on using

organometal halide perovskite as sensitizers in liquid electrolyte based devices. They achieved a PCE of 3.8 % with a $CH_3NH_3PbI_3$ perovskite and a V_{OC} of 0.96 V with a $CH_3NH_3Br_3$ perovskite ¹². The realisation that these perovskite materials could 40 be utilised in ss-DSSCs as light harvesters lead to high efficiency

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⁵⁰ devices, whereby a PCE of 9.7 % was achieved ¹³. In other work focussing on a mixed halide (CH₃NH₃PbI_{3-x}Cl_x) perovskite it was found that electron transport was faster when an alumina scaffold was utilised than when using a TiO₂ scaffold. Higher efficiencies were achieved when using the insulating mesoporous Al₂O₃
 ⁵⁵ scaffold than with a semiconducting mesoporous TiO₂ scaffold/electron-acceptor. A PCE of 10.9 % was achieved with V_{OC} in excess of 1.1 V in a device utilising a sintered alumina scaffold ¹⁴. Caesium tin iodide (CsSnI₃) perovskite has also been employed as solid hole conductor in a ss-DSSC with a PCE of 60 8.5 % ¹⁵.

Organolead halide perovskite materials are a promising, low cost, easily synthesised set of materials. They act as light absorber and both electron and hole transporter. Indeed, efficient devices have been made where no organic hole transporter is 65 utilised ¹⁶. All the technologies mentioned so far require a high temperature heating step in order to sinter the TiO₂ or Al₂O₃ nanoparticles. Perhaps from a manufacturing point of view, one of the most promising aspects of the Al₂O₃ based devices is the fact that, as Al₂O₃ is electrically insulating, there is no need to 70 sinter the nanoparticles, as particle interconnectivity will not be as important as it is in TiO₂ based devices where poor particle interconnectivity results in slower electron transport and lower photocurrents ¹⁷. In the work outlined by Lee *et al.* ¹⁴, nanoparticles are sintered at 550 °C but this may not be necessary 75 and indeed, low temperature deposition of Al₂O₃ has now been achieved with device performances better than that of devices made with a sintered alumina film ¹⁸

In this work, we propose an alternative method of Al_2O_3 /perovskite deposition whereby the two step deposition ⁸⁰ process can be performed in a single step. The alumina nanoparticles are suspended in the perovskite precursor solution and the Al_2O_3 /perovskite layer is co-deposited by spin coating in a single deposition. This is followed by a low temperature heating step at T < 110 °C. The mixed halide perovskite precursor and ⁸⁵ device manufacturing method outlined by Lee *et al.* ¹⁴ have been utilised. Our methodology differs in that instead of depositing a lead halide perovskite precursor solution onto a pre-sintered Al_2O_3 scaffold, we have added Al_2O_3 nanoparticles directly to the perovskite precursor solution. This is followed by a low ⁹⁰ temperature heating step at T < 110 °C. This has the advantage of combining two manufacturing steps into one and negates the need for a high temperature (550 °C) sintering step. This results in

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devices that have a lower embodied energy with a relatively more simple manufacturing process. This may prove to be of great importance to the scale up and manufacture of this technology.

The alumina nanoparticle suspension is obtained from Sigma-5 Aldrich (20 wt. % in isopropanol). Initial experiments involved adding the alumina suspension directly to the perovskite precursor solution. The resultant Al₂O₃/perovskite precursor solution was non-homogeneous in appearance which we have hypothesised as being caused by mixed solvent/solute 10 incompatibilities, as the perovskite precursor is poorly soluble in isopropanol. Devices made with this Al₂O₃/perovskite solution had low efficiencies. In order for high efficiency devices to be made, it was found that the nanoparticles must be suspended in DMF (N,N-Dimethylformamide). This is achieved via solvent 15 exchange in a rotary evaporator whereby equal volumes of the nanoparticle suspension and DMF were put into a round bottom flask. A rotary evaporator is then used to remove the lower boiling point isopropanol, thus leaving the nanoparticles suspended in DMF. The nanoparticle suspension in DMF is then 20 added to the perovskite precursor solution which is also dissolved in DMF. The first devices manufactured, did not perform well and showed evidence of shunting in their IV curves. This was solved by sonication of the nanoparticle suspension for one hour prior to addition to the perovskite precursor solution. This 25 suggests that the shunting could have been caused by nanoparticle aggregation leading to film imhomogeneity and possible contact between the perovskite and the gold counter electrode. Fig. 1 below shows the statistical IV data for all manufactured devices, with varying nanoparticle weight 30 percentages dispersed in the perovskite precursor prior to deposition.

