## DOI: 10.1039/b111382h

## Low temperature selective catalytic reduction (SCR) of NO with NH<sub>3</sub> over Fe–Mn based catalysts

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Received (in Cambridge, UK) 13th December 2001, Accepted 21st January 2002 First published as an Advance Article on the web 4th February 2002

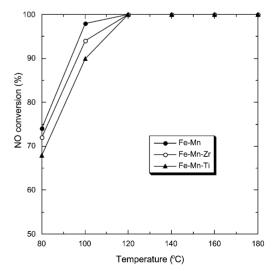
Fe–Mn based transition metal oxides (Fe–Mn, Fe–Mn–Zr and Fe–Mn–Ti) show nearly 100% NO conversion at 100–180 °C for selective catalytic reduction of NO with NH $_3$  under the applied conditions with a space velocity of 15 000 h $^{-1}$ 

Nitrogen oxides (NO, NO<sub>2</sub> and N<sub>2</sub>O) have been a major source of air pollution. They contribute to photochemical smog, acid rain, ozone depletion and the greenhouse effect. An efficient technology for removing NO from power plants is selective catalytic reduction (SCR) with ammonia  $(4 \text{ NO} + 4 \text{ NH}_3 + \text{O}_2 =$  $4 N_2 + 6 H_2O$ ). The industrial operations are carried out on  $V_2O_5 + WO_3(MoO_3)/TiO_2$  catalysts at 350–400 °C.<sup>1–3</sup> However, the high concentration of ash (e.g., K<sub>2</sub>O, CaO and As<sub>2</sub>O<sub>3</sub>) in the flue gas reduces their performance and longevity, although they are resistant to  $SO_2$ .<sup>2,4</sup> To solve this problem, one attractive option is to place the SCR unit downstream of the desulfurizer and electrostatic precipitators where SO<sub>2</sub> and ash have been removed. Since the temperature in the downstream is typically below 200 °C, this makes it necessary to develop low temperature SCR catalysts to avoid reheating of the flue gas and thus decrease the capital cost.

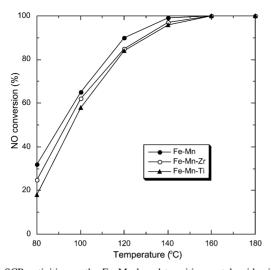
Some transition metal containing catalysts have been investigated for the low temperature SCR reaction, such as amorphous chromia,<sup>5</sup> NiSO<sub>4</sub>/Al<sub>2</sub>O<sub>3</sub>,<sup>6</sup> MnO<sub>x</sub>/Al<sub>2</sub>O<sub>3</sub>,<sup>7</sup> V<sub>2</sub>O<sub>5</sub>/activated carbon8 and MnO<sub>x</sub>/TiO<sub>2</sub>.9 They showed various SCR activities at below 200 °C under different conditions. It is known that ammonium nitrite decomposes quickly into N<sub>2</sub> (majority) and NO (minority) below 100 °C.<sup>10</sup> The formation of ammonium nitrite from NO, O<sub>2</sub> and NH<sub>3</sub> requires oxidation of NO to NO<sub>2</sub> by O<sub>2</sub>. In our previous work, 11,12 we have shown that an increase in NO oxidation to NO2 on Fe-ZSM-5 will result in a significant improvement of the SCR activity and, moreover, the reaction rate of NH<sub>3</sub> with NO<sub>2</sub> + NO is much higher than that with NO. Therefore, it is expected that a high activity for NO conversion to NO<sub>2</sub> at low temperatures may facilitate a high SCR activity because it can enhance the formation of ammonium nitrite. More recently, we found that Fe-Mn based transition metal oxides were highly efficient sorbents for NO removal.<sup>13</sup> In particular, these sorbents showed very high activity for NO oxidation to NO<sub>2</sub> at room temperature; 63–76% NO conversions were obtained on Fe-Mn, Fe-Mn-Zr and Fe-Mn-Ti oxides under the conditions of 500 ppm NO, 10% O<sub>2</sub> and GHSV (gas hourly space velocity) =  $6000 \text{ h}^{-1}$ . Therefore, we investigated these mixed oxides as low temperature SCR catalysts in this work.

