

# Phase Equilibria in the System $\text{Ti}_2\text{Te}$ – $\text{SnTe}$ – $\text{TiBiTe}_2$ \*

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**Abstract**—The phase equilibria in the system  $\text{Ti}_2\text{Te}$ – $\text{SnTe}$ – $\text{TiBiTe}_2$  (A) have been studied using differential thermal analysis, x-ray diffraction, and microhardness measurements. We have constructed the  $T$ – $x$  phase diagrams along the  $\text{SnTe}$ – $\text{TiBiTe}_2$ ,  $\text{SnTe}$ – $\text{Ti}_9\text{BiTe}_6$ , and  $\text{Ti}_4\text{SnTe}_3$ – $\text{TiBiTe}_2$  joins, the 600- and 800-K sections of the phase diagram of system A, and its liquidus diagram. The results demonstrate that the system contains broad ranges of  $\text{Ti}_5\text{Te}_3$ -structured and  $\text{SnTe}$ -based solid solutions ( $\delta$  and  $\gamma_1$  phases, respectively). There are also relatively small fields of the  $\text{Ti}_2\text{Te}$ -based phase ( $\alpha$ ) and low- and high-temperature  $\text{TiBiTe}_2$ -based solid solutions ( $\gamma_2$  and  $\gamma'_2$ ). The liquidus surface of system A comprises the primary crystallization fields of the  $\delta$ ,  $\gamma_1$ , and  $\gamma'_2$  phases. The liquidus of the  $\alpha$  phase is degenerate. The ternary eutectic between the  $\delta$ ,  $\gamma_1$ , and  $\gamma'_2$  phases melts at 755 K.

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## INTRODUCTION

Tellurides of heavy  $p$ -metals are thought to be attractive hosts for the preparation of new thermoelectric materials [1, 2]. In this family of compounds, tin, bismuth, and thallium tellurides are of considerable practical importance [1–5]. One way of enhancing the performance of thermoelectric materials is by utilizing multicomponent compounds with complex structures [2, 6]. The key to the targeted synthesis of new multicomponent tellurides of the above elements lies in knowing the phase equilibria in the corresponding systems.

This led us to study the phase equilibria in the composition region  $\text{Ti}_2\text{Te}$ – $\text{SnTe}$ – $\text{TiBiTe}_2$  (A) of the quaternary system  $\text{Ti}$ – $\text{Sn}$ – $\text{Bi}$ – $\text{Te}$ . The constituent binary tellurides  $\text{Ti}_2\text{Te}$  and  $\text{SnTe}$  melt congruently at 698 and 1080 K, respectively [1, 7, 8].  $\text{Ti}_2\text{Te}$  has a monoclinic structure [9], and  $\text{SnTe}$  has a primitive cubic unit cell [7]. The ternary compound  $\text{TiBiTe}_2$  exists in two crystalline polymorphs. At 780 K, the low-temperature, orthorhombic phase transforms into the high-temperature, disordered phase of variable composition, which melts congruently at 830 K [10–12].

The constituent binaries of system A have been studied by several groups. The  $\text{Ti}_2\text{Te}$ – $\text{SnTe}$  system was reported to contain a ternary compound of composition  $\text{Ti}_4\text{SnTe}_3$ , which has a broad homogeneity range (12–40 mol %  $\text{SnTe}$ ) and melts congruently at 825 K [13, 14]. This compound, as well as related solid solu-

tions ( $\delta$  phase), crystallizes in tetragonal symmetry ( $\text{Ti}_5\text{Te}_3$  structure, sp. gr.  $I4/mcm$ ). The lattice parameters of  $\text{Ti}_4\text{SnTe}_3$  are  $a = 8.82 \text{ \AA}$  and  $c = 13.01 \text{ \AA}$  ( $Z = 4$ ) [15]. The  $\text{Ti}_2\text{Te}$ – $\text{TiBiTe}_2$  system contains a compound of composition  $\text{Ti}_9\text{BiTe}_6$ , which melts congruently at 830 K, also has a tetragonal structure of the  $\text{Ti}_5\text{Te}_3$  type ( $a = 8.855 \text{ \AA}$ ,  $c = 13.048 \text{ \AA}$ ,  $Z = 2$ ) [10, 16], and forms a continuous series of solid solutions with  $\text{Ti}_2\text{Te}$  [10].

