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Freezing of water droplets colliding with kaolinite particles

E. A. Svensson¹, C. Delval^{2,3}, P. von Hessberg², M. S. Johnson², and J. B. C. Pettersson¹

¹Department of Chemistry, Atmospheric Science, University of Gothenburg, 41296 Gothenburg, Sweden

²Copenhagen Centre for Atmospheric Research, Department of Chemistry, University of Copenhagen, Universitetsparken 5, 2100 København Ø, Denmark

³EPFL STI IMT LOA, Station 17, 1015 Lausanne, Switzerland

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Correspondence to: J. B. C. Pettersson (janp@chem.gu.se)

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Abstract

Contact freezing of single supercooled water droplets colliding with kaolinite dust particles has been investigated. The experiments were performed with droplets levitated in an electrodynamic balance at temperatures from 240 to 268 K. Under dry conditions freezing was observed to occur below 249 K, while a freezing threshold of 267 K was observed at high relative humidity. The effect of relative humidity is attributed to an influence on the contact freezing process for the kaolinite-water droplet system, and it is not related to the lifetime of the droplets in the electrodynamic balance. Freezing probabilities per collision were derived assuming that collisions at the lowest temperature employed had a probability of unity. The data recorded at high humidity should be most relevant to atmospheric conditions, and the results indicate that parameterizations currently used in modelling studies to describe freezing rates are appropriate for kaolinite aerosol particles. Mechanisms for contact freezing are briefly discussed.

1 Introduction

At temperatures higher than the threshold for homogeneous nucleation, a solid particle is required for ice nucleation to take place. In this heterogeneous nucleation process, the solid surface helps align the water molecules in an ice-like structure (Cantrell and Heymsfield, 2005). Hence, heterogeneous freezing temperatures depend on the surface properties of the solid substrate. Other influential factors are droplet volume and surface area of the solid particle. At the moment, there is no unifying theoretical framework to describe heterogeneous freezing of water.

It is known that heterogeneous freezing occurs at higher temperatures when a solid particle collides with the droplet compared to when the particle is completely immersed inside the droplet (Pruppacher and Klett, 1998). This has been confirmed for mineral dust (Pitter and Pruppacher, 1973) and pollen (von Blohn et al., 2005), with a possible exception for soot particles (Diehl and Mitra, 1998). Kaolinite ($\text{Al}_2\text{Si}_2\text{O}_5(\text{OH})_4$) is built

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up from alternating layers of silica and aluminum hydroxide (Miller et al., 2007) and it is known to make an important contribution to the atmospheric aerosol in several parts of the world (e.g. Singer et al., 2004; Drab et al., 2002; Shi et al., 2005). Kaolinite particles are known to be moderately efficient cloud condensation nuclei (Gibson et al., 2007). Salam et al. (2006) examined heterogeneous ice nucleation on kaolinite particles in the deposition mode involving the direct transition of water vapor into ice. The particles were activated as ice nuclei at 251 K and 123% relative humidity with respect to ice. In the immersion freezing mode previous studies have been performed using a wind tunnel (Pitter and Pruppacher, 1973) and an acoustic levitator (Ettner et al., 2004). Pitter and Pruppacher (1973) observed freezing of water droplets with kaolinite immersions in a temperature range from 243 to 259 K. They also studied contact freezing with the same components and showed that in this mode the freezing temperatures were substantially higher, 266 K to 268 K.

In the present study, we reexamine contact freezing between water and kaolinite dust particles in an electrodynamic balance (EDB). Experiments have been performed in the temperature range from 240 to 268 K, and the effects of temperature and relative humidity on the efficiency of contact freezing were investigated.

2 Experimental

The experiments were performed in an EDB setup described in detail elsewhere (Svensson et al., 2009). Briefly, a double-ring EDB (Davis et al., 1990) is situated in a temperature controlled chamber. A HeNe-laser operating at 633 nm illuminates the central region of the EDB and two cameras observe the droplet. One camera records the ordinary picture of the droplet and the surroundings and the other records the light scattering pattern. The droplet size can be estimated by counting the fringes and comparing with predictions from Mie theory (Mishchenko et al., 2002). Droplets were produced using a syringe with an electrically charged needle or a piezoelectric droplet generator. This setup has proven its ability to reproduce homogeneous freezing

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rates for pure water (Svensson et al., 2009).