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Fig. 1 Statistical IV data showing: a) efficiency (PCE), b) open-circuit voltage (V_{OC}), c) short-circuit current density (J_{SC}) and d) fill-factor (FF) of devices *vs.* the nanoparticle wt. % in the perovskite precursor solution before deposition



40 Fig.2 Plan view SEM images of co-deposited Al₂O₃/perovskite films. The wt. % of alumina in the precursor solution prior to spin coating is shown top-left in each SEM micrograph. It can be seen that the co-deposited alumina/perovskite forms a dual-phase structure with alumina rich (lighter shading) and alumina poor (darker shading) areas

- ⁴⁵ It can be seen that device PCE improves as the wt. % is increased from 0 % (a planar junction cell) to 5 %. At higher weight percentages, PCE decreases. Fig. S1[†] shows the UV-Vis absorbance of co-deposited Al₂O₃/perovskite films, spin coated onto microscope slides, the average Al₂O₃/perovskite film ⁵⁰ thickness was found to be 400 nm using a profilometer. A cross sectional SEM of the best performing device in this study is shown in Fig. S2[†]. The absorbance spectra show increasing absorbance with increased particle loading. The increasing PCE (Fig.1) could possibly be due to increased amounts of perovskite
 ⁵⁵ crystallizing from the precursor solution with increased nanoparticle wt. %. However, there is also expected to be an increase in light scattering with an increase in nanoparticle wt. % which could account for, at least a proportion of, the absorbance
- increase. At the highest nanoparticle weight percentages (6 % and $_{60}$ 8 % by wt. in the precursor solution), the UV-VIS absorbance continues to increase despite the photovoltaic PCE decreasing at wt. % > 5 %. This decrease in performance may occur due to the dual phase nature that has been observed and is evident in Fig. 2 which shows plan-view SEM images of the same films as in Fig.
- 65 S1[†]. EDX analyses of these films shows that there are alumina rich areas (lighter shading, figure 2) and alumina poor areas (darker shading) which could indicate poor wetting of the alumina surface by the perovskite precursor solution. At higher nanoparticle wt. %, electron transport through the perovskite film 70 could be restricted by the large alumina deposits. This is supported by the IV data where devices made with the higher weight percentage precursor solutions show lower photocurrents and fill factors.

To date our most efficient organolead trihalide perovskite devices, incorporating an alumina scaffold, have been manufactured using the low temperature manufacturing method described here. For comparison, a statistical analysis of the 8 ⁵ most efficient devices made with a sintered (550 °C) Al₂O₃ scaffold has been conducted and the results are summarised in Table S1[†] where it can be seen that the average PCE = 3.17 % (\pm 0.88 %). The average device efficiency for the 8 most efficient low T, co-deposited devices is PCE = 3.98 % (\pm 0.33 %). The improvement in device PCE and improvement in device consistency is in accordance with the recent report by Ball *et al.* in which they have achieved their best device performances with

a low temperature Al₂O₃ deposition technique ¹⁵. Following the work presented so far to determine the optimum ¹⁵ nanoparticle wt. %, steps have been taken to improve device efficiencies. We have observed that the performance of these devices is sensitive to the relative humidity (RH) in the laboratory at the point of manufacture. When devices are manufactured in an atmosphere of RH < 35 %, improvements in PCE are significant.
²⁰ Indeed, we have recently manufactured our highest efficiency devices, using the low temperature method which is described in the ESI[†] and by controlling the humidity during manufacture. The average PCE of our ten most recent devices is 7.2 % (± 0.6 %).

Fig. 3 shows the IV curve of one such device with PCE = 7.2 %.

12.78

J_{sc} (mA cm⁻²) Fill Factor Efficiency

0.61

7.16

V_{oc} (V)

0.925



Fig 3. IV curve of the best performing device manufactured so far using the low temperature co-deposition technique.

³⁰ It can be seen that the fill factor of this device and indeed, of all devices presented in this work, is low. The IV curve above shows evidence of shunting, which could be the source of our comparatively low device efficiencies. This is perhaps as a result
 ³⁵ of our HTM layer not being optimised (in terms of layer thickness, precursor solution concentration and dopant levels). In fact it should be noted that very little optimisation work has been carried out on these devices. Emphasis has been put on

determining the best nanoparticle wt. % in the perovskite 40 precursor and controlling the laboratory humidity during manufacture. Optimisation of the HTM layer is the focus of ongoing work and it is therefore conceivable that devices manufactured in the way described above can match the performance of devices described in ¹⁵, especially when the dual ⁴⁵ phase nature of the co-deposited layer is considered. If it is possible to encourage the perovskite to wet the surface of the nanoparticles more effectively upon crystallization then it may be possible to achieve large improvements in device light harvesting efficiency, which may improve photocurrents. If fill factors can ⁵⁰ also be improved by HTM optimisation then it is conceivable that high efficiency devices can be manufactured using this low temperature co-deposition technique.

Conclusions

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We have shown that it is possible to obtain efficient lead halide based perovskite devices by co-depositing a single Al₂O₃/perovskite layer at low temperatures. We believe this will be of great interest to those working on the development and ⁶⁰ scale-up manufacture of these devices. Furthermore, we believe that with further optimisation, devices manufactured using this low temperature method can be improved upon and leads to the distinct realisation of highly efficient, low temperature, solidstate devices.

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