As shown by Mazelsky and Lubell [17], the  $\text{SnTe}$ – $\text{TiBiTe}_2$  system contains limited solid solutions based on  $\text{SnTe}$  (56 mol %) and  $\text{TiBiTe}_2$  (21 mol %).

Dashdieva et al. [18] studied the phase equilibria in the composition region  $\text{Ti}_2\text{Te}$ – $\text{Ti}_4\text{SnTe}_3$ – $\text{Ti}_9\text{BiTe}_6$  of system A. According to their results, the  $\text{Ti}_4\text{SnTe}_3$ – $\text{Ti}_9\text{BiTe}_6$  join is pseudobinary, with a continuous series of  $\text{Ti}_5\text{Te}_3$ -structure solid solutions ( $\delta$  phase). Their lattice parameters follow Vegard's law ( $a = 8.821$ – $8.854 \text{ \AA}$ ,  $c = 13.01$ – $13.05 \text{ \AA}$ ). The  $\delta$  phase field extends over most of the  $\text{Ti}_2\text{Te}$ – $\text{Ti}_4\text{SnTe}_3$ – $\text{Ti}_9\text{BiTe}_6$  system [18].

## EXPERIMENTAL

The constituent tellurides of system A were synthesized by melting appropriate high-purity elemental mixtures in silica tubes sealed off under a vacuum of  $\sim 10^{-2} \text{ Pa}$ , followed by slow cooling. The synthesis temperature was 750 (Tl<sub>2</sub>Te), 1150 (SnTe), or 900 K (TiBiTe<sub>2</sub>), that is, slightly above the corresponding melting point. The synthesized compounds were identified by differential thermal analysis (DTA) and x-ray diffraction (XRD).

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Alloys of system A were prepared by vacuum-melting telluride mixtures. We prepared  $\text{SnTe}-\text{TiBiTe}_2$ ,  $\text{Ti}_4\text{SnTe}_3-\text{TiBiTe}_2$ , and  $\text{SnTe}-\text{Ti}_9\text{BiTe}_6$  alloys and a number of alloys beyond these joins. Using DTA results for a number of unhomogenized alloys and earlier data [10, 13, 18], we selected heat-treatment temperatures at which the alloys were equilibrated for 500 h. The alloys annealed at 600 K were furnace-cooled, and those annealed at 800 K were quenched in cold water.

The alloys were characterized by DTA (NTR-74 pyrometer, Chromel-Alumel thermocouples), XRD (DRON-2 powder diffractometer,  $\text{CuK}\alpha$  radiation), and microhardness measurements (PMT-3 tester, 0.2-N indentation load).

## RESULTS AND DISCUSSION

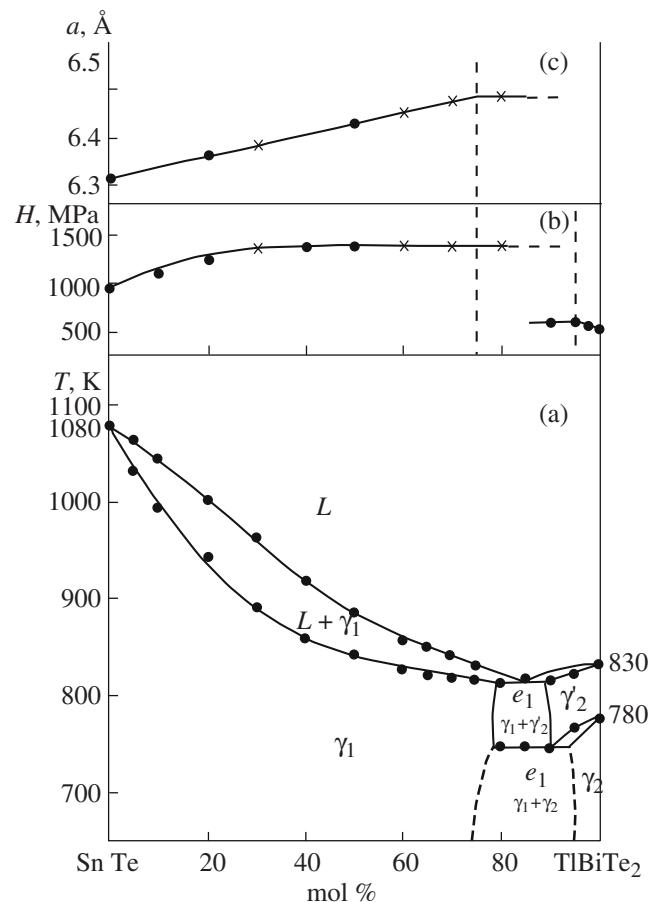
The present experimental data and earlier results [10, 13, 14, 18] for the constituent binaries and the  $\text{Ti}_2\text{Te}-\text{Ti}_4\text{SnTe}_3-\text{TiBi}_6\text{Te}_2$  system are summarized in Figs. 1–6.