For the studies presented here two important features were added, which are shown schematically in Fig. 1. In order to be able to operate at high temperatures (268 K) the relative humidity (RH) had to be high. Otherwise, droplets would have evaporated within a few seconds. There was an air flow in thermal equilibrium with the chamber walls running through the chamber during the experiments. Due to a pressure drop in the circuit, it was not possible to humidify this air efficiently. A minor flow of humid air was instead injected directly into the chamber. This humid air mixed with the upward flow of dry air in thermal equilibrium with the walls about 50 mm below the EDB rings, which increased the RH substantially. At 267 K a droplet with an initial diameter of 50 μm typically stayed large enough to be observed for about 30 s. In all cases in this study droplets evaporated, which implies that the water vapor pressure was below saturation. Injecting warm and humid air into the chamber changed the temperature in the chamber. The temperature at the droplet position between the rings was calibrated using a small Pt-100 sensor. At a setpoint temperature of 267 K, the temperature at the droplet position was about 1 K higher than the copper blocks.

An aerosol generator was also constructed. A plastic bottle with kaolinite powder (Fluka, purum, natural, product number 13584) and a magnetic stirrer was used to dispense dust. Suspension and settling was assumed to result in an equilibrium concentration of kaolinite particles in the air inside the bottle. The number concentration of kaolinite particles from the aerosol generator was stable within 20%. The air flow through the bottle was regulated by a mass flow controller (MFC) and was running continuously during an experiment. A valve directed the aerosol flow either out through the lab ventilation or into the experiment chamber. The aerosol was injected into the chamber from below by a third inlet. The flow was cooled to chamber wall temperature by passing through a piece of copper in contact with the temperature controlled chamber walls. The outlet of the cooling unit was located about 10 mm under the electrode rings. The particle flow into the chamber was switched off most of the time. As a droplet was trapped, the flow was turned on until the droplet was frozen or had evaporated. Before

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the next droplet was injected, the chamber was flushed with air. At all temperatures droplets were also trapped without injecting dust particles and on these occasions no freezing was observed.

The copper cooling device was electrically grounded by contact with the chamber walls. This modified the electrical field in which the droplet was trapped, which changed the movement of the droplet in the trap. With this arrangement, superposing a DC voltage between the rings had little effect on droplet position and was not used during the experiments. The spring-point phenomenon (Davis et al., 1990) was not observed here. As droplets evaporated, they tended to move upwards and if the AC amplitude was decreased the droplets exited to the sides rather than downwards as in ordinary EDBs.

The aerosol size distribution between the rings was measured between the experimental runs using an aerosol spectrometer (Grimm, Dustmonitor model 1.108) and the number concentration was measured with a condensation particle counter (CPC) (TSI model 3010). A typical particle size distribution measured with the aerosol spectrometer at the droplet position is shown in Fig. 2. The size distribution was broad with a substantial fraction of submicron particles and the concentration dropped rapidly for particle sizes above $3\ \mu\text{m}$. Concentrations measured with the CPC at the droplet position varied with the flow through the dust dispensing bottle. Rise times from turning on the valve to steady state concentrations were typically 6 s, and the measured values were compensated for this effect. The measured concentrations are not expected to be representative for the concentration in the vicinity of the droplet during freezing experiments. This is due to two reasons: i) There was a spatial distribution of particles coming out from the particle outlet, and ii) the presence of the tube sucking air into the CPC disturbed the flow inside the chamber. In addition, the probability for particle-droplet collisions should depend on the flow conditions around the droplets during the experiments, which introduces a dependence on particle size. Due to the oscillation of the droplets in the EDB (a few mm) the droplets sweep a larger space than the product of their cross-sections and the gas flow velocity. These different effects are

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not expected to change significantly within the limited temperature and relative humidity ranges used in this study, and they have not been directly accounted for. Instead, the observed particle number concentrations were assumed to be proportional to the probability of collision with a droplet per time unit.

3 Results

Contact freezing of water droplets colliding with kaolinite dust particles has been investigated at temperatures from 240 to 268 K and with different relative humidities. The initial droplet size was typically about 60 μm . In total 159 droplets were analyzed in this study, and the results from the experiments are summarized in Table 1. Experiments were carried out with different kaolinite particle air flows, PF, in order to change the particle number concentrations. The last column in the table gives the ratio between the number of frozen droplets and the total number of droplets at each temperature. The additional flow of humid air was zero at 240–251 K, intermediate at 258 K and high at 263–268 K. As explained above, the RH could not be explicitly known, but it was below water saturation for all droplets. The results in Table 1 show that for a given flow of kaolinite particles and a given humidity, the freezing probability decreased with increasing temperature. The particle-droplet collisions thus became less efficient in inducing freezing at high temperatures. The decrease in freezing probability could be partially counter-acted by increasing kaolinite particle concentration and thereby the collision rate. The relative humidity was mainly increased in order to maintain levitated droplets for a longer time in the EDB at high temperatures where the evaporation rate is high. However, an interesting result is that the freezing probability also appears to increase with increasing humidity.