The Fe–Mn based transition metal oxides (Fe–Mn, Fe–Mn–Zr and Fe–Mn–Ti, with equal mol of metals) were prepared by the coprecipitation method as described in detail previously. <sup>13</sup> The BET surface areas were 54, 178 and 183 m² g⁻¹, respectively, for Fe–Mn, Fe–Mn–Zr and Fe–Mn–Ti oxides. The SCR activity measurements were carried out in a fixed-bed quartz reactor. The reaction conditions were as follows: 0.5 g sample (0.4 ml), 1000 ppm NO, 1000 ppm NH<sub>3</sub>, 2% O₂, 2.5% water vapor (when used), 37.5 or 1000 ppm SO₂ (when used), balance He, 100 ml min⁻¹ total flow rate and GHSV = 15 000

 $h^{-1}$  (ambient conditions). The premixed gases (1.01% NO/He, 1.00% NH<sub>3</sub>/He and 0.99% SO<sub>2</sub>/He) were supplied by Matheson. Water vapor was generated by passing He through a gaswash bottle containing deionized water. The tubings of the reactor system were heat-traced to prevent formation and deposition of ammonium sulfate/bisulfate and ammonium nitrate. The NO and NO<sub>2</sub> concentrations were continually monitored by a chemiluminescent NO/NO<sub>x</sub> analyzer (Model 42C, Thermo Environmental Instruments Inc.). To avoid errors caused by the oxidation of ammonia in the converter of the NO/ NO<sub>x</sub> analyzer, an ammonia trap containing phosphoric acid solution was installed before the sample inlet to the chemiluminescent analyzer. The products were analyzed by a gas chromatograph (Shimadzu, 14A) at 50 °C with 5A molecular sieve column for N2 and Porapak Q column for N2O. All the data were obtained after 60-200 min when the SCR reaction reached a steady state. The SCR activities of Fe-Mn, Fe-Mn-Zr and Fe-Mn-Ti oxides at 80-180 °C are shown in Fig. 1. These mixed oxides showed excellent activities at low temperatures. At 80 °C, 68-74% NO conversions were obtained at a space velocity of 15 000 h<sup>-1</sup>. With increasing temperature, NO conversion increased significantly and reached nearly 100% at above 120 °C. The products were N<sub>2</sub> and H<sub>2</sub>O only and N<sub>2</sub>O formation was not observed by GC. However, on pure MnO<sub>x</sub>, we observed 8-35% N<sub>2</sub>O selectivity (with 72-93% NO conversion) at 80–180 °C under the same reaction conditions. The SCR activity at low temperatures decreased in the following order: Fe-Mn > Fe-Mn-Zr > Fe-Mn-Ti. As mentioned above, the Fe-Mn catalyst has a much lower surface area than Fe-Mn-Zr and Fe-Mn-Ti oxides. Hence it seems that the SCR activity does not have a correlation with the surface



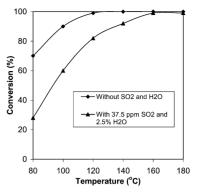
**Fig. 1** SCR activities on the Fe–Mn based transition metal oxides in the absence of  $H_2O$ . *Reaction conditions*: 0.5 g catalyst, [NO] = [NH<sub>3</sub>] = 1000 ppm, [O<sub>2</sub>] = 2%, He = balance, total flow rate = 100 ml min<sup>-1</sup> and GHSV = 15 000 h<sup>-1</sup>.



**Fig. 2** SCR activities on the Fe–Mn based transition metal oxides in the presence of  $H_2O$ . *Reaction conditions*: 0.5 g catalyst, [NO] = [NH<sub>3</sub>] = 1000 ppm, [O<sub>2</sub>] = 2%, [H<sub>2</sub>O] = 2.5%, He = balance, total flow rate = 100 ml min<sup>-1</sup> and GHSV = 15 000 h<sup>-1</sup>.