The present  $T-x$  phase diagram of the  $\text{SnTe}-\text{TiBiTe}_2$  system (Fig. 1a) differs somewhat from that reported by Mazelsky and Lubell [17]. According to our results, this system involves both eutectic and eutectoid phase relations. The eutectic ( $e_1$ ) is located at  $\approx 85$  mol %  $\text{TiBiTe}_2$ , with a melting point of 815 K.

The homogeneity range of the  $\text{SnTe}$ -based phase ( $\gamma_1$  phase) extends to 80 mol %  $\text{TiBiTe}_2$  at 800 K and to 72 mol %  $\text{TiBiTe}_2$  at 600 K. The formation of low- and high-temperature  $\text{TiBiTe}_2$ -based solid solutions ( $\gamma_2$ - and  $\gamma'_2$  phases) is accompanied by a reduction in the temperature of the polymorphic transformation from 765 to 750 K and a transition to eutectoid phase relations. The eutectoid point ( $e_2$ ) is located at  $\approx 90$  mol %  $\text{TiBiTe}_2$  and 750 K (Fig. 1a). The width of the homogeneity range of the  $\gamma'_2$  phase is 10 mol % (800 K), and that of the  $\gamma_2$  phase is  $\approx 5$  mol % (600 K).

XRD and microhardness data are consistent with the  $T-x$  phase diagram of the  $\text{SnTe}-\text{TiBiTe}_2$  system. Powder XRD patterns of the alloys containing 0–70 mol %  $\text{TiBiTe}_2$  (annealing at 600 K) or 0–80 mol %  $\text{TiBiTe}_2$  (quenching after annealing at 800 K) show only reflections from an  $\text{SnTe}$ -based cubic phase, and its lattice parameter varies almost linearly with composition, from  $a = 6.327$  (SnTe) to  $6.465$  Å (80 mol %  $\text{TiBiTe}_2$ ) (Fig. 1c). The microhardness  $H$  of the  $\gamma_1$  phase rises steadily from  $\approx 850$  (SnTe) to  $\approx 1400$  MPa (80 mol %  $\text{TiBiTe}_2$ ), and that of the  $\gamma_2$  phase rises from  $\approx 500$  ( $\text{TiBiTe}_2$ ) to 600 MPa (95 mol %  $\text{TiBiTe}_2$ ). The microhardness of the samples quenched from 800 K slightly exceeds that of the corresponding samples annealed at 600 K (Fig. 1b).

The XRD, DTA, and microhardness data for the alloys annealed at 600 K were used to map out the sub-solidus phase diagram of system A (Fig. 2). As seen in



**Fig. 1.**  $T-x$  phase diagram of the  $\text{SnTe}-\text{TiBiTe}_2$  system (a); composition dependences of the microhardness (b) and lattice parameter (c). The crosses in panels b and c represent samples quenched from 800 K.