To study the collision efficiency in greater detail, the results were corrected for differences in the number of collisions experienced by each droplet. For each droplet, the number of collisions before freezing was estimated by

$$N_{\text{coll}} = F \times t_f \times C, \quad (1)$$

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where F is a conversion factor derived assuming that all droplets freeze on the first collision at 240 K, t_f is the time before freezing and C is the measured particle number concentration. Hence, in cases where all droplets freeze, the freezing efficiency, i.e. the number of freezing events per collision, can be estimated by,

$$E = \frac{N_{\text{droplets}}}{\sum N_{\text{coll}}} = \frac{N_{\text{droplets}}}{F \times \sum t_f \times C}, \quad (2)$$

where N_{droplets} is the number of droplets at each temperature. Because freezing is assumed to happen by the first collision at 240 K, C is calculated by setting E to 1 for the droplets at this temperature. However, at many temperatures not all droplets froze. We can estimate the number of collisions experienced by an unfrozen droplet with the average of the freezing times for the frozen droplets at the same temperature. Using the number of frozen droplets, N_{frozen} and the total number of droplets, N_{total} , the freezing efficiency becomes

$$E = \frac{N_{\text{frozen}}}{F \times \sum_{\text{frozen}} t_f \times C} \times \frac{N_{\text{frozen}}}{N_{\text{total}}} \quad (3)$$

Effects of droplet size were not included in this analysis. The freezing efficiencies are plotted in Fig 3. The data clearly illustrate that under dry conditions, the freezing efficiency decreases when going from 240 to 251 K. The decrease is not an effect of a shorter residence time in the EDB at higher temperatures since the droplet lifetime has been accounted for in Eq. (3). The results in Fig. 3 also show that the humidity has an important effect on the freezing probability. For the highest flow of humid air, the freezing probability is high at 263 K, and then again drops as the temperature is further increased.

4 Discussion

There exist pronounced differences between the major ice formation mechanisms involving kaolinite (as well as other clays and minerals). Several earlier studies (Mason

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and Maybank, 1958; Roberts and Hallett, 1968; Shaller and Fukuta, 1979; Bailey and Hallett, 2002) demonstrated that the threshold temperature for ice nucleation by deposition freezing on kaolinite is about 253 K. For immersion mode freezing, an onset temperature of 259 K has been reported (Pitter and Pruppacher, 1973). The results presented here confirm that contact freezing is the most efficient ice nucleation process involving kaolinite particles, with freezing temperatures being observed up to 267 K. In previous work Pitter and Pruppacher (1973) studied contact freezing of water drops with kaolinite and montmorillonite particles. Supercooled water droplets with a diameter of $650\ \mu\text{m}$ were suspended in a vertical wind tunnel at temperatures from 243 to 273 K and in a relatively dry airstream, and the RH varied from 60% to ice saturation depending on operating conditions. The size of the clay particles varied from about 0.1 to $30\ \mu\text{m}$ in diameter and had a mode between 1 and $2\ \mu\text{m}$. Kaolinite and montmorillonite were concluded to behave similarly as ice-forming nuclei and induce freezing at temperatures up to 270 K. For kaolinite, contact freezing was observed below 269 K and the freezing probability increased to 100% as the temperature decreased to 256 K. It was estimated that the water drops captured several thousand particles during the time the clay particles passed the drops. The results from the present study are consistent with the previous results by Pitter and Pruppacher (1973) when water vapour is added. Assuming a collision efficiency of unity at 240 K, we conclude that one or a few collisions are usually sufficient to induce contact freezing under the conditions employed here. We can not directly prove that a single collision at 240 K indeed is sufficient to induce contact freezing, and the direct proof will have to await further studies using fast cameras with micrometer resolution. However, the assumption appears reasonable considering that 240 K is close to the temperature where homogeneous freezing of water occurs and far below the threshold temperature for immersion freezing induced by kaolinite.