Since the combustion gases contain water vapor, we further studied the effect of  $\rm H_2O$  on the SCR activities of the mixed oxides. As shown in Fig. 2, when 2.5%  $\rm H_2O$  was added to the reactants, NO conversion decreased sharply at lower temperatures, e.g., 80 °C. It is likely that  $\rm H_2O$  occupies some of the active sites for the SCR reaction. When the reaction temperature was increased, the  $\rm H_2O$  inhibition effect became less significant. At 160–180 °C, nearly 100% NO conversion was still obtained on the three catalysts. In addition, the Fe–Mn based catalysts did not show any decrease in activity after 10 h on stream at 140 °C in the presence of  $\rm H_2O$ . Also, the inhibition by  $\rm H_2O$  is reversible. When  $\rm H_2O$  was removed from the reaction gases, NO conversions were recovered on these catalysts.

The above results indicate that the Fe-Mn based transition oxides are highly active for the low temperature SCR reaction and they are resistant to water vapor at 140-180 °C. Their SCR activities are much higher than those on 20%MnO<sub>x</sub>/Hombikat TiO<sub>2</sub>, the 'best' low temperature catalyst reported in ref. 9. For instance, at 100 °C, 89-98% NO conversions were observed on the Fe-Mn based catalysts at GHSV =  $15\,000\,h^{-1}$  (Fig. 1), whereas only 82% NO conversion was reported on the MnO<sub>x</sub>/  $TiO_2$  at GHŠV = 8000 h<sup>-1</sup>. The superior SCR activity on these Fe-Mn catalysts is probably related to their high activity for NO oxidation to  $NO_2$  at low temperatures. Since  $NO_2 + NO$  is very active in reacting with NH3 adsorbed species at low temperatures,  $^{12}$  the formed NO<sub>x</sub> can be reduced to nitrogen by NH<sub>3</sub>. It is noted that there are still small concentrations of SO<sub>2</sub> in combustion gases even after the desulfurizer (except when using very clean fuels such as liquefied natural gas). Effects of SO<sub>2</sub> on the SCR activity are also important for the low temperature SCR catalyst. Our result indicated that, when 1000 ppm SO<sub>2</sub> was added to the reaction gas and the space velocity was kept at 15 000 h<sup>-1</sup>, NO conversions on Fe-Mn-Zr oxides were decreased significantly to 8-23% at 80-180 °C under steady state conditions. This is consistent with the previous observations that  $MnO_x$  catalysts were deactivated by  $SO_2$ .<sup>7,14</sup>



**Fig. 3** SCR activities on the Fe–Mn based transition metal oxides in the presence of SO<sub>2</sub> + H<sub>2</sub>O. *Reaction conditions*: 0.5 g catalyst, [NO] = [NH<sub>3</sub>] = 1000 ppm, [O<sub>2</sub>] = 2%, [SO<sub>2</sub>] = 37.5 ppm and [H<sub>2</sub>O] = 2.5% (when used), He = balance, total flow rate = 100 ml min<sup>-1</sup> and GHSV = 15 000 h<sup>-1</sup>

In the presence of SO<sub>2</sub>, SO<sub>2</sub> can be oxidized to SO<sub>3</sub> by O<sub>2</sub>. The SO<sub>x</sub> compounds (SO<sub>2</sub> + SO<sub>3</sub>) are adsorbed on the transition metal oxides and they are difficult to desorb at low temperatures. Our FTIR spectrum of the used Fe–Mn–Zr oxides showed two strong bands centered at 1402 and 1120 cm<sup>-1</sup>, indicating formation of ammonium ions and sulfate species, respectively.<sup>15</sup> The occupation of the active sites by metal sulfates and ammonium sulfates will decrease the SCR activity.<sup>14</sup> The effects of lower levels of SO<sub>2</sub> have also been studied. The results for 37.5 ppm SO<sub>2</sub> plus 2.5% H<sub>2</sub>O are shown in Fig. 3. As expected, less deactivation was seen for 37.5 ppm SO<sub>2</sub> compared with that by 1000 ppm SO<sub>2</sub>. Further work on the modification of the catalysts is needed to improve sulfur resistance.

We thank Mr G. Qi for measuring the effects of  $SO_2$  at 37.5 ppm. This work was supported by EPRI and NSF under Grant CTS-0095909.

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