Fig. 2, the 600-K section comprises single- ( $\delta$ ,  $\gamma_1$ , and  $\gamma_2$ ), two-, and three-phase fields. The  $\gamma_1$  and  $\gamma_2$  phase fields extend along the constituent binary  $\text{SnTe}-\text{TiBiTe}_2$  and are 2–3 mol % in width. The  $\delta$  phase field extends over most of the  $\text{Ti}_2\text{Te}-\text{Ti}_4\text{SnTe}_3-\text{Ti}_9\text{BiTe}_6$  region. In addition, there are two fields ( $\alpha$  and  $X$ ) near  $\text{Ti}_2\text{Te}$ . The alloys in the  $\alpha$  field are isostructural with  $\text{Ti}_2\text{Te}$ . We failed to detect an  $\alpha + \delta$  two-phase field, which leads us to assume that the  $\alpha \rightleftharpoons \delta$  phase transformation is morphotropic. In the  $X$  field, the  $\text{Ti}_2\text{Te}-\text{SnTe}-\text{TiBiTe}_2$  plane is unstable: the equilibrium alloys contain, in addition to the  $\alpha$  and  $\delta$  phases, a  $\text{Ti}$ -based metallic phase [18]. This rare effect, also encountered in the constituent system  $\text{Ti}_2\text{Te}-\text{SnTe}$ , was analyzed in detail elsewhere [13, 14].

The phase diagram of the  $\text{SnTe}-\text{Ti}_9\text{BiTe}_6$  system (Fig. 3) is similar in appearance to that of a pseudobinary eutectic, but this system is not pseudobinary. The alloys of this system consist of two phases,  $\gamma_1 + \delta$ , but, as seen in Fig. 2, the compositions of the equilibrium  $\gamma_1$  and  $\delta$  phases lie beyond this join. Comparison of Figs. 3

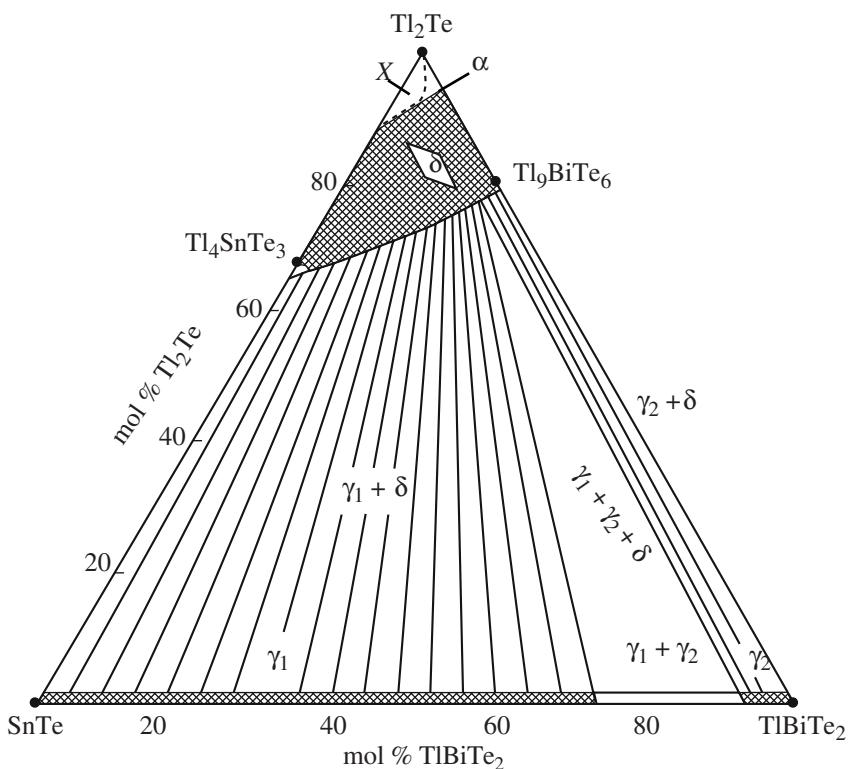


Fig. 2. 600-K section of the  $T$ - $x$ - $y$  phase diagram of the  $\text{Tl}_2\text{Te}$ - $\text{SnTe}$ - $\text{TlBiTe}_2$  system.