A few attempts have been made to explain the mechanism(s) behind contact freezing, but the matter remains unresolved. Cooper (1974) suggested a mechanism by which an ice nucleus formed on the surface of an ice nucleus was able to induce

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freezing upon contact with a supercooled water drop. Fukuta (1975) suggested that contact nucleation is associated with liquid-air interface movement along the nucleus surface during the mechanical contact process, which results in transient high free energy conditions. Other hypotheses include the partial solubility of the ice nucleus in water (Fletcher, 1970; Guenadiev, 1970), and incomplete adsorption upon initial contact with water (Evans, 1970). In related work Czys (1989) presented an experiment in which the freezing of 3 mm drops was stimulated by a mechanical shock. Czys (1989) speculated that collision of supercooled drops in clouds might result in freezing, but the importance of the mechanism under atmospheric conditions remains uncertain (Czys and Lew, 1999). In recent studies Shaw et al. (2005) and Durant and Shaw (2005) investigated heterogeneous freezing induced by volcanic ash particles. Ash particles were immersed in water droplets and cycled through hundreds of freezing events. Ice nucleation occurred at higher temperatures if the ice nucleus was in contact with the surface of the drop, than if it was fully immersed within the drop. The contact freezing efficiency did not depend on whether surface contact was from the outside in, or the inside out. The experimental results appear to rule out most of the earlier proposed hypotheses for the contact freezing mechanism, since there was no transient contact event during the experiments and contact freezing was in operation during many freezing cycles. Suzuki et al. (2007a) used a high-speed camera to observe the freezing behavior of a water droplet on silicon surfaces treated with various silanes. Freezing was observed to preferably occur from the three-phase solid-liquid-air contact line. The freezing temperature was also higher on a rough coating than on a smooth fluoroalkylsilane coating (Suzuki et al., 2007b).

The effect of humidity on freezing in the kaolinite-water system is not easily understood based on the current knowledge. The available experimental evidence from previous studies indicates that the existence of a solid-liquid-air interface strongly favour ice nucleation. The detailed surface properties of the solid particle may determine the onset temperature for contact freezing, but a number of different materials are able to induce contact freezing at a higher temperature compared to immersion freezing. The

surface layer on water has somewhat different properties compared to the bulk. The mobility is higher and the density is somewhat lower. It is also likely that the surface layer more easily adapt to density changes when an ice phase is formed compared to the bulk. On its own, water does not appear to crystallize faster in the surface layer compared to in the bulk. A template is obviously required that can help the liquid to form an ice nucleus of sufficient size that may continue to grow. The template is related to the surface properties of the solid particle. One may speculate that the molecular level water-surface interactions are important, but confined spaces like pores and other surface features may play a role.

5 Conclusions

Freezing of supercooled water droplets induced by collisions with kaolinite dust particles has been studied in an EDB at temperatures from 240 to 268 K. The relative humidity was observed to influence the freezing process. Under dry conditions freezing occurred below 249 K, while a freezing threshold of 267 K was observed at a high relative humidity. The effect of relative humidity appears to be related to a direct influence on the contact freezing process itself, and it is not related to the lifetime of the droplets in the electrodynamic balance. Assuming that collisions at the lowest temperature employed had a probability of unity, one or a few collisions were usually sufficient to produce contact freezing. In clouds, the RH is close to 100%. Hence, the data recorded with water vapor added is the most realistic case for atmospheric applications. The present results support the parameterization used in the modelling study by Lohmann and Diehl (2005).

This limited study should be extended to improve our understanding of the process responsible for the contact freezing phenomenon. There is considerable room for improvement of the experiments. Experiments should in the next step be carried out with monodisperse aerosol particles, and the influence of droplet size should be evaluated. The effects of relative humidity should be quantified. Further improvements should also

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involve using fast cameras with micrometer resolution to directly observe the freezing efficiency in single particle-droplet collisions.

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Table 1. Summary of the experiments. T is the air temperature between the rings, N_{tot} is the number of particles studied at each temperature, N_{frozen} is the number of frozen particles, and PF is the kaolinite particle air flow.

T/K	N_{tot}	$PF \text{ l min}^{-1}$	$N_{\text{frozen}}/N_{\text{tot}}$
240	9	0.43	1
242	3	0.43	1
243	7	0.43	1
244	4	0.43	0.75
246	10	0.43	0.5
247	10	0.43	0.3
249	3	0.43	0
251	4	0.43	0
258	10	0.83	0.5
263	5	0.83	1
266	29	0.83	0.79
267	4	0.83	0
267	8	1.25	1
268	7	0.83	0

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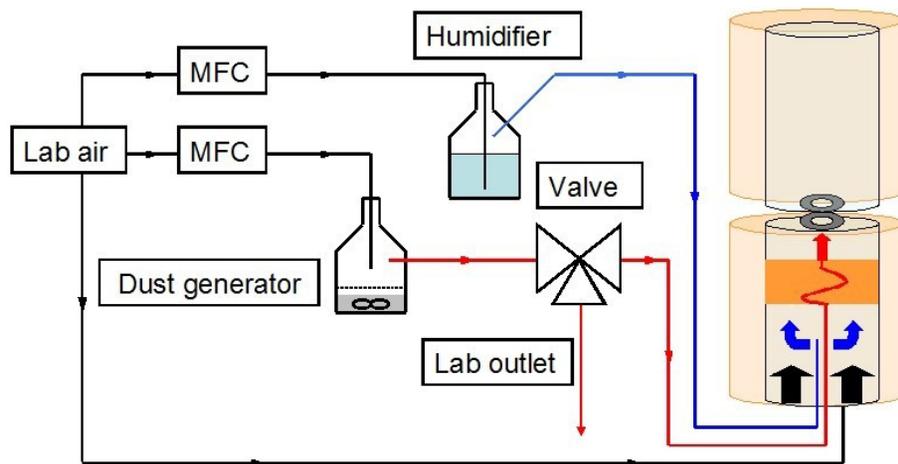


Fig. 1. Schematic view of the experimental setup. Black lines and arrows correspond to clean dry air, red lines/arrows to kaolinite aerosol and blue lines/arrows to humidified air.

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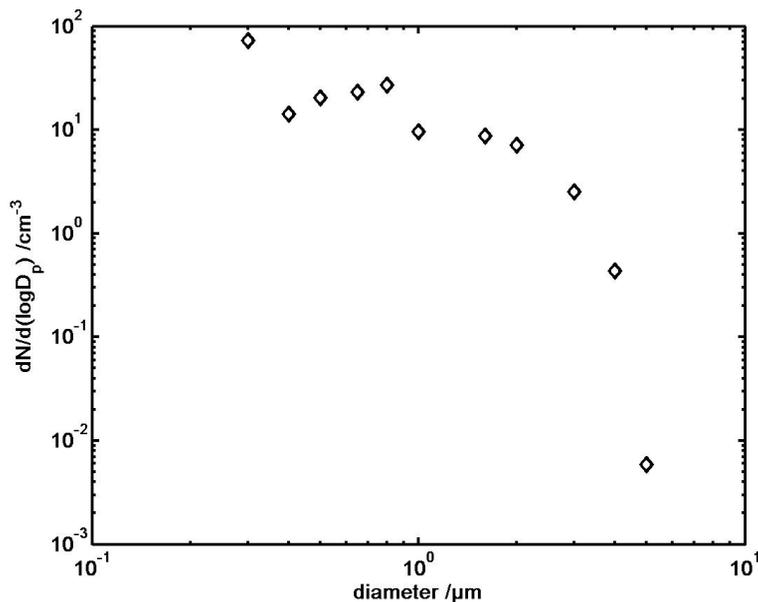


Fig. 2. Number size distribution of the kaolinite dust particles measured with an aerosol spectrometer.

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Collision freezing

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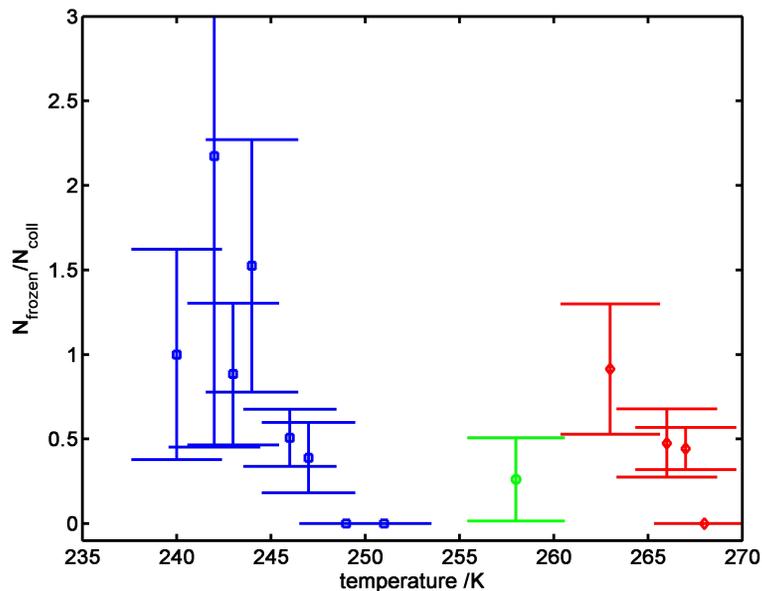


Fig. 3. Estimated number of freezing events per collision. Error bars are the standard deviation of the entity $N_{\text{frozen}}^3 \times t_f / (F \times \sum_{\text{frozen}}^2 t_f \times C \times N_{\text{total}})$ whose mean is the E of Eq. (3). Blue symbols represent experiments under dry conditions, green symbols intermediate flow of humid air, and red symbols high flow of humid air.

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