and 5 demonstrates that the  $\text{SnTe}-\text{Tl}_9\text{BiTe}_6$  join passes through primary crystallization fields and intersects the eutectic curve  $e_2E$ , representing the univariant equilibrium

$$L \rightleftharpoons \gamma_1 + \delta. \quad (1)$$

Because of the very small slope of the  $e_2E$  curve over the  $\text{SnTe}-\text{Tl}_9\text{BiTe}_6$  join, this eutectic transformation occurs in a very narrow temperature range, and is represented by a single, sharp DTA peak. For this reason, the  $L + \gamma_1 + \delta$  field in Fig. 3 is marked by a dashed line. Along this join, the homogeneity ranges of the  $\gamma_1$  and  $\delta$  phases are  $\approx 3$ – $4$  mol % in width (600 K).

More complex phase relations were found along the  $\text{Tl}_4\text{SnTe}_3$ - $\text{TlBiTe}_2$  join (Fig. 4), which passes through five phase fields below the solidus (Fig. 2). Its liquidus comprises three branches, corresponding to the primary crystallization of the  $\delta$ -,  $\gamma_1$ -, and  $\gamma_2'$  phases, which are separated by the eutectic curves  $e_1E$  and  $e_2E$  (Fig. 5). The 755-K horizontal represents the four-phase equilibrium

$$L_E \rightleftharpoons \gamma_1 + \gamma_2' + \delta, \quad (2)$$

and the 748-K horizontal represents the eutectoid equilibrium

$$\gamma_2' \rightleftharpoons \gamma_1 + \gamma_2 + \delta. \quad (3)$$

Below this horizontal, the alloys containing 50–87 mol %  $\text{TlBiTe}_2$  consist of three phases:  $\gamma_1 + \gamma_2 + \delta$  (Fig. 2). In the composition ranges  $\approx 7$ – $50$  and  $80$ – $90$  mol %  $\text{TlBiTe}_2$ , the solidus line represents the univariant eutectic processes (1) and (4), respectively:

$$L_E \rightleftharpoons \gamma_2' + \delta. \quad (4)$$

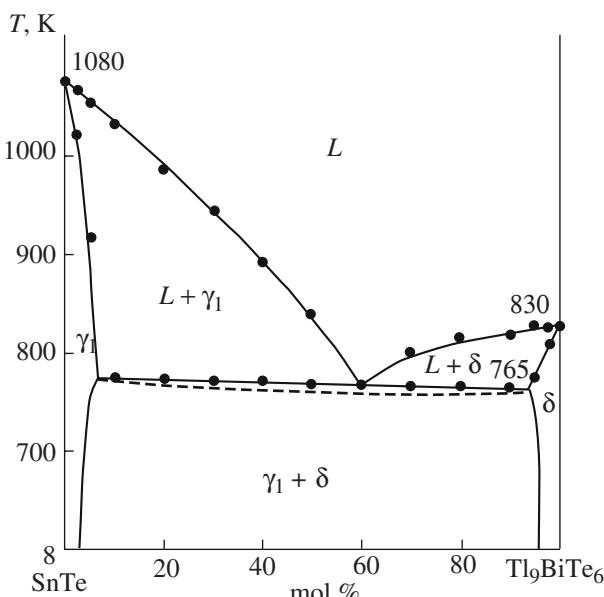
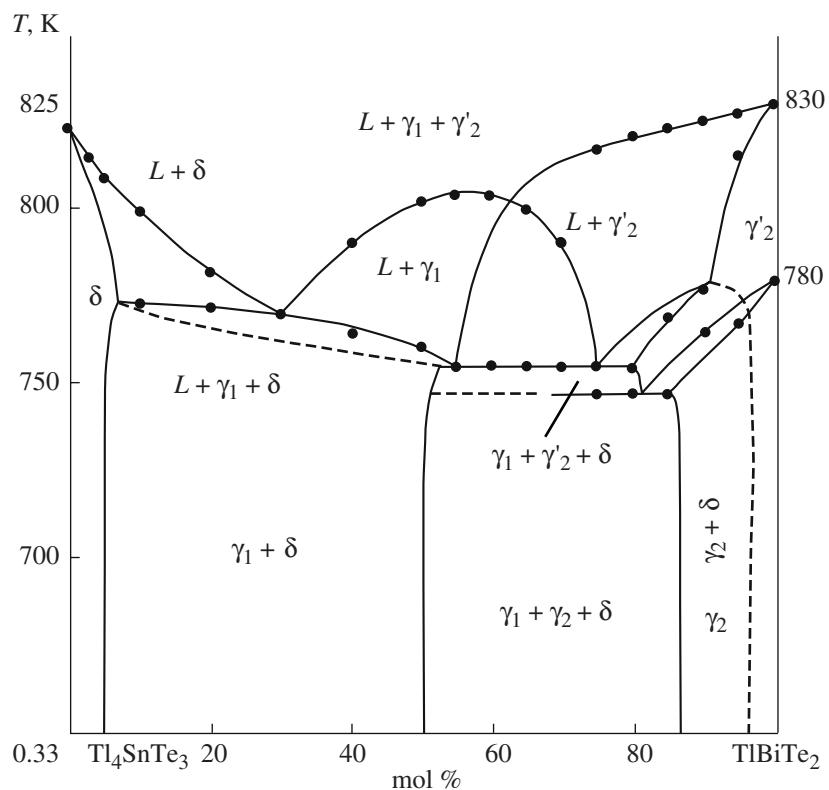
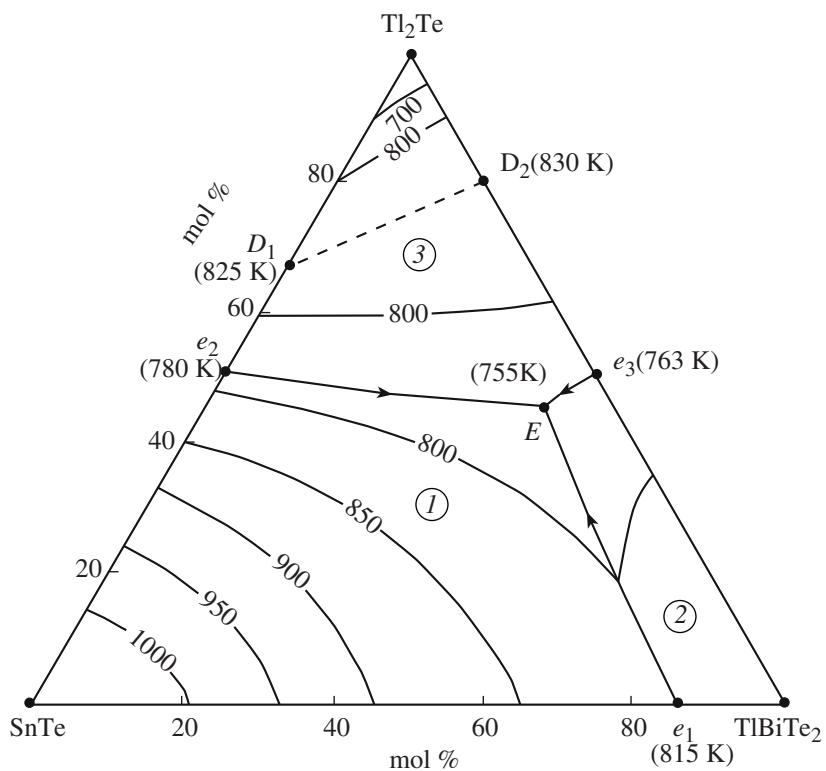


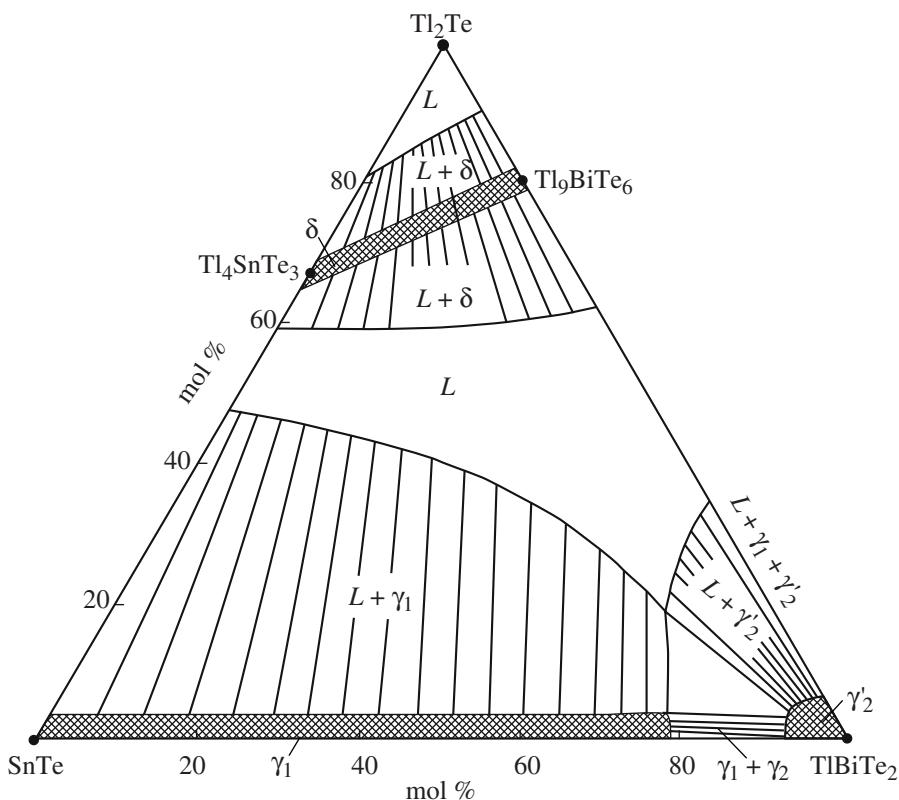
Fig. 3.  $T$ - $x$  phase diagram of the  $\text{SnTe}-\text{Tl}_9\text{BiTe}_6$  system.



**Fig. 4.**  $T$ - $x$  phase diagram of the  $\text{Tl}_4\text{SnTe}_3$ - $\text{TlBiTe}_2$  system.



**Fig. 5.** Liquidus diagram of the  $\text{Tl}_2\text{Te}$ – $\text{SnTe}$ – $\text{TlBiTe}_2$  system. Primary crystallization fields: (1)  $\gamma_1$ , (2)  $\gamma'_2$ , (3)  $\delta$ . The dashed line represents the pseudobinary join  $\text{Tl}_4\text{SnTe}_3$ – $\text{Tl}_9\text{BiTe}_6$ .



**Fig. 6.** 800-K section of the  $\text{Tl}_2\text{Te}$ – $\text{SnTe}$ – $\text{TlBiTe}_2$  phase diagram.

The homogeneity ranges of the  $\delta$  and  $\gamma_2$  phases along the  $\text{Tl}_4\text{SnTe}_3$ – $\text{TlBiTe}_2$  join are no wider than 5 mol %.

The liquidus surface of system A comprises three primary crystallization fields, those of the  $\delta$ -,  $\gamma_1$ -, and  $\gamma'_2$  phases (Fig. 5). The eutectic curves  $e_2E$ ,  $e_3E$ , and  $e_1E$ , separating these fields, represent the univariant equilibria (1), (4), and

$$L_{e_1E} \rightleftharpoons \gamma_1 + \gamma'_2.$$

The ternary eutectic point  $E$  is located at  $\approx 45$  mol %  $\text{Tl}_2\text{Te}$  and  $\approx 10$  mol %  $\text{SnTe}$ .

The dashed line in Fig. 5 represents the only pseudo-binary join ( $\text{Tl}_4\text{SnTe}_3$ – $\text{Tl}_9\text{BiTe}_6$ ) in system A. The liquidus surface of the  $\text{Tl}_2\text{Te}$ -based phase ( $\alpha$ ) is degenerate.

Figure 6 shows the isothermal section of the phase diagram of system A inferred from the data for alloys quenched after 800-K annealing and from the position of the corresponding isotherms in Fig. 5. From the position of tie lines in the two-phase regions  $L + \gamma_1$ ,  $L + \gamma'_2$ , and  $L + \delta$ , one can select melt compositions for the crystal growth of solid solutions of controlled composition by directional solidification.

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